

## Solutions to Homework 4

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### BJT Model:

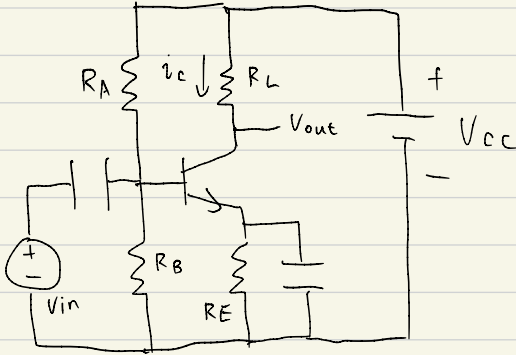
```
.model Q2N3904 NPN(Is=6.734f Xti=3 Eg=1.11 Vaf=74.03 Bf=416.4 Ne=1.259
+
+           Ise=6.734f Ikf=66.78m Xtb=1.5 Br=.7371 Nc=2 Isc=0 Ikr=0
Rc=1
+
+           Cjc=3.638p Mjc=.3085 Vjc=.75 Fc=.5 Cje=4.493p Mje=.2593
Vje=.75
+
+           Tr=239.5n Tf=301.2p Itf=.4 Vtf=4 Xtf=2 Rb=10)
*
*           National          pid=23          case=T092
*
*           88-09-08 bam      creation
*$
```

```
.model Q2N3906 PNP(Is=1.41f Xti=3 Eg=1.11 Vaf=18.7 Bf=180.7 Ne=1.5
Ise=0
+
+           Ikf=80m Xtb=1.5 Br=4.977 Nc=2 Isc=0 Ikr=0 Rc=2.5
Cjc=9.728p
+
+           Mjc=.5776 Vjc=.75 Fc=.5 Cje=8.063p Mje=.3677 Vje=.75
Tr=33.42n
+
+           Tf=179.3p Itf=.4 Vtf=4 Xtf=6 Rb=10)
*
*           National          pid=66          case=T092
*
*           88-09-09 bam      creation
*$
```

### MOSFET Model:

```
.model nch nmos(Level=1 Tox=300n Uo=600 Kp=20.54u W=144u L=8u Vto= 1.3
+
+           Lambda=15m Cbd=4p Cbs=4p Cgdo=1.7n Cgso=1.7n Rs=1 Rd=1)
.model pch pmos(Level=1 Tox=300n Uo=300 Kp=10.32u W=328u L=8u Vto=-1.5
+
+           Lambda=15m Cbd=8p Cbs=8p Cgdo=1.7n Cgso=1.7n Rs=1 Rd=1)
```

# Common - Emitter Amp. using npn 2N3904



$$V_{CC} = 6V \quad R_E = 1k\Omega$$

$$V_A = 74.03V, \quad \beta = 416.4$$

$$Q \text{ Point} \Rightarrow I_C = 2.6mA$$

small-signal:

$$g_m = \frac{I_C}{V_T} = \frac{2.6mA}{25mV} = 0.104S$$

$$r_o = \frac{V_A}{I_C} = \frac{74.03V}{2.6mA} = 28.5k\Omega$$

$$A_v = -g_m (R_L // r_o), \quad R_L = -\frac{A_v r_o}{g_m r_o + A_v} = 193.6\Omega$$

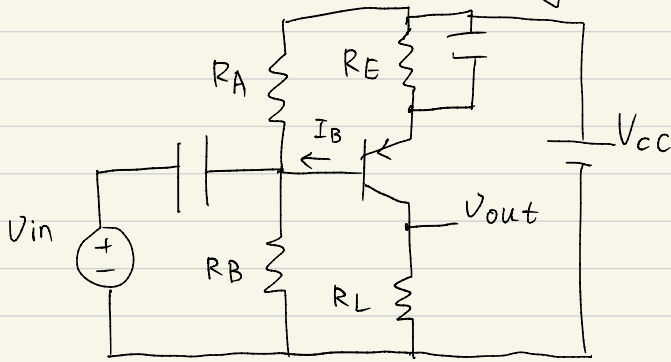
$$I_E = \frac{I_C}{\alpha} = \frac{I_C}{\beta/\beta+1} = \frac{2.6mA}{0.9976} = 2.606mA, \quad I_B = \frac{I_C}{\beta} = 6.244\mu A,$$

$$V_{BE} \cong 0.7V \quad V_B = V_{BE} + I_E R_E = 3.306V$$

choose  $R_A = 1k\Omega$ ,  $I_{RA}$  should be larger than  $I_B$ ,

$$R_B = \frac{V_B}{I_{RA} - I_B} = \frac{V_B}{\frac{V_{CC} - V_B}{R_A} - I_B} = 1.23k\Omega$$

# Common - Emitter using pnp 2N3906



$$\beta = 180.7 \quad V_A = 18.7V$$

$$V_{CC} = 6V, \quad R_E = 1k\Omega$$

$$I_C = 2.6mA,$$

$$g_m = \frac{I_C}{V_T} = 0.104S$$

$$r_o = \frac{V_A}{I_C} = \frac{18.7V}{2.6mA} = 7.19k\Omega$$

$$I_B = \frac{I_C}{\beta} = \frac{2.6mA}{180.7} = 14.39\mu A$$

$$I_S = 1.41fA$$

$$R_L = - \frac{A_v r_o}{g_m r_o + A_v} = 197.59\Omega$$

$$I_E = \frac{I_C}{\alpha} = \frac{I_C}{\beta/\beta+1} = \frac{2.6mA}{0.9945} = 2.614mA$$

$$V_{EB} \cong 0.7V$$

$$V_B = V_{CC} - I_E R_E - V_{EB} = 6V - 2.614mA \cdot 1k\Omega - 0.7V = 2.686V$$

