

for signal analysis:

$i_D = \text{total}$

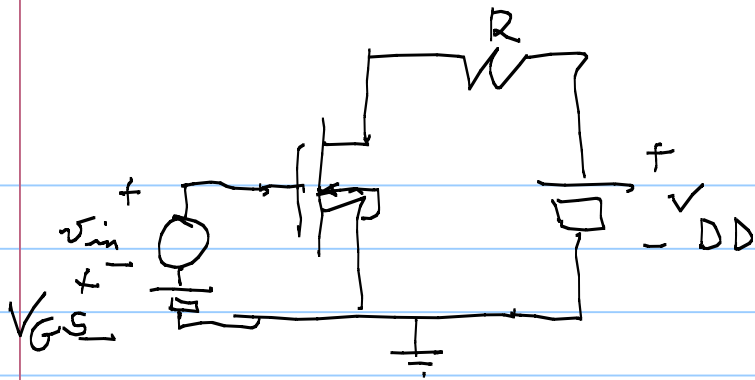
$I_D = \text{bias (DC state at Q point)}$

$i_d = \text{signal}$

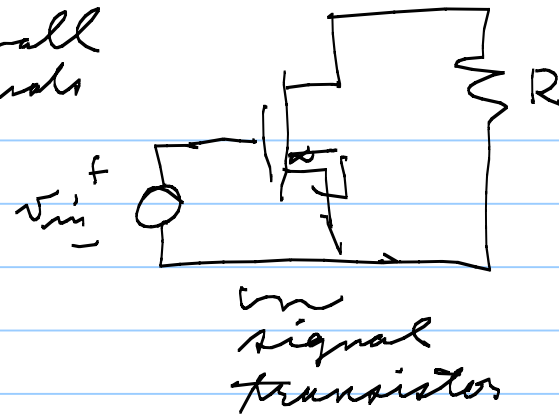
$i_D = I_D + i_d$

$v_{DS} = V_{DS} + v_{ds}$

i_d vs v_{ds} signal behavior



for small signals \Rightarrow



$$i_D(v_{GS}, v_{DS}) = I_D + \frac{\partial I_D}{\partial v_{GS}} \bigg|_{v_{GS}, v_{DS}} (v_{GS} - V_{GS}) + \frac{\partial I_D}{\partial v_{DS}} \bigg|_{v_{GS}, v_{DS}} (v_{DS} - V_{DS}) + \dots$$

signal

Q pt values

if $|v_{GS} - V_{GS}|, |v_{DS} - V_{DS}|$ are small we can ignore

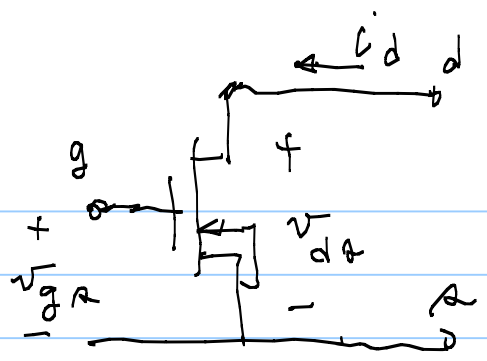
$$i_D = I_D + i_d$$

$$i_d = \frac{\partial I_D}{\partial v_{GS}} \bigg|_{Q} v_{gs} + \frac{\partial I_D}{\partial v_{DS}} \bigg|_{Q} v_{ds}$$

