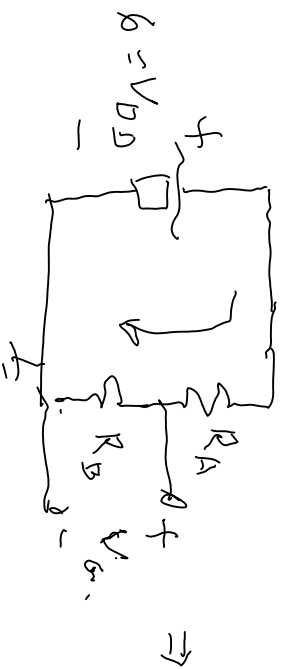


Character 9 = differentials pairs  
 Character 10 = frequency response



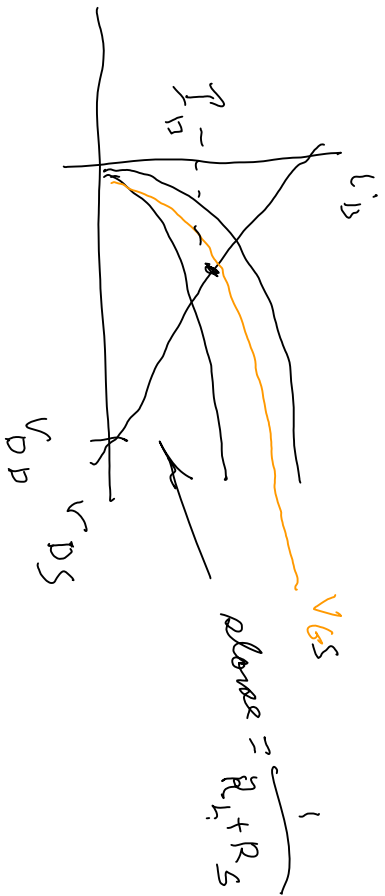
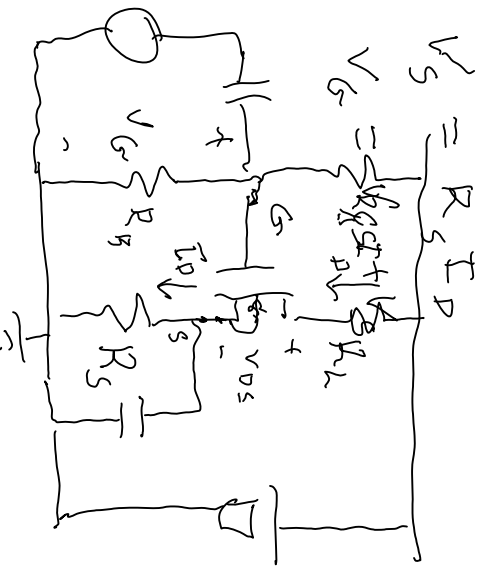
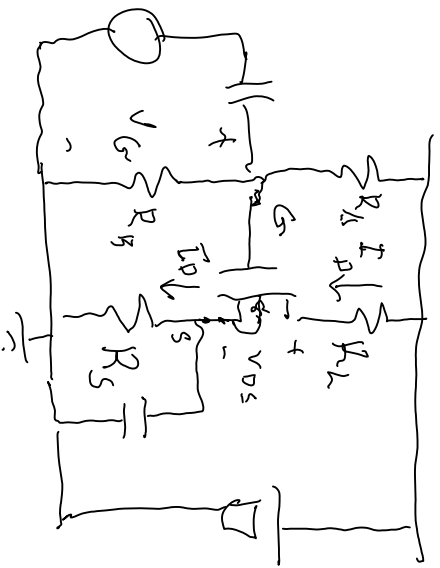
$$R_{Th} = \frac{R_A R_B}{R_A + R_B}$$

