

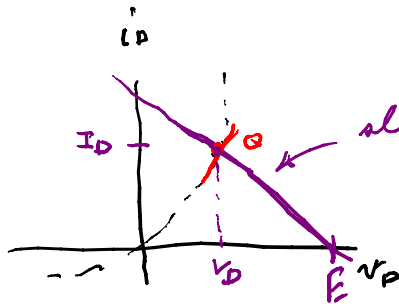
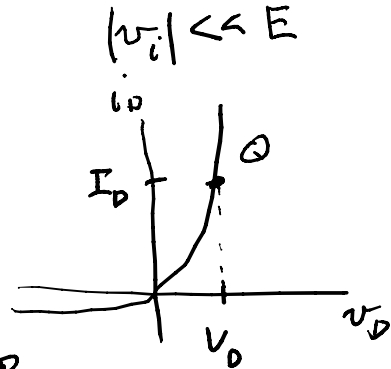
$$I_D = I_S (e^{V_D/V_T} - 1)$$

$$V_T \ln \left(\frac{I_D}{I_S} + 1 \right) = V_D$$

$$V_T = \frac{kT}{q} \approx 26 \text{ mV} @ \text{room T}$$

I_S a constant for a given diode

$|q| = \text{electronic charge}$

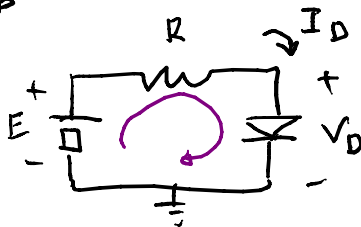


slope = $-\frac{1}{R}$

$$i_{cap} = C \frac{dv_{cap}}{dt}$$

zero for bias

for bias



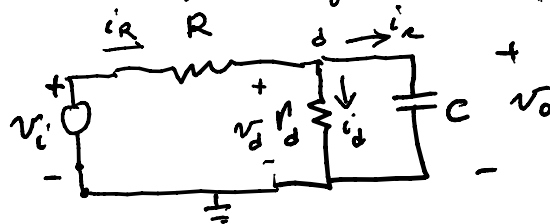
$$E = R I_D + V_D$$

$$I_D = \frac{E - V_D}{R}$$

$$R = \frac{E - V_D}{I_D}$$

$$R = - \frac{dV_D}{dI_D}$$

for signal (small signal) for v_i & for change



$$i_D = I_D + \frac{\partial i_D}{\partial v_D} (v_o - V_D) + \dots \Rightarrow i_d = g_d \cdot v_d$$

$$i_D - I_D = i_d$$

$$g_d = \frac{\partial i_D}{\partial v_D} \approx \frac{I_D}{V_T}$$

$$v_d = \frac{1}{g_d}$$

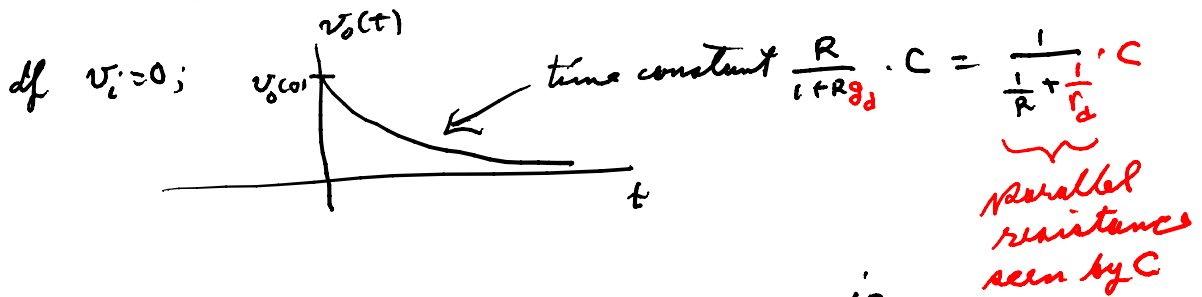
$$\begin{aligned}
 v_i &= R i_R + v_o \\
 &= R(i_d + i_c) + v_o \\
 &= R g_d v_d + R i_c + v_o \\
 &= R g_d v_o + RC \frac{dv_o}{dt} + v_o \\
 &= (1 + R g_d) v_o + RC \frac{dv_o}{dt}
 \end{aligned}$$

KVL $v_o = v_d$
 KCL $i_R = i_d + i_c$

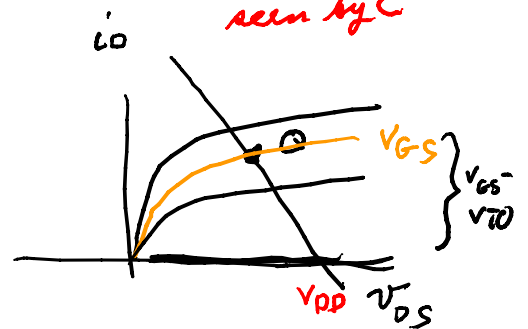
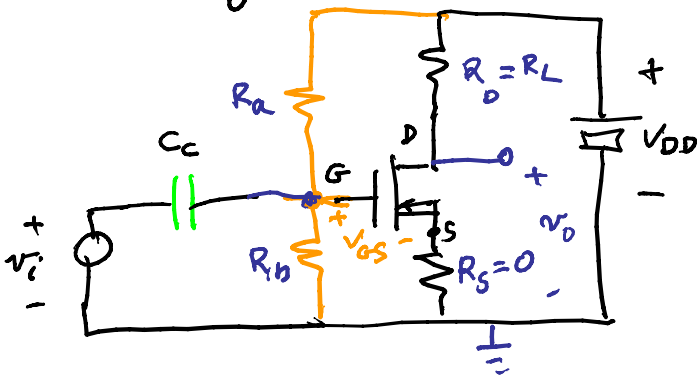
$v_o(0)$ given

$$V_i(s) = (1 + R g_d) V_o(s) + RC s V_o(s)$$

$$\frac{V_o(s)}{V_i(s)} = \frac{1}{RC s + (1 + R g_d)} = \frac{1/RC}{s + \frac{(1 + R g_d)}{RC}}, \quad s = \sigma + j\omega$$