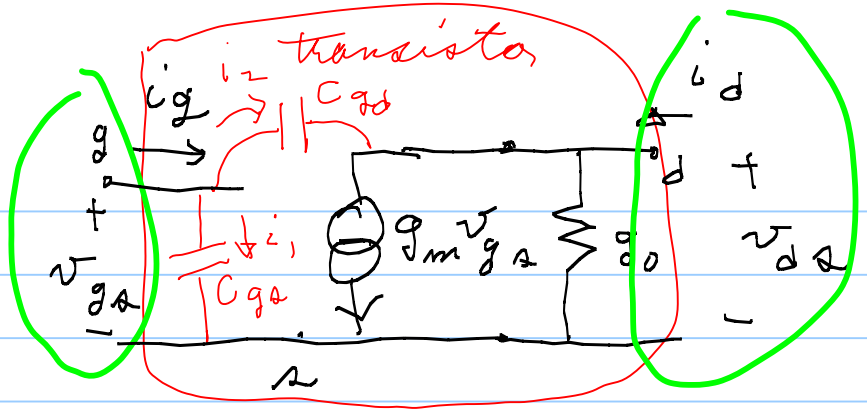
$$= g_m v_{gs} + g_o v_{ds}$$

$g_m =$ mutual conductance

$g_o =$ output conductance



⇒



⊙ = 2-port equivalent circuit

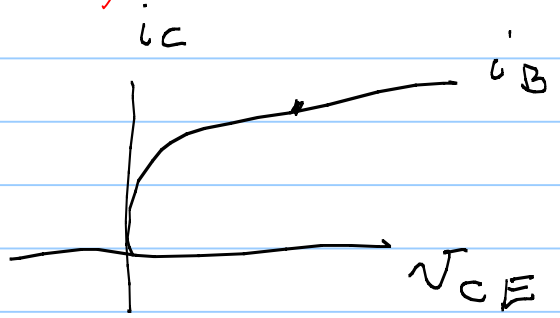
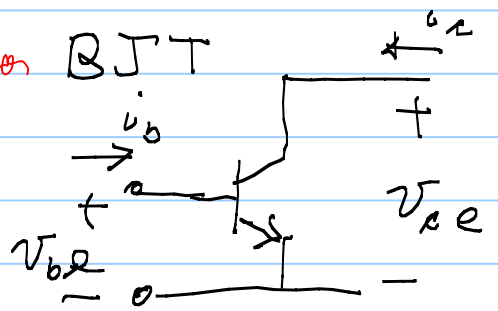
has an admittance

$$\begin{bmatrix} i_g \\ i_d \end{bmatrix} = \begin{bmatrix} 0 \\ g_m \\ g_o \end{bmatrix} \begin{bmatrix} v_{gs} \\ v_{ds} \end{bmatrix} \Rightarrow \begin{bmatrix} sC_{gs} + sC_{gd} & -sC_{gd} \\ -sC_{gd} + g_m & sC_{gd} + g_o \end{bmatrix} = Y(s)$$

$$i_g = sC_{gs} v_{gs} + sC_{gd} (v_{gs} - v_{ds})$$

$s = d/dt$ or Laplace transform variable

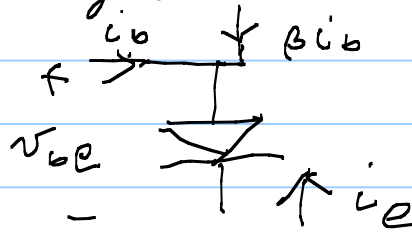
for BJT



$$i_c = I + i_c' ; \quad i_c' = \underbrace{\frac{\partial i_c}{\partial v_{CE}}}_{Q} v_{ce} + \underbrace{\frac{\partial i_c}{\partial i_B}}_{Q} i_b$$

$Q \quad \beta \cdot i_b$

note at the base we have a forward biased diode usually for small signals



$$-i_E = I_S (e^{v_{BE}/V_T} - 1)$$

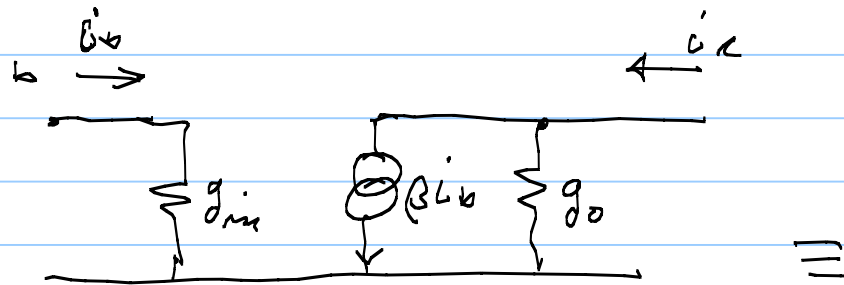
$$-i_E' = -I_E + \frac{\partial(-i_E)}{\partial v_{BE}} (v_{BE} - V_{BE}) ; \quad \frac{\partial(-i_E)}{\partial v_{BE}} = I_S \cdot \frac{1}{V_T} \cdot e^{v_{BE}/V_T}$$

$$\text{at } Q \text{ point } -i_E' = -I_E \approx I_S e^{v_{BE}/V_T} \gg I_S \approx \frac{-I_E}{V_T}$$

$$I_C + I_B + I_E = 0 \Rightarrow I_E = -I_C - I_B \Rightarrow I_E = -I_C - \frac{I_C}{\beta} = \frac{(\beta+1)(-I_C)}{\beta}$$