$$I_{sc} = \frac{V_{DD}}{R_A}$$

$$V_{oc} = \frac{R_B}{R_A + R_B} \cdot V_{DD}$$

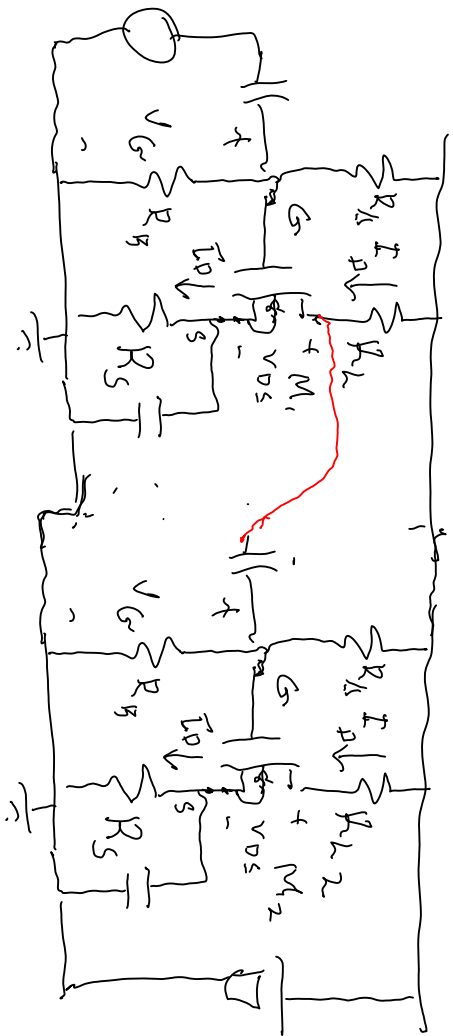
$$V_{oc} = \frac{1}{1 + \frac{R_B}{R_A}} \cdot V_{DD}$$

$R_{Th}$  is the Thevenin resistance seen from the gates looking into the drain network.  
 $I_{sc}$  is the short-circuit current when the gates are shorted to ground.  
 $V_{oc}$  is the open-circuit voltage when the gates are open.  
 can choose one of  $R_A$  &  $R_B$