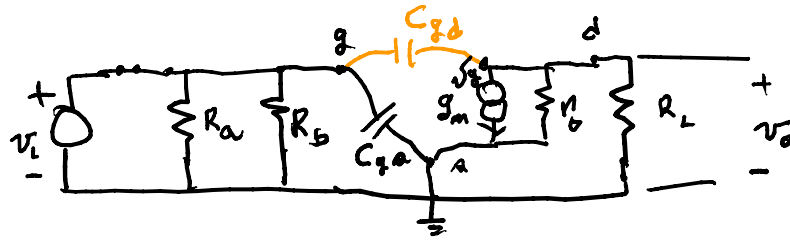
MOS amplifiers



$$V_{GS} = \frac{R_b}{R_a + R_b} V_{DD} \text{ if } R_S = 0$$

$Z_c(s) = \frac{1}{s C_c}$ if $s = j\omega \rightarrow |Z_c(j\omega)| = \frac{1}{\omega C_c}$ choose C_c large
 to allow signal frequencies to pass through

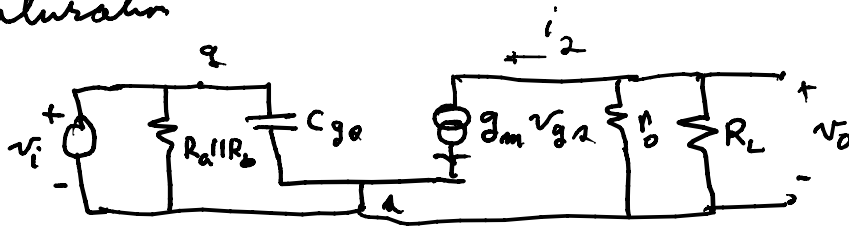
Use small signal equivalent circuit



If M is in saturation $C_{gd} = 0$, $C_{gs} = \frac{2}{3} C_{ox} \times W \times L$

see p. 321

If in saturation



$$v_o = -(r_o \parallel R_L) \cdot i_2 = - \frac{R_L \cdot r_o}{R_L + r_o} \cdot g_m \cdot v_i$$

$$\frac{v_o}{v_i} = -g_m \cdot R_{L \text{ effective}} \quad I_D = \frac{K_P W}{2L} (V_{GS} - V_{TO})^2 (1 + \lambda V_{DS})$$

$$g_m = \left. \frac{\partial I_D}{\partial V_{GS}} \right|_Q = \frac{2 I_D}{(V_{GS} - V_{TO})}$$

$\Sigma_x: I_D = 2 \text{ mA}$
 $V_{GS} = 2.9, V_{TO} = 0.9 \text{ V}$
 = mutual conductance
 = transconductance

If $R_L = 10 \text{ k}\Omega$ then $\frac{v_o}{v_i} = -2 \times 10^{-3} \times 10^3 \times 10 = -20$

Effect of $\lambda = 15 \times 10^{-3}$:

$$g_o = \left. \frac{\partial I_D}{\partial V_{DS}} \right|_Q = \lambda \left(\frac{K_P W}{2L} (V_{GS} - V_{TO})^2 \right)$$

$$= \frac{\lambda I_D}{1 + \lambda V_{DS}}$$

$$= 15 \times 10^{-3} \times \frac{2 \times 10^{-3}}{1 + 15 \times 10^{-3} \cdot V_{DS}} \approx \frac{15 \times 2 \times 10^{-6}}{1}$$

$r_o \approx 30.3 \text{ k}\Omega$

$$= g_o = 30 \mu\text{S}; r_o = \frac{10^6}{30} = 10^4 \times \frac{100}{30}$$

To find V_{DS} : $I_D = 2 \times 10^{-3} = \frac{K_P W}{2 L} (\underbrace{2.9}_{V_{GS}} - \underbrace{0.9}_{V_{TO}})^2 (1 + 15 \times 10^{-3} V_{DS})$

$\approx \frac{K_P W}{2 L} = \frac{2 \times 10^{-3}}{2^2} = \frac{1}{2} \times 10^{-3}$ if $\lambda = 0$

$\therefore V_0 \parallel R_L \neq R_L$ but $R_{L_{eff}} = \frac{r_o R_L}{r_o + R_L} = \frac{30.3 \times 10^3 \times 10 \times 10^3}{(30.3 + 10) \times 10^3}$

$= \frac{303 \times 10^3}{40.3} \approx 8 \text{ k}\Omega$

\Rightarrow gain decreases due to the Early effect

gain = $\frac{V_o}{V_i} = -20$ when no Early effect

$\Rightarrow -2 \times 10^{-3} \times 8 \times 10^3 = -16$ when an Early effect.