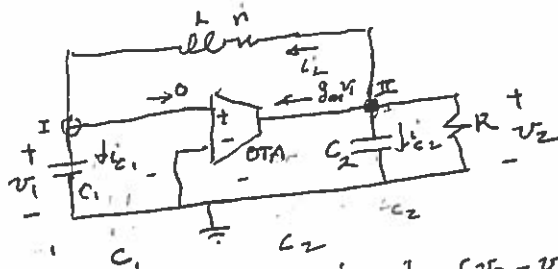


# Improved Colpitts Using OTA

04/12/14  
RWH



Make OTA as differential pair with current mirror output & tail current  $I_T$ ;  $i_{out} = I_T \tanh\left(\frac{v_{in}}{2V_T}\right) \approx g_m v_{in}$

KCL @ II:  $0 = i_L + g_m v_i + i_{C2} + \frac{v_2}{R} = \frac{1}{\alpha L + \mu} (v_2 - v_1) + g_m v_1 + \alpha C_2 v_2 + G v_2$

1)  $\Rightarrow \left(\frac{1}{\alpha L + \mu} - g_m\right) v_1 = \left(\frac{1}{\alpha L + \mu} + \alpha C_2 + G\right) v_2$

KCL @ I:  $0 = -i_L + i_{C1} = -\frac{1}{\alpha L + \mu} (v_2 - v_1) + \alpha C_1 v_1$

2)  $\Rightarrow \left(\frac{1}{\alpha L + \mu} + \alpha C_1\right) v_1 = \frac{1}{\alpha L + \mu} v_2$

Dividing 2) (when  $v_1 \neq 0, v_2 \neq 0$ )

$$\frac{1 - g_m(\alpha L + \mu)}{1 + \alpha C_1(\alpha L + \mu)} = \frac{1 + (\alpha C_2 + G)(\alpha L + \mu)}{1}$$

$$\Rightarrow (1 - g_m(\alpha L + \mu)) = [1 + (\alpha C_2 + G)(\alpha L + \mu)][1 + \alpha C_1(\alpha L + \mu)]$$

$$\Rightarrow 1 - \zeta = [g_m + (\alpha C_2 + G) + \alpha C_1 + (\alpha C_2 + G)(\alpha L + \mu) + \alpha C_1(\alpha L + \mu)](\alpha L + \mu)$$

$$\Rightarrow 0 = (g_m + \alpha C_2 + G + \alpha C_1 + \alpha^3 C_2 L C_1 + \alpha^2 G L C_1 + \alpha C_2 \mu C_1 + \alpha G \mu C_1)(\alpha L + \mu)$$

$$\Rightarrow \alpha L(\alpha L + \mu) \neq 0$$

3)  $P(\alpha) = C_1 C_2 L \alpha^3 + [G L C_1 + C_1 C_2 \mu] \alpha^2 + [C_1 + C_2 + G \mu C_1] \alpha + (g_m + G)$

Let  $\alpha = j\omega_0 \Rightarrow$

4)  $\begin{cases} -j\omega_0^3 C_1 C_2 L + j\omega_0 [C_1 + C_2 + G \mu C_1] \end{cases} + \begin{cases} -\omega_0^2 [G L C_1 + C_1 C_2 \mu] + (g_m + G) \end{cases}$

as  $\omega_0 \neq 0$

5)  $\text{Im} = 0 = -\omega_0^2 C_1 C_2 L + [C_1 + C_2 + G \mu C_1]$

6)  $\text{Re} = 0 = -\omega_0^2 [G L C_1 + C_1 C_2 \mu] + (g_m + G)$

5\*)  $\omega_0^2 = \frac{C_1 + C_2 + G \mu C_1}{C_1 C_2 L}$

6\*)  $g_m + G = \omega_0^2 [G L C_1 + C_1 C_2 \mu] = \left[\frac{C_1 + C_2 + G \mu C_1}{C_1 C_2 L} + \frac{G \mu C_1}{C_2 L}\right] [G L C_1 + C_1 C_2 \mu]$

$$= \frac{(C_1 + C_2) G + (C_1 + C_2) \mu + \frac{C_1 G^2 \mu}{C_2} + G \mu^2 \frac{C_1}{L}}$$