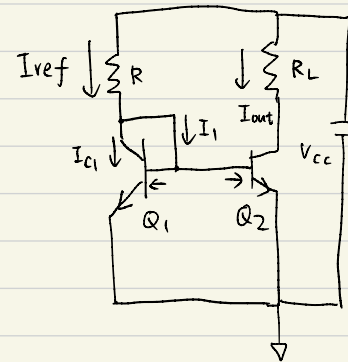
choose  $R_A = 1k\Omega$ , then,

$$R_B = \frac{V_B}{I_{RA} + I_B} = \frac{V_B}{\frac{V_{CC} - V_B}{R_A} + I_B} = 807\Omega$$

## Current Mirror using BJT

1) Sinking, npn, 2N3904

$$\hookrightarrow \beta = 416.4, V_A = 74.03V \quad I_S = 6.734fA$$



$$I_{B1} = \frac{I_{C1}}{\beta}$$

$Q_1$  &  $Q_2$  share  $V_{BE}$

$$\Rightarrow I_{B2} = I_{B1} = I_{C1}/\beta$$

$$\Rightarrow I_1 = I_{B1} + I_{B2} = 2I_{C1}/\beta$$

$$I_{ref} = I_1 + I_{C1} = \left(1 + \frac{2}{\beta}\right) I_{C1} = \left(1 + \frac{2}{\beta}\right) I_S e^{\frac{V_{BE}}{V_T}}$$

Solve  $V_{BE} = 0.683V$  [which is close to  $0.7V$ ]

$$R = \frac{V_{CC} - V_{CE}}{I_{ref}} = \frac{6V - 0.683V}{5mA} = 1063\Omega$$

mirror:

$$I_o = I_{ref} \frac{1}{1 + \frac{2}{\beta}} \left[ 1 + \frac{V_o - V_{BE}}{V_A} \right]$$

as we want  $I_o = I_{ref}$ , then,  $\frac{2}{\beta} = \frac{V_o - V_{BE}}{V_A}$

$$V_o = V_{BE} + V_A \frac{2}{\beta} = 0.683V + 74.03V \cdot \frac{2}{416.4} = 1.039V$$

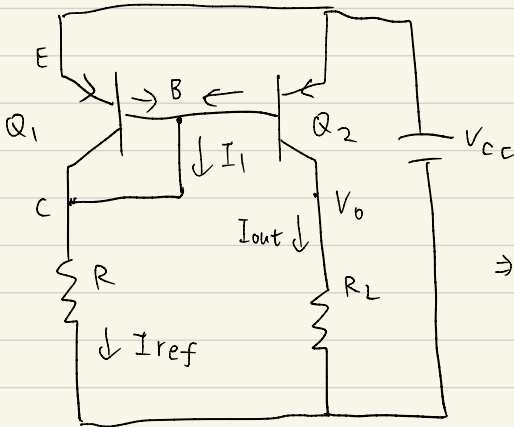
$$R_L = \frac{V_{CC} - V_o}{I_o} = \frac{(6 - 1.039)V}{5mA} = 992\Omega$$

2) Sourcing, PNP 2N3906

$$\beta = 180.7, \quad I_s = 1.41 \text{ fA}$$

$$V_A = 18.7 \text{ V}$$

$$I_1 = 2 I_B = \frac{2 I_{C1}}{\beta}$$



$$I_{ref} = I_1 + I_{C1} = \left( \frac{2}{\beta} + 1 \right) I_{C1}$$

$$= \left( \frac{2}{\beta} + 1 \right) I_s e^{V_{EB}/V_T}$$

Solve  $V_{EB} = 0.722 \text{ V}$

$$\Rightarrow R = \frac{V_{CC} - V_{EB}}{I_{ref}} = \frac{6 \text{ V} - 0.722 \text{ V}}{5 \text{ mA}} = 1056 \Omega$$

Similarly, 
$$I_o = I_{ref} \frac{1}{1 + \frac{2}{\beta}} \cdot \left[ 1 + \frac{V_{CC} - V_{EB} - V_o}{V_A} \right]$$

then, 
$$\frac{2}{\beta} = \frac{V_{CC} - V_{EB} - V_o}{V_A}$$

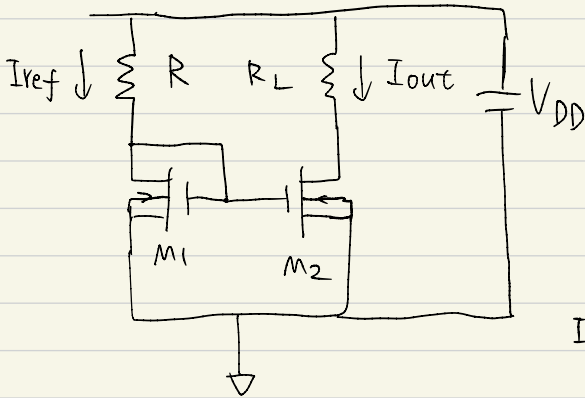
$$V_o = V_{CC} - V_{EB} - \frac{2}{\beta} V_A = 6 \text{ V} - 0.722 \text{ V} - \frac{2}{180.7} \cdot 18.7 \text{ V}$$

