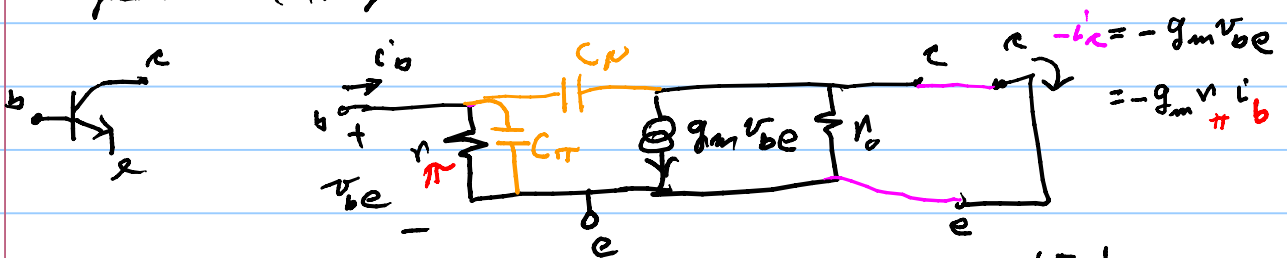


pp. $f_T \Rightarrow$ p. 489 & BJT small signal
 MOS small signal p. 591
 current mirrors p. 563 & 649
 differential pairs p. 704, 710 (BJT)
 p. 721 (MOS)

EE 303H
 02/17/09

f_T = transition frequency for BJT
 frequency at which $|i_c/i_b| = 1$; i.e. β drops to 1
 for small signals



$$\frac{i_c}{i_b} = \beta = g_m r_{\pi}$$

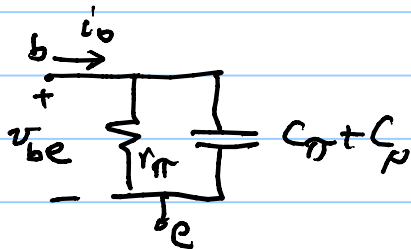
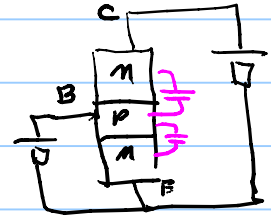
$$g_m = \frac{|I_C|}{V_T}$$

C_{π} on p. 486

$$C_{\pi} = C_{de} + C_{je}$$

$$\frac{C_{je0}}{(1 - V_{be}/V_{be0})^m}$$

$$V_{be0} \approx 0.75V$$



$$i_b = y_{be}(\alpha) \cdot v_{be}$$

$$y_{be} = g_{\pi} + \alpha(C_{\pi} + C_{\mu})$$

$$-i_c = -g_m v_{be} = -g_m \left(\frac{i_b}{y_{be}(\alpha)} \right) \Rightarrow \frac{i_c}{i_b} = \frac{g_m}{g_{\pi} + \alpha(C_{\pi} + C_{\mu})}$$

$$\beta(\alpha) = \frac{g_m r_{\pi}}{1 + \alpha(C_{\pi} + C_{\mu})/g_{\pi}}$$

$$= \frac{\beta(0)}{1 + \alpha(C_{\pi} + C_{\mu})/r_{\pi}}$$

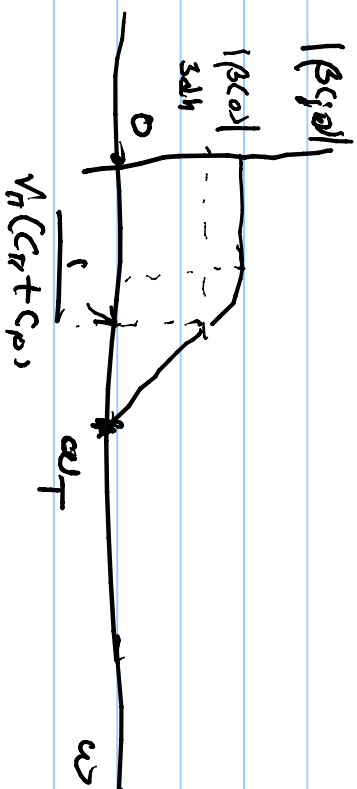
$$f_T \Rightarrow \left| \frac{i\omega C_j \omega}{i\omega} \right| = 1 \text{ i.e. when } |\beta(j\omega)| = 1$$

$$|\beta(\omega)| = \left| \frac{\beta_0}{1 + j\omega(C_T + C_P)R_T} \right| = \frac{\beta_0}{\sqrt{1 + \omega^2(C_T + C_P)^2 R_T^2}}$$

