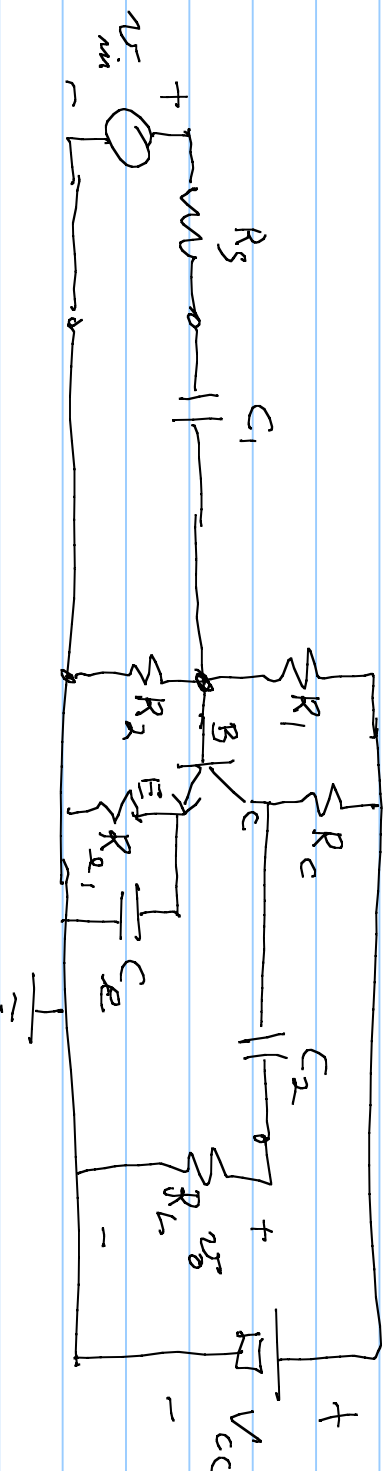


EE307

03/09/16

High frequency response AC analysis in Series



$$A_{v_{mid}} = \frac{V_o}{V_{i_{in}}}(\omega) \Rightarrow a = g'(\omega), \text{ and } \text{RPF} = \omega$$

$$|A_{v_{mid}}(j\omega)|$$



$$i = \frac{dq}{dt} = C \frac{dv}{dt}$$

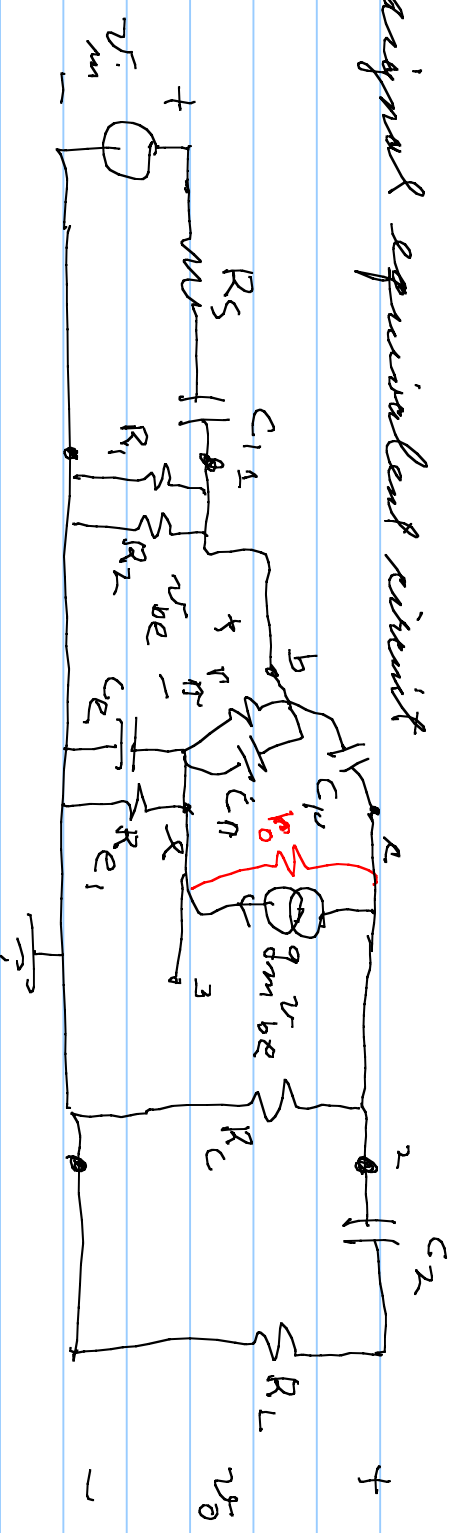
$$g(\omega) = \frac{I(\omega)}{V(\omega)} = aC \Rightarrow \text{RPF}(j\omega) = \frac{1}{j\omega} \cdot \frac{1}{C}$$