$$= 5.071 \text{ V}$$

$$R_L = \frac{V_o}{I_o} = \frac{5.071 \text{ V}}{5 \text{ mA}} = 1014 \Omega$$

# Current Mirror using 4007 NMOS

① sinking, use NMOS



We want  $I_{out} = I_{ref} = 5 \text{ mA}$

for  $M_1$ :  $V_{GS} = V_{DS}$ ,

$k_n' = 20.54 \mu$ ,  $W = 144 \mu$

$V_{to} = 1.3 \text{ V}$   $L = 8 \mu$

$\lambda = 15 \text{ m}$

$$I_{ref} = \frac{1}{2} k_n' \left( \frac{W}{L} \right) (V_{GS} - V_{to})^2 (1 + \lambda V_{DS})$$



Solve  $V_{GS}$  in matlab,

$$V_{GS} = V_{DS} = 6.27 \text{ V}$$

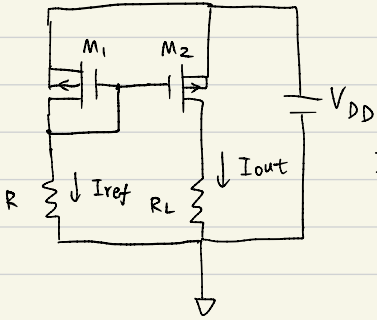
We notice that  $V_{GS} > V_{DD}$ , so  $V_{DD} = 6 \text{ V}$  is not enough to drive this current mirror,

So we change  $V_{DD}$  to  $9 \text{ V}$ , then

$$R = \frac{V_{DD} - V_{GS}}{I_{ref}} = \frac{9 \text{ V} - 6.27 \text{ V}}{5 \text{ mA}} = 546 \Omega$$

So we approximately set  $R_L = R = 546 \Omega$

② Sourcing, using PMOS



$$k_p' = 10.32 \mu, \quad W = 328 \mu,$$

$$V_{to} = -1.5V \quad L = 8 \mu$$

$$\lambda = 15 \text{ m}$$

$$I_{ref} = \frac{1}{2} k_p' \left( \frac{W}{L} \right) (V_{SG} - |V_{to}|)^2 (1 + \lambda V_{SD})$$

$$= 5 \text{ mA}$$

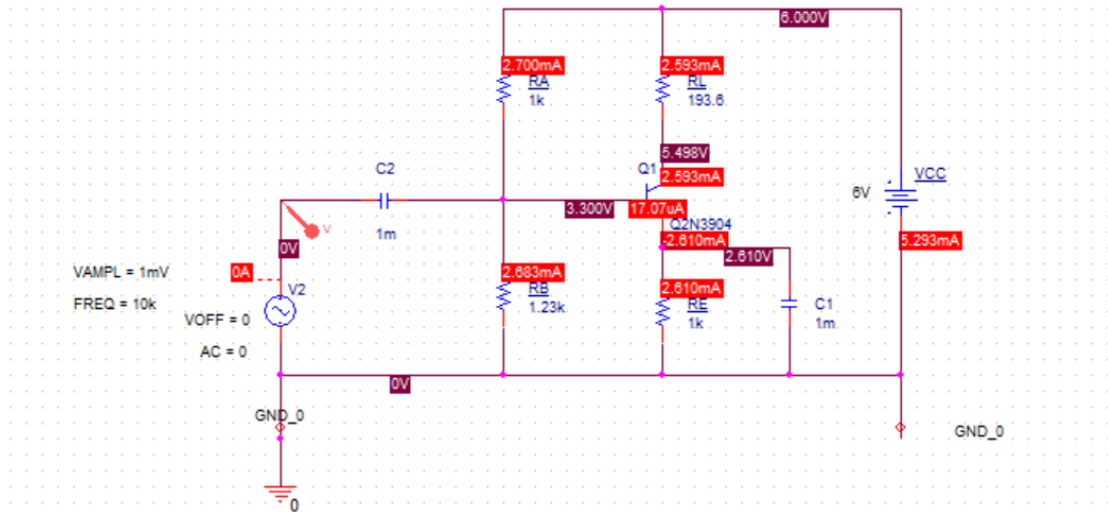
$$\text{Solve in matlab, } V_{SG} = V_{SD} = 6.15V$$

$$\text{Set } V_{DD} = 9V, \quad R = \frac{V_{DD} - V_{SD}}{I_{ref}} = \frac{9V - 6.15V}{5A} = 570 \Omega$$

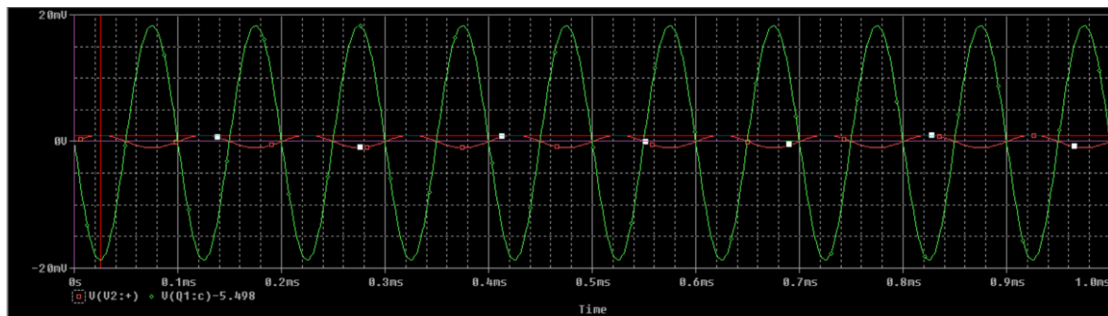
$$R_L = R = 570 \Omega$$

Problem 1

b.