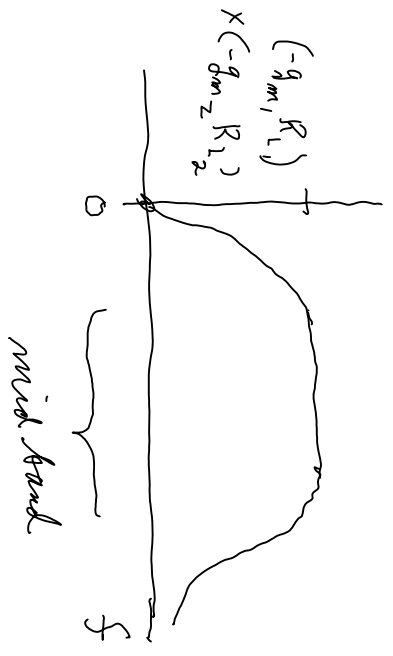


gain =  $A_v = -g_m R_L = -8$

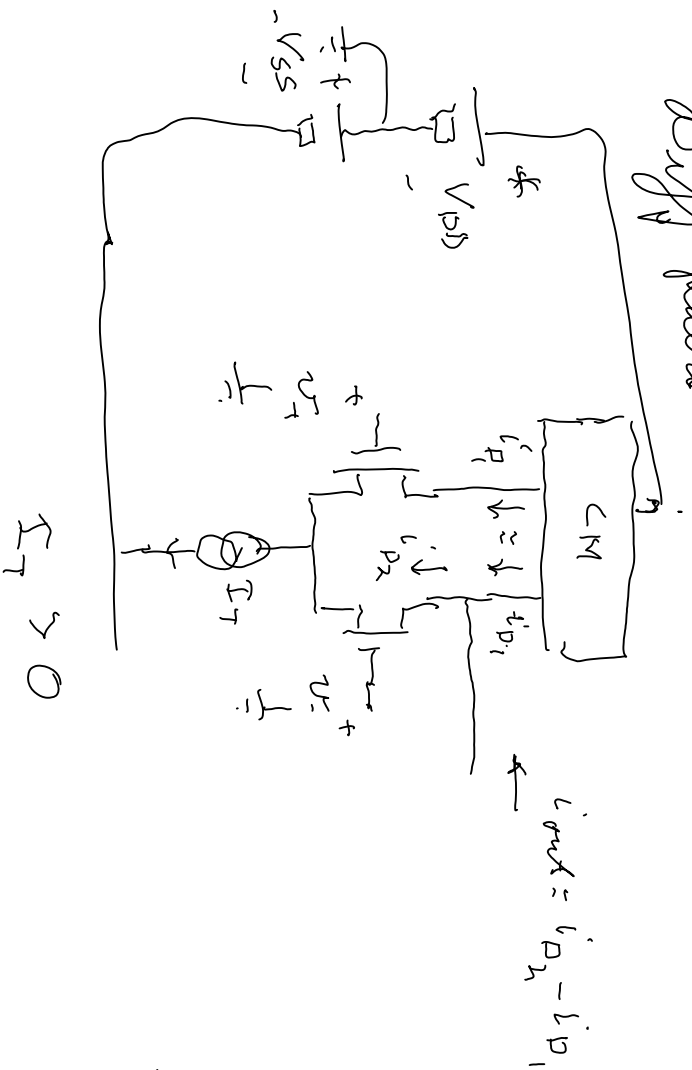
$I_D = K_2 (V_{GS} - V_{T0})^2$ ;  $g_m = 2K_2 (V_{GS} - V_{T0}) = \frac{2 \cdot I_D}{V_{GS} - V_{T0}}$



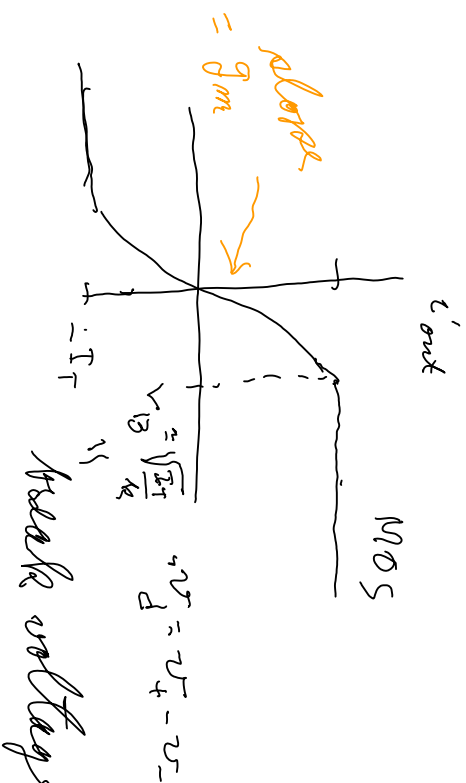
$$|A_v(j\omega)|$$



Differential pair



$$i'_{out} = i_{D2} - i_{D1}$$

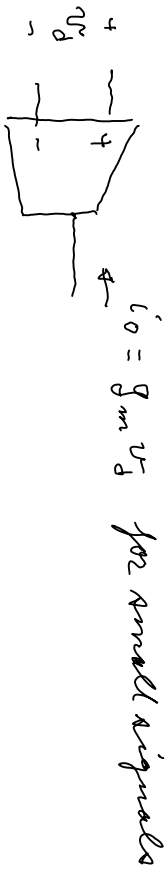


if diff pair is BJT

$$i_D = I_T \tanh\left(\frac{v_D}{2V_T}\right); \quad g_m = I_T \cdot \left(\frac{1 - \tanh^2\left(\frac{v_D}{2V_T}\right)}{2V_T}\right)$$

