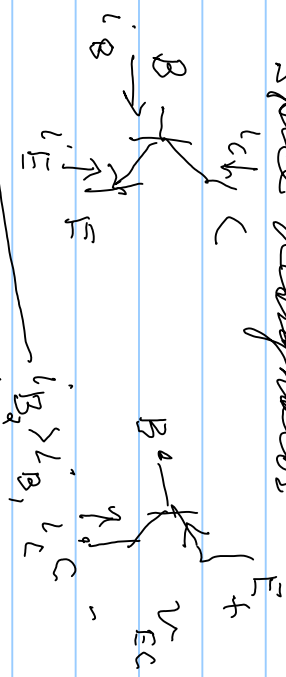
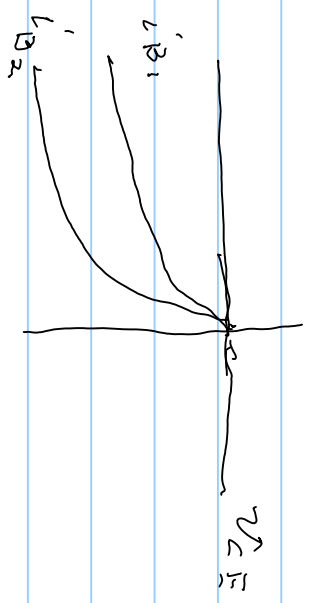
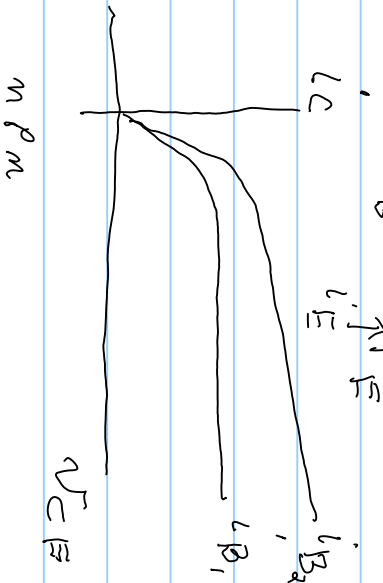