$I_C=2.593\text{mA}$ , which is close to the required  $2.6\text{mA}$



Trace Color	Trace Name	Y1
	X Values	25.439u
CURSOR 1,2	V(V2:+) 1.0000m	
	V(Q1:c)-5.498 -18.714m	

The amplitude of output voltage is approximately  $18.7\text{mV}$ , and  $v_{in}$  and  $v_{out}$  are in opposite phase.

So the voltage gain

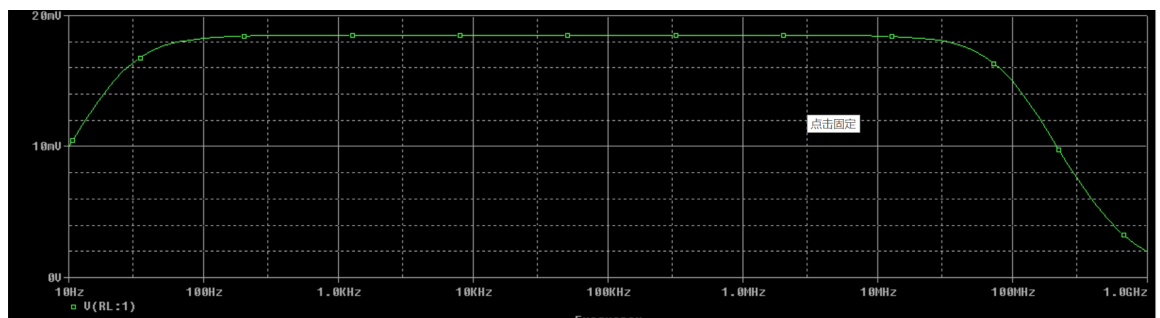
$A_v = 18.7\text{mV}/1\text{mV} = -18.7$ , which is close to  $-20$ .

c.

Use Pspice>>Markers>>Advanced>>phase of voltage

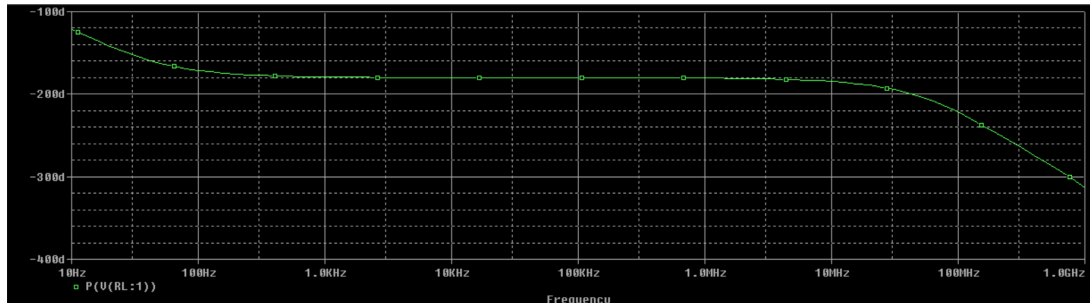
AC=1m, run in AC sweep

Voltage magnitude:



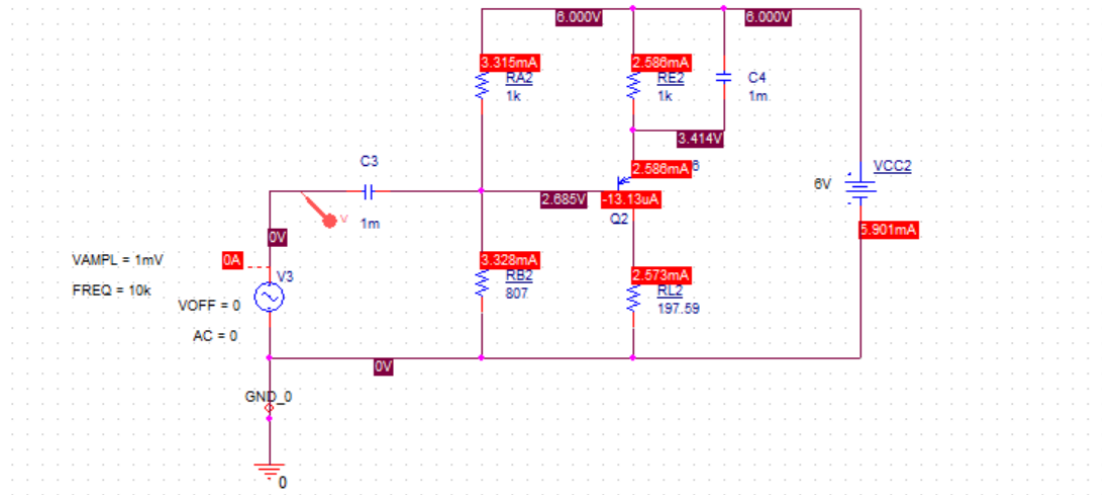


Voltage phase:

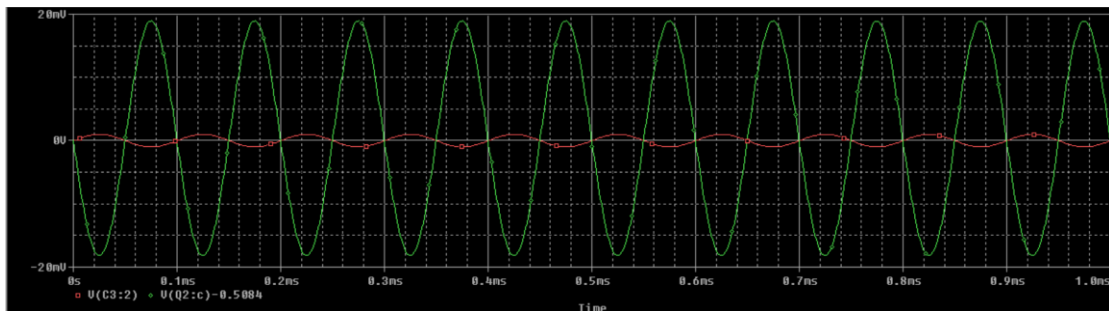


The amplitude of output voltage remains nearly 20mV and the phase stays at -180 degrees in a frequency band with the range of about 100Hz-10MHz. At low frequency, voltage gain is lower and the phase is higher than -180 degrees because of the bypass capacitors. As the frequency further increases, the amplitude starts to drop and the phase starts to drop. It is because of the existence of parasitic capacitors of the transistor.

d.  
pnp



$I_C = 2.586\text{mA}$ .



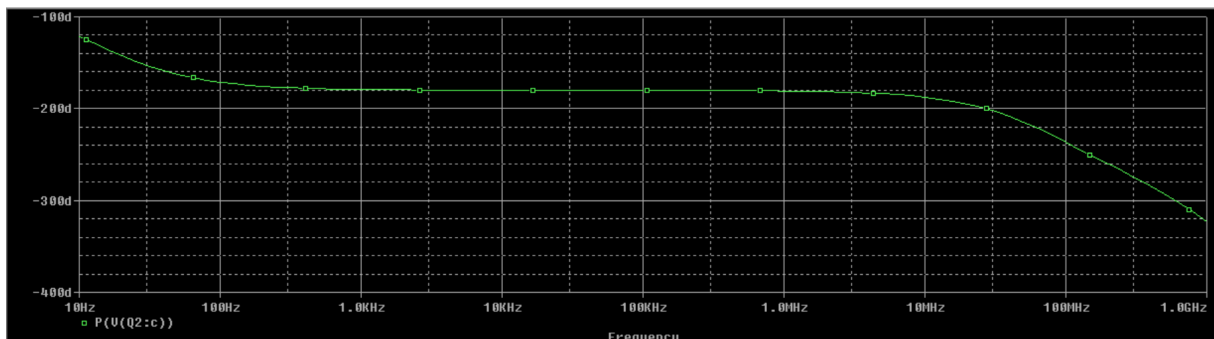
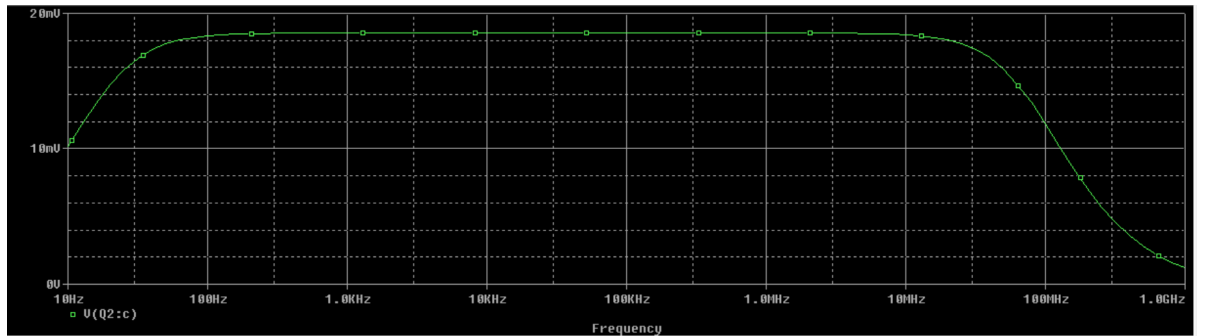
Trace Color	Trace Name	Y1
	X Values	74.561u
CURSOR 1,2	V(C3:2)	-1.0003m
	V(Q2:c)-0.5084	18.915m

The amplitude of output voltage is approximately 18.9mV, and  $v_{in}$  and  $v_{out}$  are in opposite phase.

So the voltage gain

$A_v = 18.9\text{mV}/1\text{mV} = -18.9$ , which is close to -20.

