

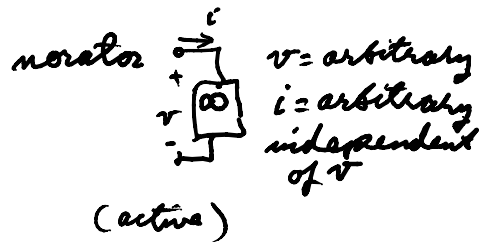
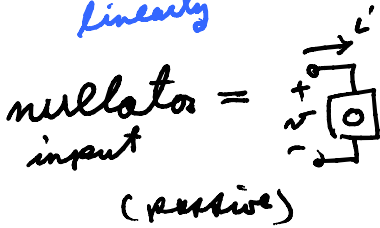
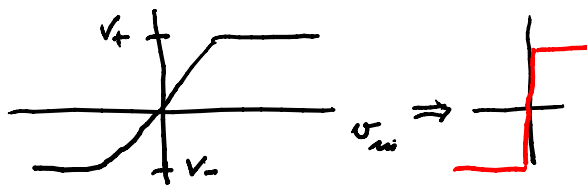
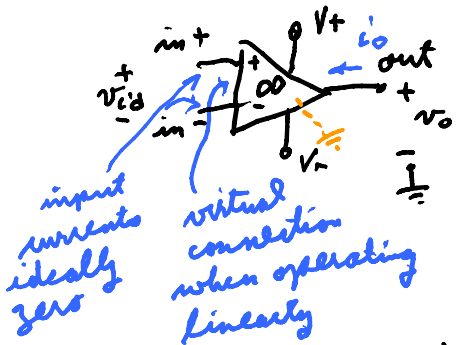
next time  
biasing

BJT = P.437, fig 5.44  
MOS = P.282, fig 4.30

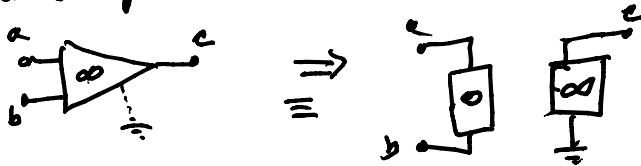
EE 303  
02/16/10

come with a base  
paper next period

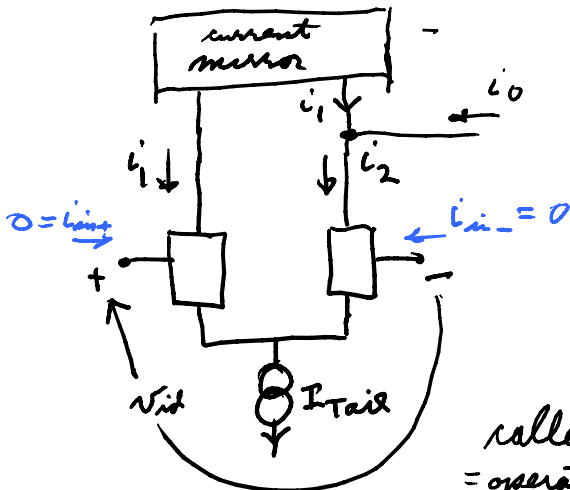
op-amps 741 ( $\Rightarrow$  1548, 2 in a package)  
P.894