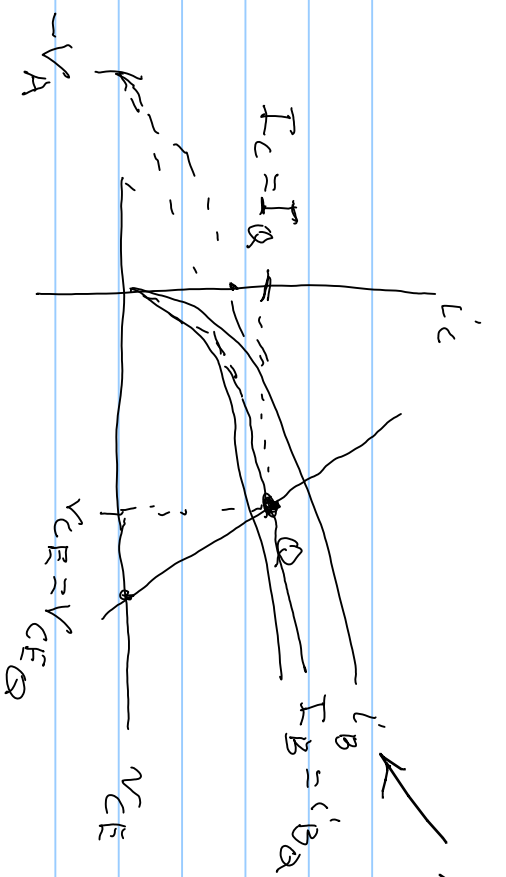
BJT 20pM 10pP Q2N3904 Q2N306

Series diodes



$$I_B + I_E + I_C = 0$$

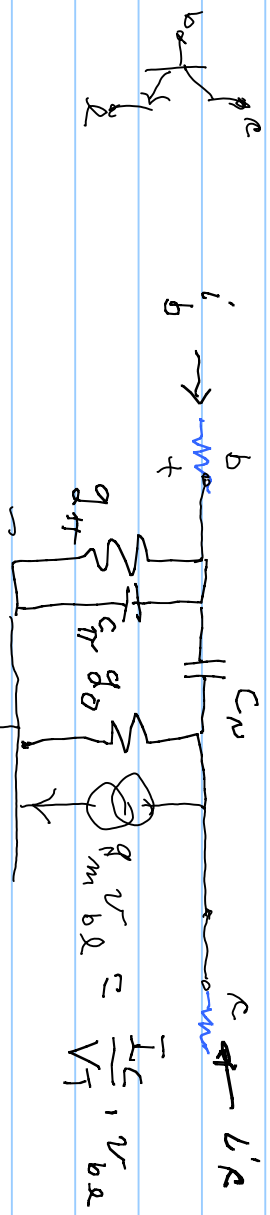




Slope $\approx \frac{I_C}{V_A} = \frac{\partial I_C}{\partial V_{CE}} \Big|_Q$

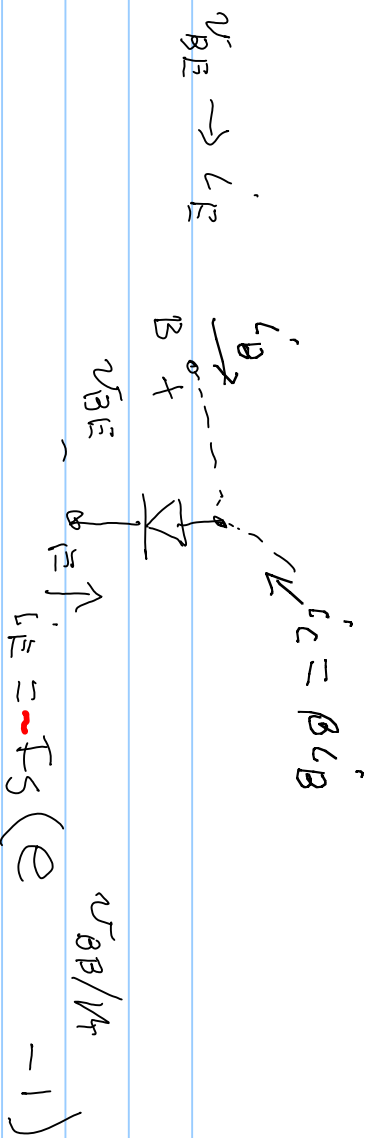
$g_o = \text{output conductance}$

Linearized $i = Yv$



$g_{\pi} = \frac{I_C}{\beta V_T}$ $g_o = \frac{I_C}{V_A}$ $g_m = \frac{I_C}{V_T}$

Hybrid π equivalent circuit



$$\frac{\partial i_B}{\partial v_{BE}} = \frac{\partial i_B}{\partial i_C} \frac{\partial i_C}{\partial v_{BE}}$$

$$= \frac{1}{\beta} \cdot \frac{I_C}{V_T}$$

$$= g_m = g_m$$

$$-i_E = -i_C \left| \frac{\partial i_E}{\partial v_{BE}} (v_{BE} - V_{BE}) + \frac{\partial^2}{\partial^2} \dots \right.$$

ignores

$$i_E - I_E = i_C = \text{signal} =$$

$$i_C = \beta i_B = \alpha (-i_E)$$

$$-\frac{\partial i_C}{\partial v_{BE}} = I_S \cdot \frac{1}{V_T} (e^{v_{BE}/V_T}) \approx \frac{-I_E}{V_T} = \frac{\alpha i_C}{V_T} \approx \frac{I_C}{V_T} \text{ a conductance}$$

$$i_C = -\alpha i_E = \alpha \left[\frac{I_C}{V_T} \right] v_{be} \Rightarrow i_C = g_m \cdot v_{be}, \quad g_m = \frac{I_C}{V_T}$$