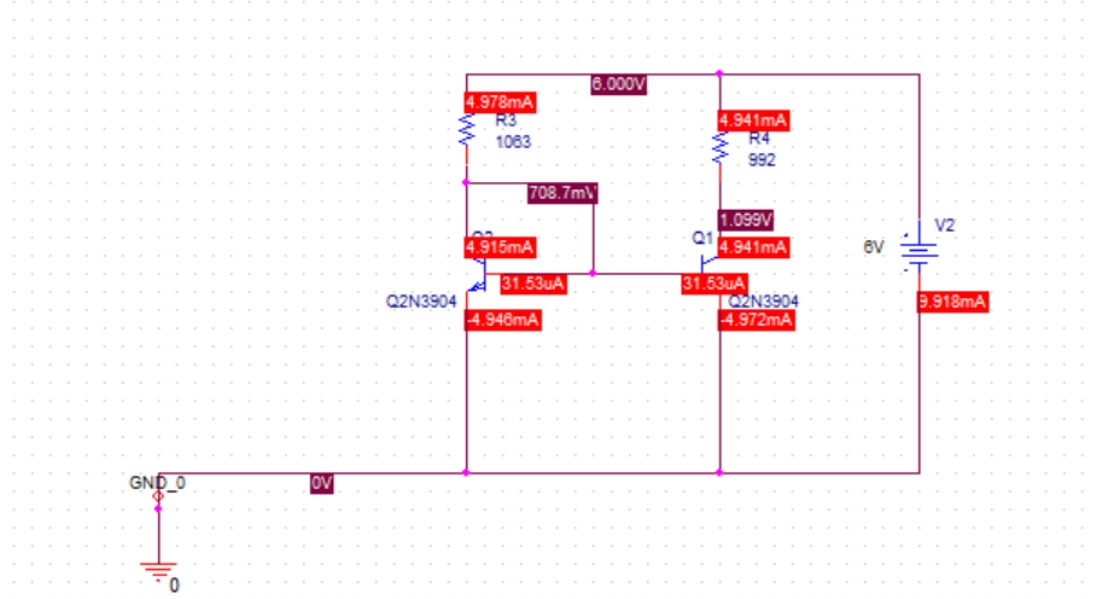
Frequency response:



## Problem 2

a/d.

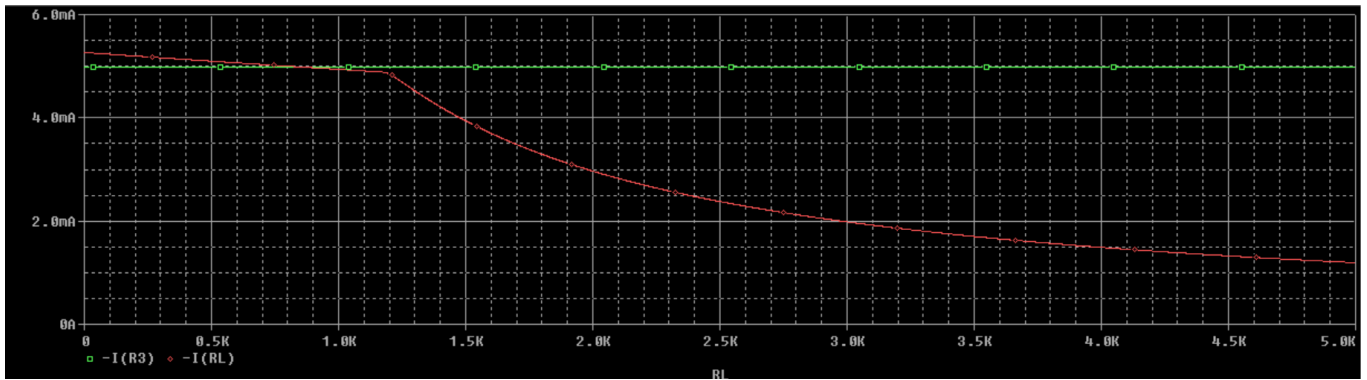
Sinking current mirror:



When  $R_L = 992\text{Ohm}$ ,

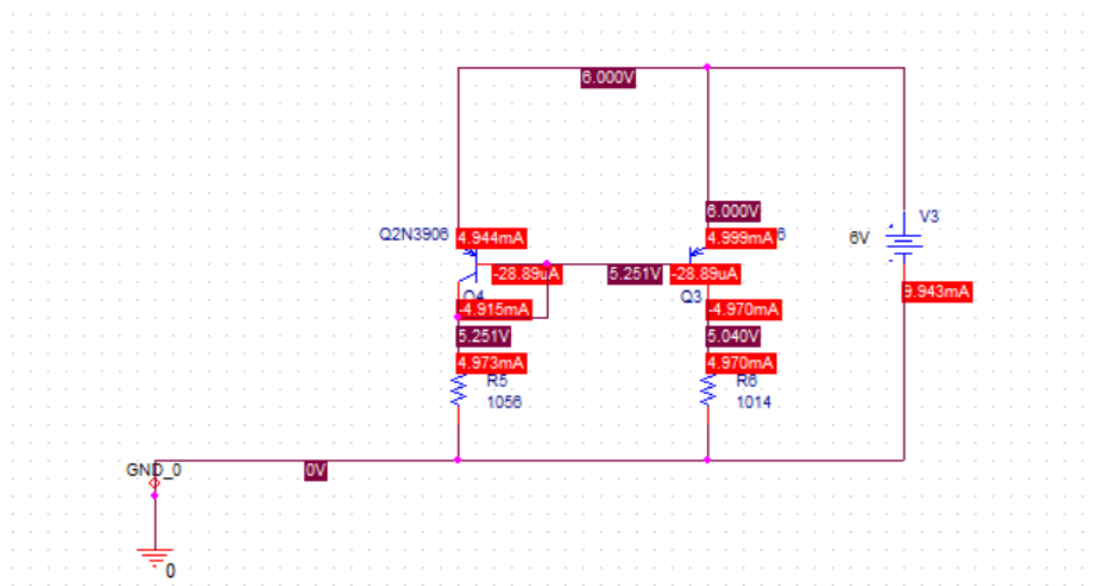
$I_{ref} = 4.978\text{mA}$ ,  $I_{out} = 4.941\text{mA}$ , which is very close.

