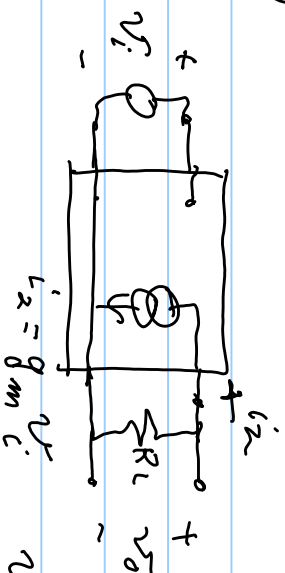


# BJT amplifiers

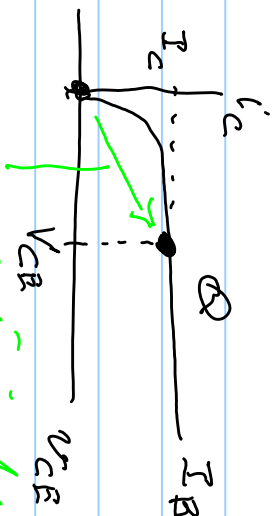


$$T_v = \frac{v_o}{v_i} = -g_m R_L$$

$$v_o = -g_m \cdot R_L \cdot v_i = -R_L i_o$$



2N3904  $\Rightarrow$  Q2N3904 in Spice Library



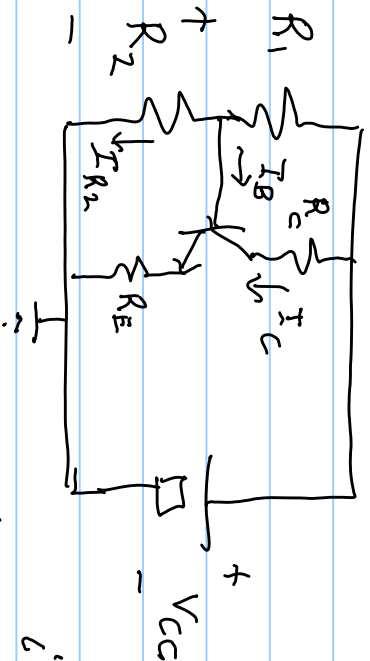
more origin for small signal

$$g_m = \frac{I_C}{V_T}, \quad V_T = \frac{kT}{q}$$

$$\approx 26mV$$

@ 300mK

forward bias BE junction  
reverse bias CE junction



$$I_E = -I_S \left( e^{V_{BE}/V_T} - 1 \right) \text{ ideal}$$

$$g_m = \frac{\partial I_C}{\partial V_{BE}}$$

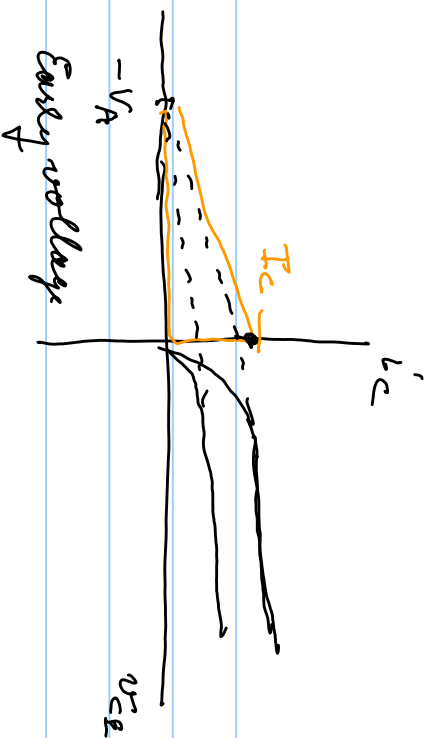
$$I_C = -\alpha I_E = \beta I_B$$

$$\frac{\partial I_C}{\partial V_{BE}} = -\alpha \frac{\partial I_E}{\partial V_{BE}} = -\alpha \left[ -I_S \cdot \frac{1}{V_T} \cdot e^{V_{BE}/V_T} \right]$$

$$\approx \alpha \frac{I_S e^{V_{BE}/V_T}}{V_T} = \frac{I_C}{V_T} = g_m$$

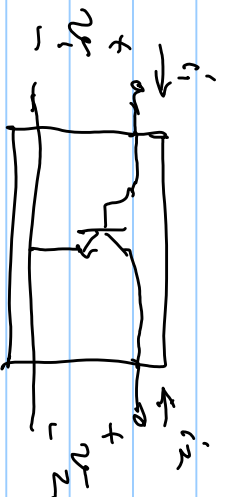
$$g_m \approx \frac{1 \times 10^{-3}}{26 \times 10^{-3}} \approx \frac{1}{26} = 0.04 \frac{\text{ampere}}{\text{volt}} \text{ for } 1 \text{ mA} = I_C$$

ideal gain is  $-g_m R_L$  but here losses



slope =  $\frac{I_C}{V_A}$  = output conductance

$= \frac{\partial i_c'}{\partial v_{CE}} = g_o$



at low frequencies  $\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} g_m & 0 \\ g_m & g_o \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \Rightarrow i = Yv$

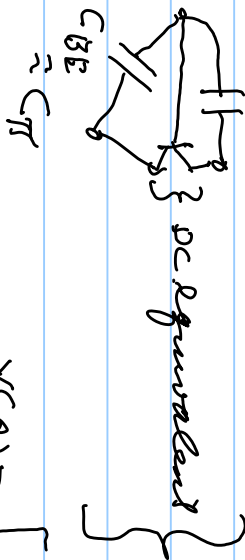
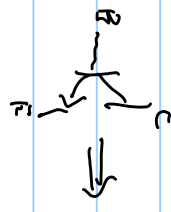
admittance

$i_1 = g_{m1}v_1 + g_{m2}v_2$   $g_{m1} = \frac{\partial i_1}{\partial v_1} = \frac{\partial i_c}{\partial v_{BE}} = \beta \frac{\partial i_c}{\partial v_{BE}}$  small signal

or  $v_{BE} \approx 0.6v$ ,  $\Rightarrow$  almost constant

$\frac{\partial i_c}{\partial v_1} \approx 0$  or  $\text{act } I_B \text{ by } R_1 \& R_2$

$$C_{BC} \approx C_p$$



$$Y(s) = \begin{bmatrix} sC_p + g_m & 0 \\ g_m & g_o \end{bmatrix}$$

(value terms with  $C_p$ )