

#1. a) For Min  $V_{DS} = V_{GS} = -V_{SS} = 5V$

$$\begin{aligned} \Rightarrow I_D &= \frac{K P_n}{2} \frac{W}{L} (V_{GS} - V_{TO_n})^2 (1 + \lambda_n V_{DS}) \\ &= \frac{10^{-4}}{2} \cdot 1 (5 - 1)^2 (1 + 0.01 \times 5) = \frac{1}{2} \times 10^{-4} (16)(1.05) = 8.4 \times 10^{-4} \\ &= 0.84 \text{ mA} \end{aligned}$$

$$R_{in} = V_{DD}/I_D = \frac{5}{0.84} \times 10^3 = 5.95 \times 10^3 \approx 6 \text{ k}\Omega$$

b)  $R_{out} = \frac{5.95 \text{ k}\Omega}{2} = 3 \text{ k}\Omega$

$M_{out}$  is in saturation since  $V_{DS_{Mout}} > V_{DS_{Min}}$  &  $V_{GS_{Mout}} = V_{GS_{Min}}$   
and  $M_{in}$  is in saturation, so  $V_{DS_{Mout}} > V_{DS_{Min}} > V_{GS_{Min}} - V_{TO_n}$

$$\begin{aligned} \therefore I_{D_{Mout}} &= \frac{K P_n}{2} \frac{W}{L} (V_{GS_{Min}} - V_{TO_n})^2 (1 + \lambda_n V_{DS_{Mout}}) \\ &= I_{D_{Min}} \cdot \left( \frac{1 + \lambda_n V_{DS_{Mout}}}{1 + \lambda_n V_{DS_{Min}}} \right) = \frac{0.84 \times 10^{-3}}{(1.05)} \times (1 + \lambda_n V_{DS_{Mout}}) \\ &= 0.8 \times 10^{-3} (1 + 0.01 \times V_{DS_{Mout}}) \\ &= (V_{R_{out}}/R_{out}) = (10 - V_{DS_{Mout}})/3 \times 10^3 \end{aligned}$$

gives  $2.4 + 0.01 \times 24 V_{DS_{Mout}} = 10 - V_{DS_{Mout}}$

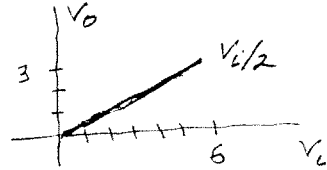
$$\Rightarrow 1.024 V_{DS_{Mout}} = 10 - 2.4 = 7.6 \Rightarrow V_{DS_{Mout}} = 7.42 \text{ V}$$

$$\begin{aligned} \Rightarrow I_{D_{Mout}} &= 0.8 \times 10^{-3} (1 + 0.0742) = 0.859 \times 10^{-3} \\ &\approx 0.86 \text{ mA} \end{aligned}$$

#2. a) as the transistors are completely complementary and

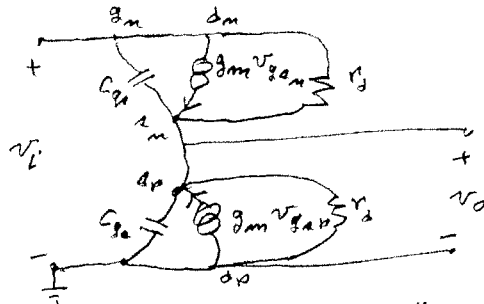
$$V_i = V_{GS_n} + V_{SG_p} = 2V_{GS_n} \Rightarrow V_{GS_n} = V_{SG_p} = V_i/2$$

$$\text{as } V_o = V_{SG_p} \Rightarrow V_o = V_i/2$$



This is not an inverter! It is a linear amplifier of gain  $1/2$  (even for  $V_i < 0$ )

b) For small signals



where

$$V_i = 3 \Rightarrow V_{GS_n} = V_{SG_p} = 3/2$$

$$V_o = \frac{V_i}{2} = \frac{3}{2} = V_{SG_p} = V_{DS_n} > V_{GS_n} - V_{Tn} > V_{SG_p} - |V_{Tp}|$$

$\Rightarrow M_{n3}$  &  $M_{p3}$  are in saturation

$$g_m = \frac{\partial |I_D|}{\partial |V_{GS}|} = \frac{\lambda |I_D|}{(|V_{GS}| - |V_{T0}|)} = 2 \frac{10^{-4}}{2} \times 1 \times \frac{(3/2 - 1)^2}{(3/2 - 1)} (1 + 0.01 \times 3/2) = 10^{-4} \times \frac{1}{2} \times (1.015)$$

$$= 50.75 \times 10^{-6} \text{ S}$$

$$g_d = \frac{\partial |I_D|}{\partial |V_{DS}|} = \frac{\lambda |I_D|}{(1 + \lambda |V_{DS}|)} = 0.01 \times \frac{10^{-4}}{2} \times 1 \times \left(\frac{3}{2} - 1\right)^2 = \frac{0.01}{8} \times 10^{-4} \approx \frac{10^{-6}}{8}$$

$$\Rightarrow r_d = 8 \times 10^6 \Omega$$

c) as the two portions of the circuit are identical  $v_i$  splits in half by voltage division. so

$$\frac{v_o}{v_i} = \frac{1}{2}$$

There are no poles or zeros; this is an "entire" function