Parametric sweep on RL:

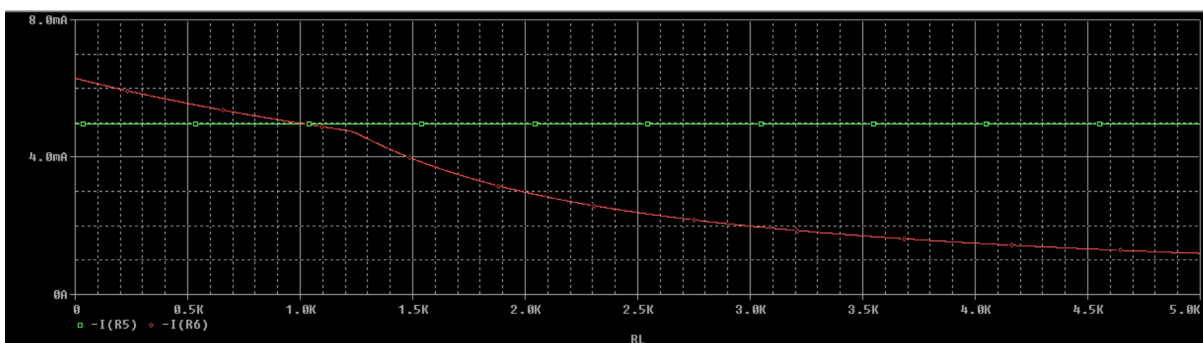


Current mirror is valid when RL is smaller than around 1.2k ohm.

Source current mirror:



When  $R_L=1014\Omega$ ,  
 $I_{ref}=4.973mA$ ,  $I_{out}=4.970mA$ , which is very close.

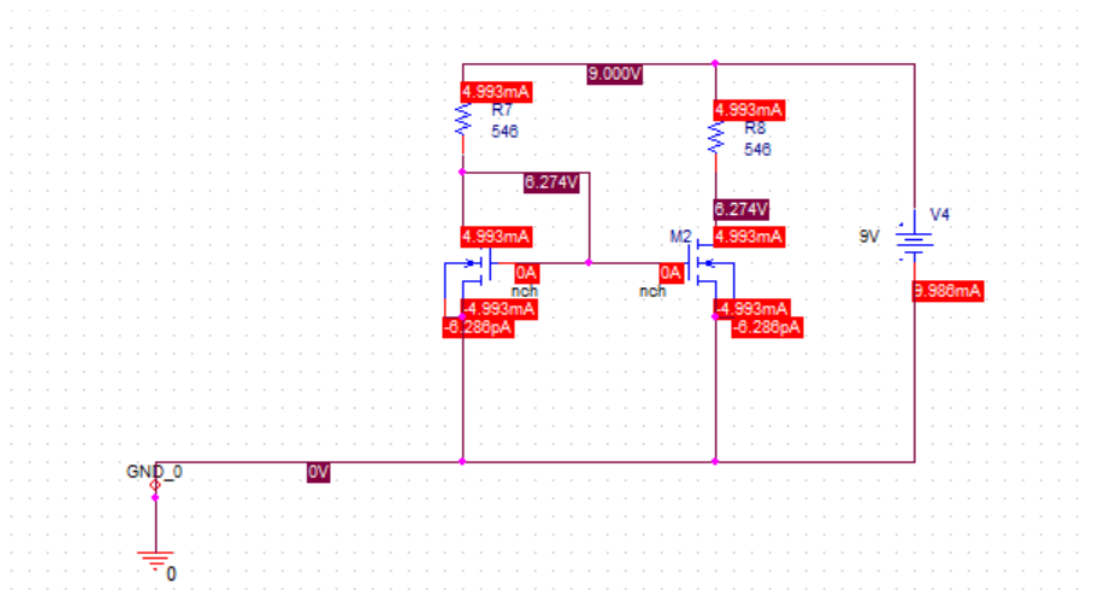


Parametric sweep on RL:

Current mirror is valid when RL is smaller than around 1.2k ohm.