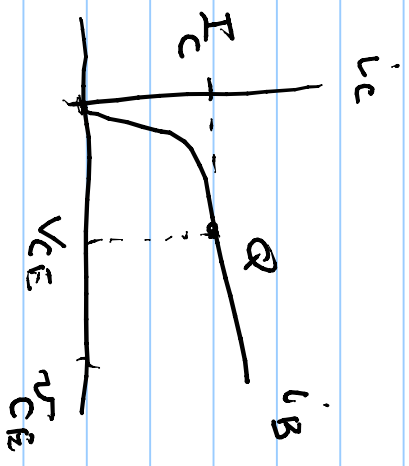
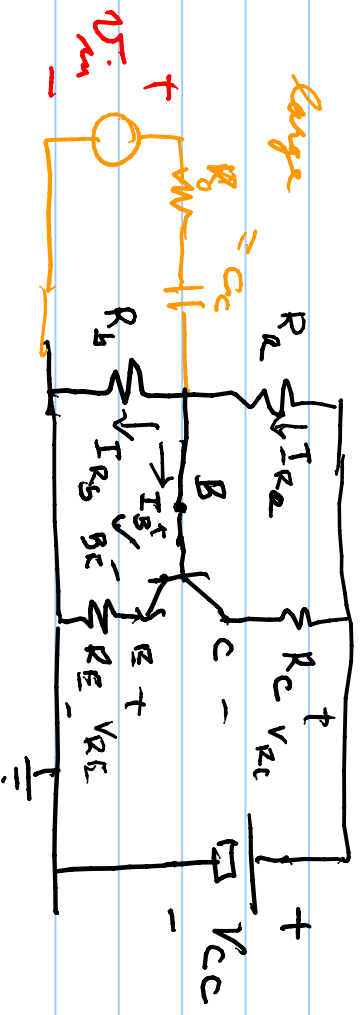
$$\approx \frac{\beta_0}{\omega(C_T + C_P)R_T} \text{ when } \omega \text{ large}$$

$$= 1 \Rightarrow \omega_T = \frac{\beta_0}{(C_T + C_P)R_T} = 2\pi f_T$$

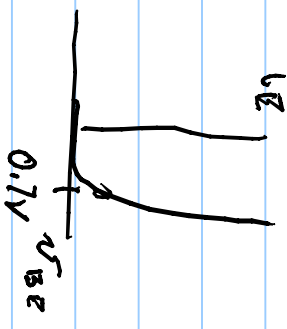
$$f_T = \frac{\beta_0}{(C_T + C_P)R_T}$$



Biasing of BJT's for small signal amp



Let $I_C = 2\text{mA}$, $\beta(D) = 100$; $I_B = \frac{I_C}{\beta} = \frac{2 \times 10^{-3}}{100} = 2 \times 10^{-5} = 20 \times 10^{-6} = 20\mu\text{A}$



use $V_{BE} \approx 0.7\text{V}$ also

$-I_E = \frac{I_C}{\alpha}$; $\alpha = \frac{\beta}{1+\beta} = \frac{100}{101}$

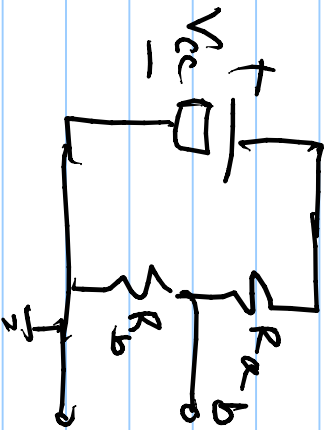
$V_{RE} = R_E \times \frac{I_C}{\alpha}$