If  $Q_L > 10$ , then  $\mu \rightarrow 0$

7a, b)  $\omega_0^2 \approx \frac{1}{L} \frac{C_1 C_2}{C_1 + C_2}$  ;  $g_m \approx \frac{C_1}{C_2} G$

(note if  $G=0 \Rightarrow$  check for LC resonator)

Note  $Q_L = \frac{\omega_0 L}{r}$  if  $> 10$  can ignore  $r$  and  $|j\omega_0 L + \mu| \approx |\omega_0 L|$

for BJT OTA

$g_m = \frac{I_T}{2V_T} \Rightarrow I_T = \frac{C_1}{C_2} \cdot G \cdot 2V_T$

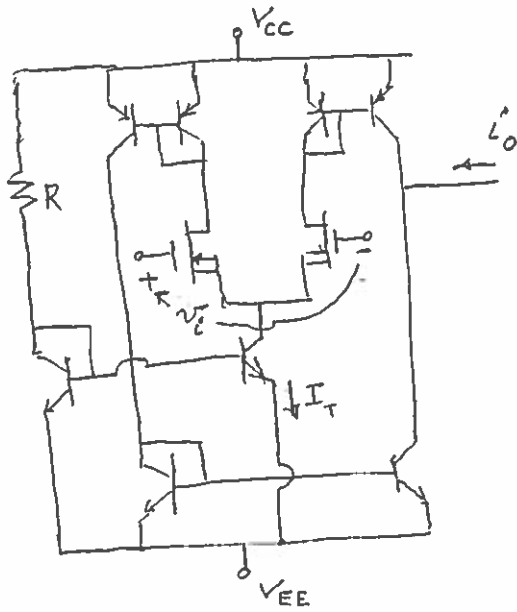
Example:  $L = 100 \text{ pF}$ ,  $f_0 = 1 \text{ MHz}$ ,  $C_1 = C_2 = \frac{2}{\omega_0^2 L} = \frac{2}{4\pi^2 \times 10^{12} \times 10^{-10}} = 0.0507 \times 10^{-9} = 507 \text{ pF}$

If  $I_T = 10 \text{ nA}$ ,  $G = 0.192 = 1/R$ ,  $R = 5.2 \text{ k}\Omega$ .  $\Rightarrow$  use MOS OTA

for MOS OTA

$g_m = \sqrt{2I_T \mu \beta}$ ,  $\beta = \frac{K P W}{2 L}$ ,  $\Rightarrow g_m = G \Rightarrow I_T = \frac{G^2}{2\beta}$ ; if  $\beta = 5 \times 10^{-4} \Rightarrow I_T = 10^3 G^2$

if  $R = 1/G = 1 \text{ k}\Omega$ ,  $I_T = 1 \text{ mA}$



$$i_o = \begin{cases} -I_T & ; \quad v_i \leq -\sqrt{\frac{I_T}{\frac{K_P W}{2} L}} \\ \sqrt{2I_T \frac{K_P W}{2} L} \cdot v_i \cdot \sqrt{1 - \frac{K_P W}{2} \frac{v_i^2}{2I_T}} & ; \quad 0 \leq |v_i| \leq \sqrt{\frac{I_T}{\frac{K_P W}{2} L}} \\ I_T & ; \quad \sqrt{\frac{I_T}{\frac{K_P W}{2} L}} \leq v_i \end{cases}$$

$$\Rightarrow g_m = \sqrt{2I_T \cdot \frac{K_P W}{2} L} \quad @ \text{ bias } (i_o = I_o = 0)$$