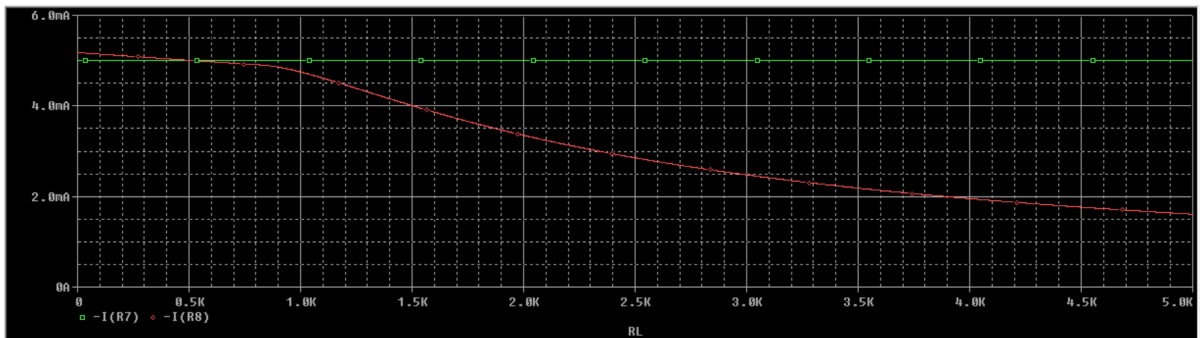
b/d

Sinking current mirror using NMOS:



When  $R_L=546\Omega$ ,

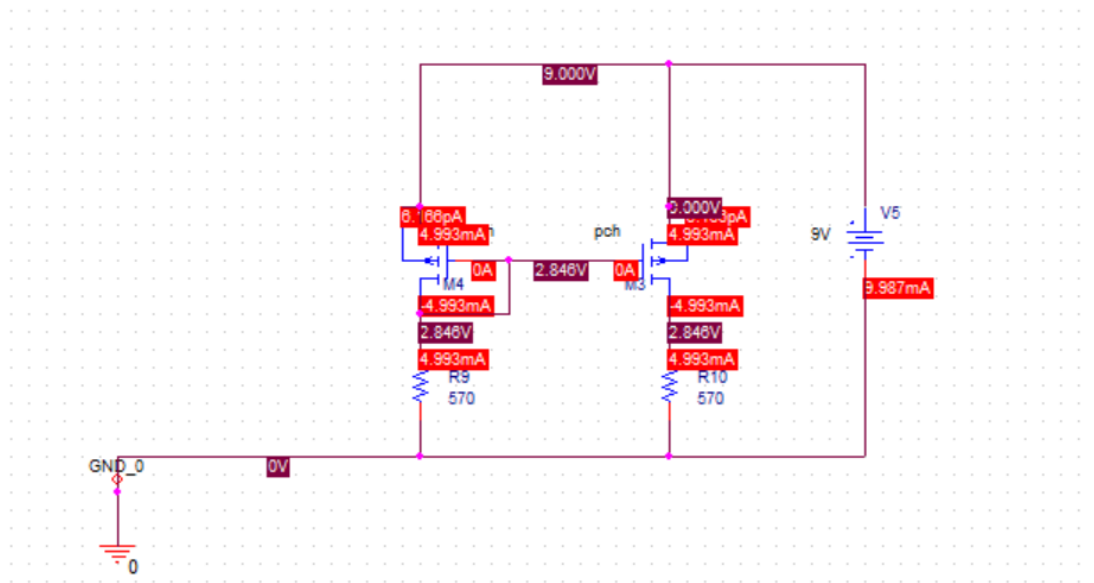
$I_{ref}=4.993\text{mA}$ ,  $I_{out}=4.993\text{mA}$ , which is very close.



Parametric sweep on  $R_L$ :

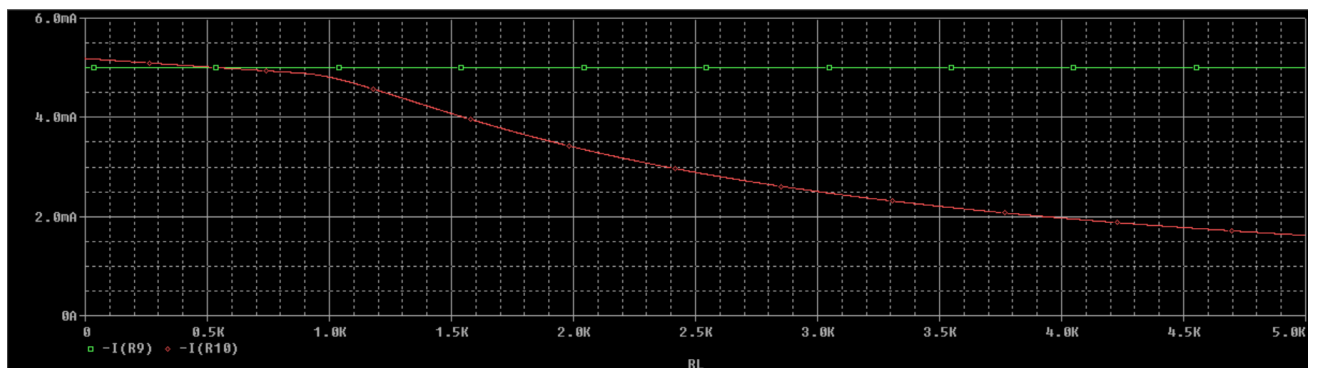
Current mirror is valid when  $R_L$  is smaller than around 1k ohm.

Sourcing current mirror using PMOS:



When  $R_L=570\Omega$ ,

$I_{ref}=4.993\text{mA}$ ,  $I_{out}=4.993\text{mA}$ , which is very close.



Parametric sweep on  $R_L$ :

Current mirror is valid when  $R_L$  is smaller than around 1k ohm.