Choose R_C & R_B as $1\text{ k}\Omega$

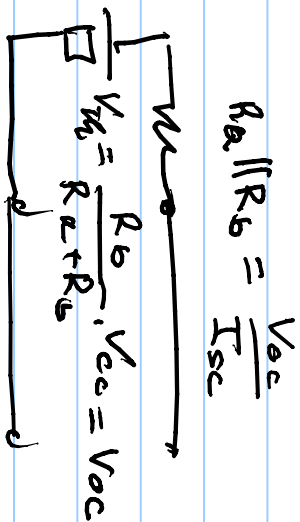
$$V_{RC} \approx R_C I_C = 10^3 \times 2 \times 10^{-3} = 2\text{ V}$$

$$V_{RB} \approx 2\text{ V}$$

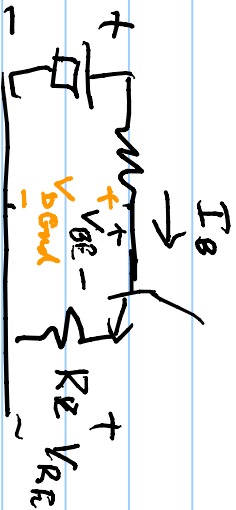
Make a Thevenin equivalent for base to ground looking left



\Rightarrow



$$R_{th} \parallel R_b = \frac{V_{oc}}{I_{sc}}$$



$$V_{BC} = V_{BE} + V_{RE} \approx 2.7\text{ V}$$

$$I_B = 20 \mu A$$

$$\frac{R_b}{R_a + R_b} V_{CC} = \frac{R_a R_b}{R_a + R_b} \cdot I_B + V_{BE_{on}}$$
$$\frac{1}{1 + \left(\frac{R_a}{R_b}\right)} V_{CC} = \frac{1}{\frac{1}{R_b} + \frac{1}{R_a}} \cdot 20 \times 10^{-6} + 2.7$$

Have 3 unknowns & 1 eq.

V_{CC} is normally a rather easy 9.0V.

still have 2 others: R_a & R_b can choose one

where one large R_a say of 10 MEG ohms

& then solve for R_b (can solve as linear eq. but would get a negative value).

can have the computer solve subject to constraints.

Note for diode $i_D = I_S (e^{v_D/kT/q} - 1)$

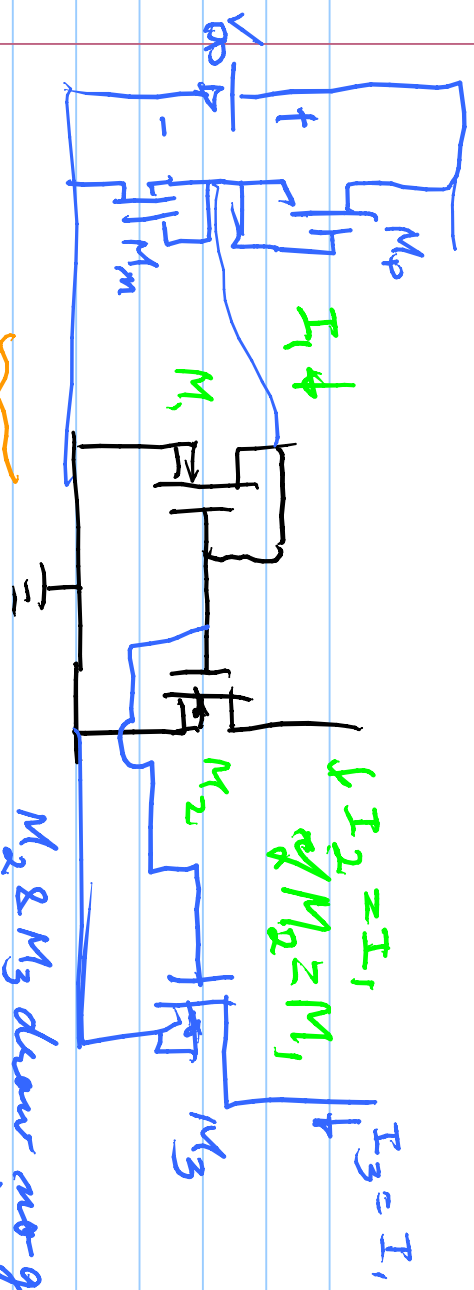
as temperature, T , increases i_D decreases
and becomes negative

R_E is present to stabilize the circuit w.r.t increases
in T_C or T_B

if take signal out of R_E the circuit is an
emitter follower as v_{RE} follows v_i .

Also $|v_{RE}/v_i| < 1$ but isolates v_i from loads.

current mirrors:



$I_2 = I_1$
 $M_2 \approx M_1$
 $I_3 = I_1$
 M_2 & M_3 draw no gate current (for bias)
 no saturation
 as $V_{DS} = V_{GS} > V_{GS} - V_{TO}$ if $V_{TO} > 0$