for small signals

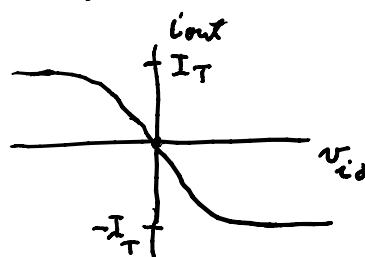


We make these with differential pairs  
and current sources & mirrors



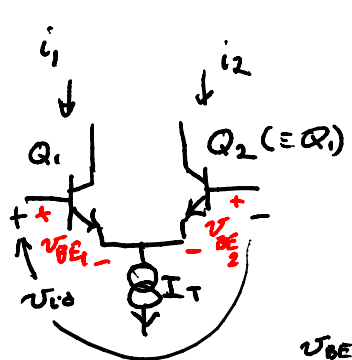
$$I_{\text{tail}} = i_1 + i_2 = I_T$$

$$i_{\text{out}} = i_2 - i_1$$



called OTA  
= operational transconductance  
amplifier

for BJT, p. 710 ; MOS, p. 721 ; OTA (MOS) = p. 728



law for forward active region

$$i_c = \alpha I_s e^{v_{BE}/V_T}$$

$$v_{id} = v_{BE1} - v_{BE2}$$

$$I_T = i_1 + i_2 = \alpha I_s (e^{v_{BE1}/V_T} + e^{v_{BE2}/V_T})$$

$$= \alpha I_s e^{v_{BE2}/V_T} [e^{(v_{BE1} - v_{BE2})/V_T} + 1]$$

$$i_o = i_2 - i_1 = \alpha I_s (e^{v_{BE2}/V_T} - e^{v_{BE1}/V_T})$$

$$= \alpha I_s e^{v_{BE2}/V_T} [1 - e^{(v_{BE1} - v_{BE2})/V_T}]$$

$$\frac{i_o}{I_T} = \frac{[1 - e^{v_{id}/V_T}]}{[1 + e^{v_{id}/V_T}]} = \frac{e^{v_{id}/2V_T} [e^{-v_{id}/2V_T} - e^{v_{id}/2V_T}]}{e^{v_{id}/2V_T} [e^{-v_{id}/2V_T} + e^{v_{id}/2V_T}]}$$

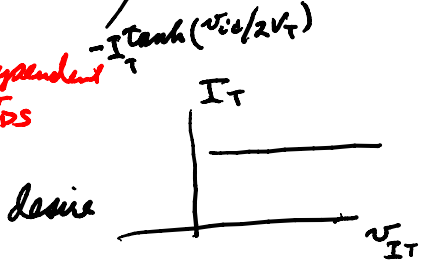
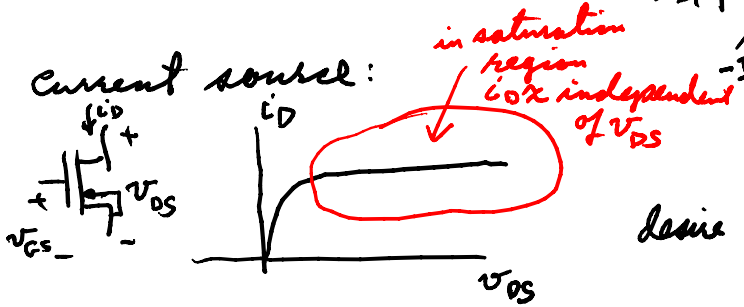
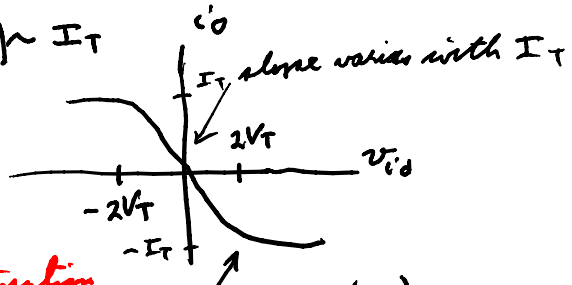
$$= -\frac{\sinh(v_{id}/2V_T)}{\cosh(v_{id}/2V_T)}$$

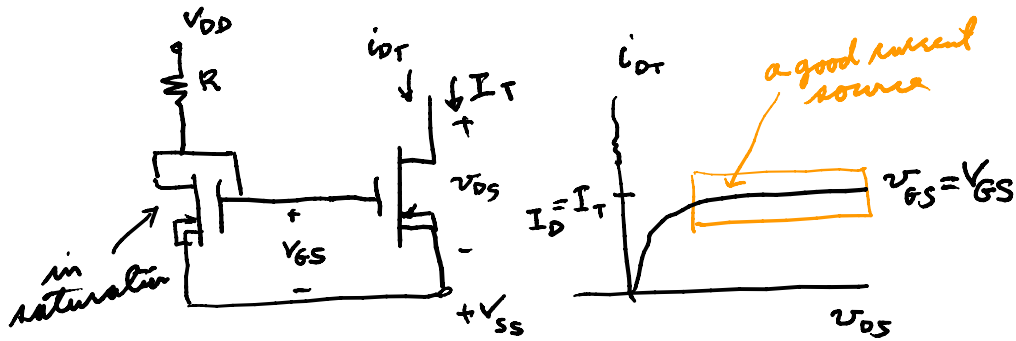
$$i_o = -I_T \tanh\left(\frac{v_{id}}{2V_T}\right)$$