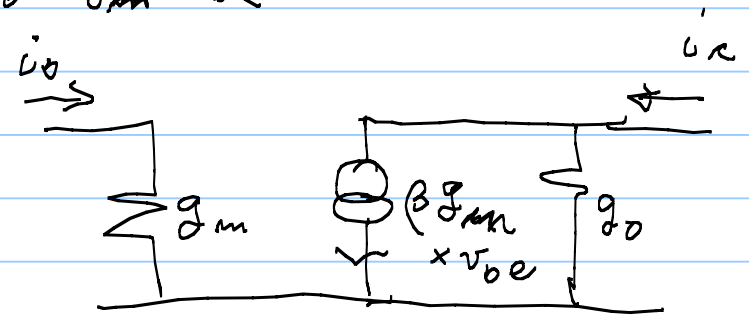
$$-i_e = i_b + \beta i_b \Rightarrow -i_e = (\beta + 1) i_b \Rightarrow -i_e = (\beta + 1) i_b = \left(\frac{-I_E}{V_T} \right) v_{be}$$

$$i_b = \frac{-I_E}{(\beta + 1) V_T}, \quad v_{be} = \frac{I_C}{\beta V_T}, \quad v_{be} = g_{in} \cdot v_{be}$$

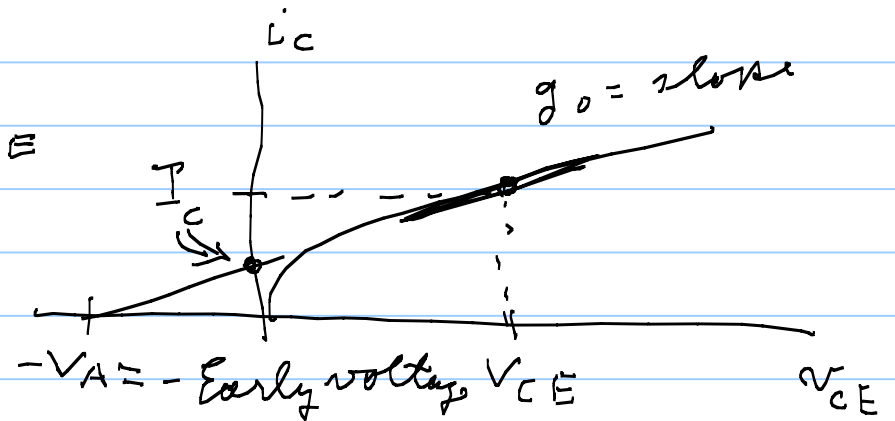


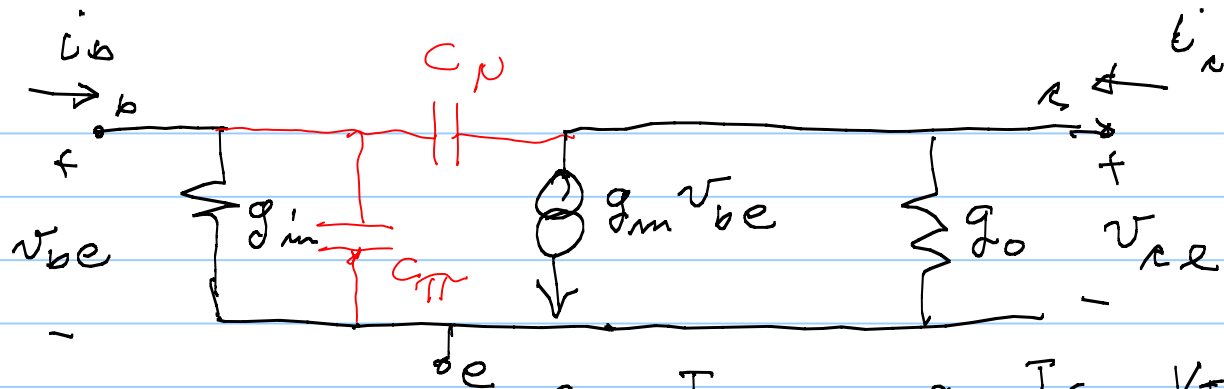
$$g_{in} = \frac{I_C}{\beta V_T} = \frac{1}{\beta} g_m$$

$$i_b = g_{in} v_{be}$$



$$\beta g_{in} = \frac{I_C}{V_T} = g_m; \quad g_o = \frac{\partial i_c}{\partial v_{CE}} \approx \frac{I_C}{V_A}$$





$$g_{\pi} \approx g_{in} = \frac{g_m}{\beta}$$

$$g_m = \frac{I_c}{V_T}$$

$$g_o = \frac{I_c}{V_A} = \frac{V_T}{V_A} \cdot g_m$$

π equivalent
 a Y matrix
 one
 intrinsic
 transistor

The hybrid- π