gives a multiplier of  $\tanh\left(\frac{v_D}{2V_T}\right)$

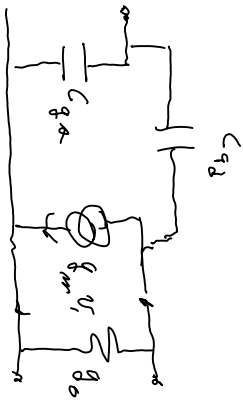
@  $v_D = 0$



Return to CS amplifiers for frequency responses



$$(g_m - \alpha C_{gd})v_i + (g_o + \alpha C_{gd})v_o = -g_L v_o$$



$$Y \Rightarrow \begin{bmatrix} \alpha(C_{ga} + C_{gd}) & -\alpha C_{gd} \\ g_m - \alpha C_{gd} & g_o + \alpha C_{gd} \end{bmatrix} \begin{bmatrix} v_i \\ v_o \end{bmatrix} = \begin{bmatrix} i_i \\ i_o = -\frac{v_o}{R_L} = -g_L v_o \end{bmatrix}$$

$$A_{v_r}(\omega) = \frac{v_o}{v_i} = \frac{v_{out}}{v_{in}} = \frac{g_m - \alpha C_{gd}}{-(g_o + g_L) + \alpha C_{gd}} \Rightarrow A = \frac{d v_o}{d v_i} \quad \frac{d i_o}{d i} = \frac{d(C v_c)}{d t} = C \frac{d v_c}{d t} = C A \cdot v_x$$

$$[(g_0 + G_L) + a C_{gD}] v_2 = -(g_m - a C_{gD}) v_1 \Rightarrow C_{gD} \frac{dv_2}{dt} + (g_0 + G_L) v_2 = C_{gD} \frac{dv_1}{dt} - g_m v_1$$

(a → d/dt)

ODE

look for solutions

$$v_1(t) = V_1 e^{at}, \quad v_2 = v_2 e^{at} \Rightarrow v_2 = v_2(t+1)$$

-∞ < t < ∞

$$\Rightarrow \frac{v_2}{v_1} = A_{v2}(a)$$

But  $e^{at} = e^{(\sigma + j\omega t)} = e^{\sigma t} (\cos \omega t + j \sin \omega t) \Rightarrow$  now  $a = \sigma + j\omega =$  complex frequency

$$A_{v2}(j\omega) = \frac{j\omega C_{gD} - g_m}{j\omega C_{gD} + (g_0 + G_L)} = \left| A_{v2}(j\omega) \right| e^{j \Delta A_{v2}(j\omega)} \Rightarrow \left| A_{v2}(j\omega) \right| = \frac{\omega^2 C_{gD}^2 + g_m^2}{\omega^2 C_{gD}^2 + (g_0 + G_L)^2} = \frac{\text{num}^2}{\text{den}^2}$$

$$C_{gD} V_2 e^{at} + (g_0 + G_L) V_2 e^{at} = C_{gD} V_1 a e^{at} - g_m V_1 e^{at}$$

$$(a C_{gD} + (g_0 + G_L)) V_2 e^{at} = (C_{gD} a - g_m) V_1 e^{at}$$

no e^{at} ≠ 0 → finite terms

But also  $\mathcal{L}[f] = \int_{-\infty}^{\infty} f(t) e^{-at} dt$  ;  $d_1 \frac{dv_2}{dt} + d_0 v_2 = \frac{m_1 dv_1}{dt} + m_0 v_1$

$$\begin{aligned} \mathcal{L}\left[d_1 \frac{dv_2}{dt}\right] + \mathcal{L}[d_0 v_2] &= d_1 \mathcal{L}\left[\frac{dv_2}{dt}\right] + d_0 \mathcal{L}[v_2] = d_1 \mathcal{L}[v_2] + d_0 \mathcal{L}[v_2] = (d_1 + d_0) \mathcal{L}[v_2] \\ &= m_1 \mathcal{L}[v_1] + m_0 \mathcal{L}[v_1] \Rightarrow \frac{\mathcal{L}[v_2]}{\mathcal{L}[v_1]} = \frac{m_1 + m_0}{k_1 + k_2} \end{aligned}$$

now  $\lambda$  is a complex variable  $\lambda = \sigma + j\omega$