C = constant in time

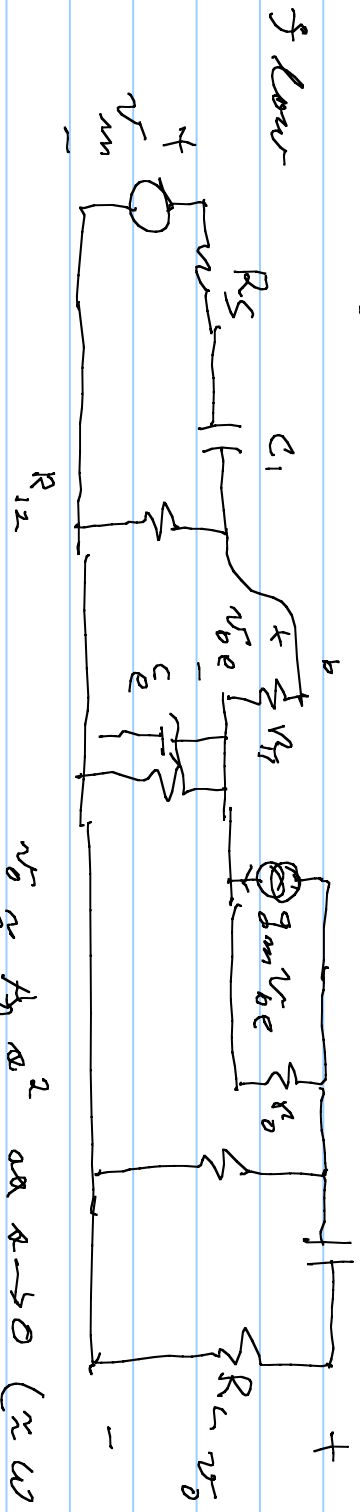
\Rightarrow

$$I(\omega) = I(\omega) = C a V(\omega)$$

signal equivalent circuit

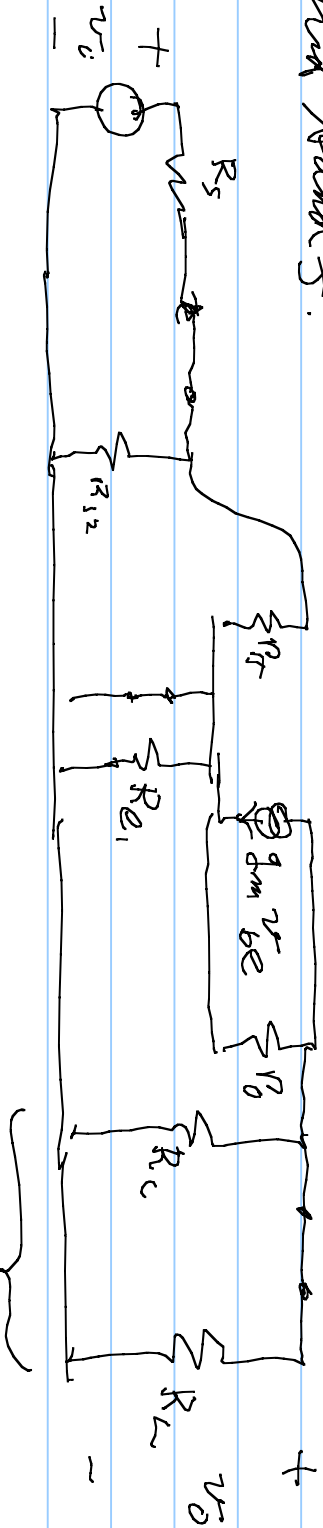


Changes in frequency f



$$\frac{v_o}{v_i} \approx A_{\omega} \omega^2 \quad \text{as } \omega \rightarrow 0 \quad (\omega \rightarrow 0 \text{ near DC})$$

mid band 5:

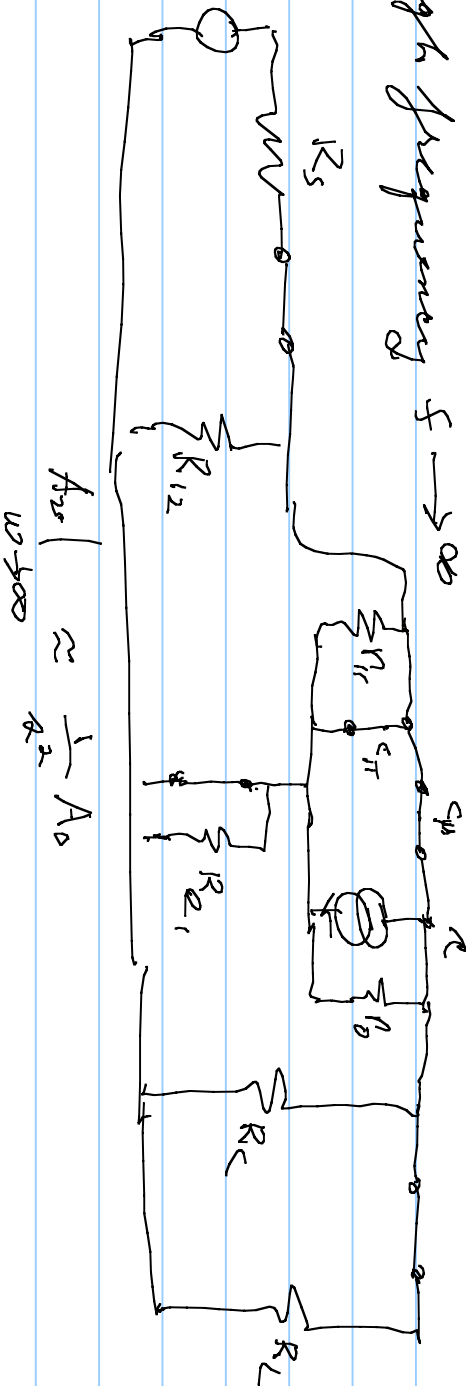


ideally $\frac{v_o}{v_i} \approx g_m R_L'$

effective $R_L = R_L'$

$g_m \approx \frac{I_C}{V_T}$

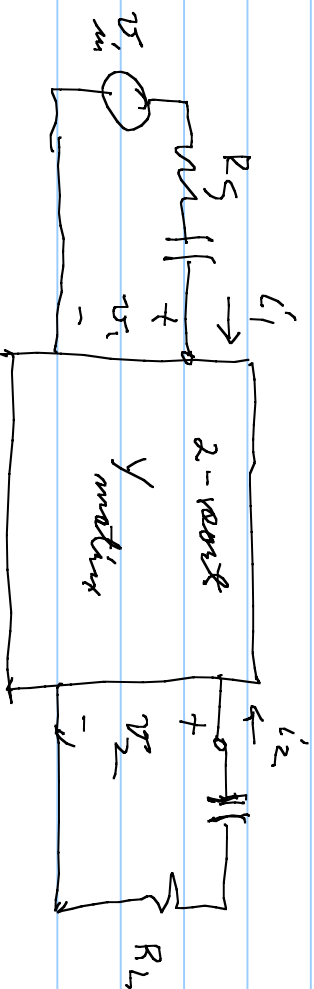
high frequency $f \rightarrow \infty$



$A_{v_{mid}} \approx \frac{1}{A_{v_{high}}}$

$\omega \rightarrow \infty$

analysis (SSSS)
 small signal sinusoidal steady state



$$Y = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = Y \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

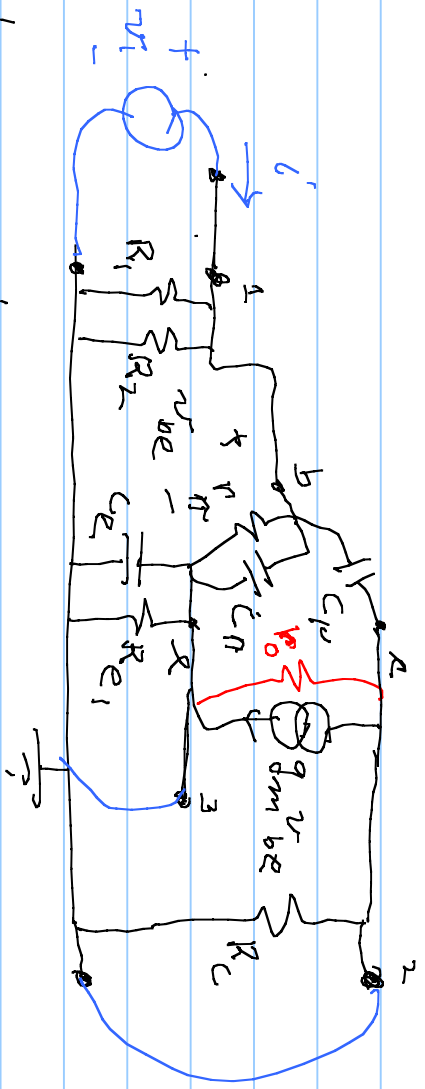
set $i_3 = 0$ to eliminate nodes

$$Y_3 \Rightarrow \begin{bmatrix} i_1 \\ i_2 \\ i_3 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \\ Y_{31} & Y_{32} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix}$$

$$0 = Y_{31} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + Y_{33} v_3 \Rightarrow v_3 = -\frac{1}{Y_{33}} Y_{31} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$\begin{bmatrix} i_1' \\ i_2' \end{bmatrix} = Y_{11}' \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + Y_{12} v_3 = \underbrace{\begin{bmatrix} Y_{11}' - Y_{12} \cdot \frac{1}{g_{33}} \\ Y_{21}' - Y_{22} \cdot \frac{1}{g_{33}} \end{bmatrix}}_Y \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

(of the 2-port)



$$Y_{11}' \Big|_{v_2 = v_3 = 0} = i_1' / v_1$$