$$V_T = 0.026 \text{ V}$$

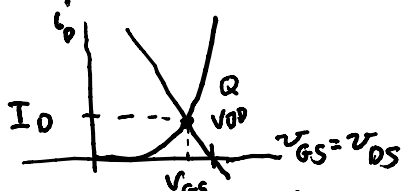
$$2V_T = 0.052 \text{ V}$$

at  $v_{id}$  near 52 mV  $|i_o| \sim I_T$



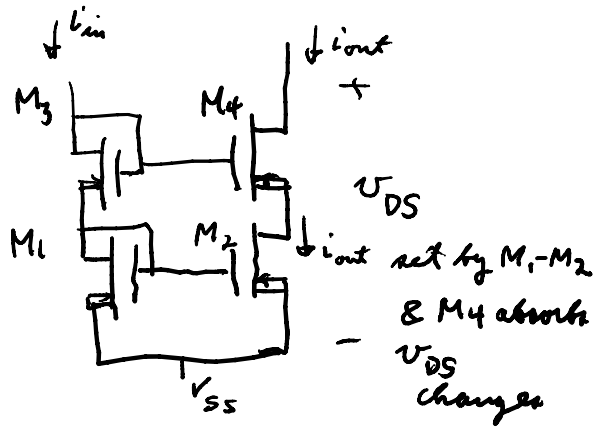


$$v_{DS} - V_{T0} = v_{GS} - V_{T0} < v_{DS}$$

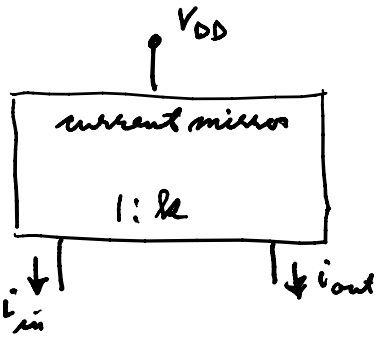


$$i_D = \frac{K_P}{2} \frac{W}{L} (v_{GS} - V_{T0})^2$$

To make with less slope (larger  $V_A = \text{Early voltage} = 1/\lambda$  for MOS)  
use a cascode, p. 892

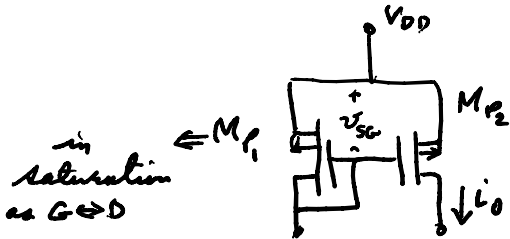


$$i_{out} = k i_{in}$$



$$i_1 = \frac{K_P W_1}{2 L_1} (v_{SG} - |V_{T0}|_p)^2$$

$$i_0 = \frac{K_P W_0}{2 L_0} (v_{SG} - |V_{T0}|_p)^2 \text{ if } i_{in} \text{ in saturation}$$

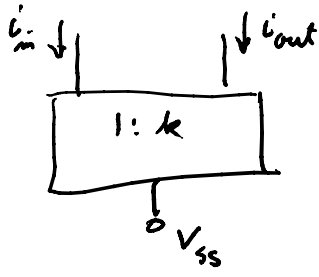


in saturation as  $G \rightarrow D$

given  $i_1$  from diff bk.

$$\frac{i_0}{i_1} = \frac{W_0/L_0}{W_1/L_1} \Rightarrow k = \frac{W_0/L_0}{W_1/L_1}$$

gives a current mirror source



current mirror  
sink

