

adjoint for sensitivity  $S_T = \frac{\partial}{\partial T} \frac{d^T}{dY}$

$$S_T = \frac{\partial}{\partial T} \frac{d^T}{dY} \quad Y^a$$

$X = a$  parameter;  $T$  = transfer function

$$\begin{aligned} \sigma^T i^* &= \langle v, i^* \rangle = v^T Y v \approx (v^T Y v)^T = v^T Y^T v \\ &\stackrel{\text{scalar}}{=} \langle v^a, i^{*a} \rangle = Y^T = Y^a \\ &\stackrel{\text{product}}{=} \langle v^a, Y^a v^a \rangle \end{aligned}$$

assume adjoint circuit has the same graph as original circuit



$$\begin{aligned} i_b^T v_b^a &= i_b^a v_b = 0 \Rightarrow [i_1^a v_1^a + i_2^a v_2^a - i_1^a v_1 - i_2^a v_2] + i_{\text{int}}^a V_{\text{int}} - i_{\text{int}}^a V_{\text{ext}} = 0 \\ i_b^T v_b^a &= 0 \quad b = \text{branch} \\ v_b^a i_b &= 0 \quad i_b^a v_b = 0 \end{aligned}$$

minus due to external branch polarities

$$\therefore i_b^T v_b^a \rightarrow i_b^a v_b = 0 \Rightarrow [i_1^a v_1^a + i_2^a v_2^a - i_1^a v_1 - i_2^a v_2]^T + i_{\text{int}}^a V_{\text{int}} - i_{\text{int}}^a V_{\text{ext}} = 0$$

These  $v_i^a, i^a$  = transfer function of interest,  $x$  = parameter {exp. C, g, temp, anything that varies}

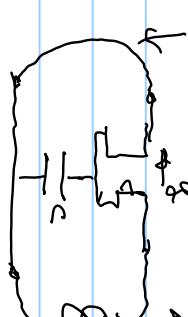
assume  $Y$  changes with  $x$  but  $Y^a$  does not

$$\begin{aligned} i^T v^a &= v^T Y^a v \quad \text{use } Y \text{ for internal} \\ \text{int mat} &= v^{\text{int}} \cdot Y^{\text{int}} \quad \text{branch by branch} \\ i^{*T} v^a &= v^{*\text{int}} \cdot Y^{*\text{int}} v^{\text{int}} \quad Y^{\text{int}} \end{aligned}$$

fixed applied  
fixed voltage (for  $i_1$  linear)  
fixed voltage  $v_1$  or current  
choose  $i_2 \equiv 0$  w/ open  
circuit



$\Rightarrow$  adjoint



$\Leftrightarrow$  choose  $\alpha = -1$

$v_1^{\alpha=0}$   $\Leftrightarrow$  desired term  $\alpha$  has  $dV_1/dx = \frac{dV_2/v_1}{R_1}$

$$\text{above } \rightarrow \frac{d}{dx} = 0 \Rightarrow -\left[ \frac{d^i_1}{dx} \cdot v_1^\alpha + i_1 \frac{dv_1^\alpha}{dx} + d^i_2 v_2 + i_2 \frac{dv_2}{dx} - d^i_1 v_1 - i_1 \frac{dv_1}{dx} - d^i_2 v_2 - i_2 \frac{dv_2}{dx} \right]$$

$$+ d^{\text{want}} \gamma^T v_{\text{out}} + v_{\text{out}}^T \frac{dy^T v^{\alpha}}{dx} + v_{\text{out}}^T d^{\text{want}} - d^{\text{want}} \gamma^T v_{\text{out}} - v_{\text{out}}^T \frac{dy^T v^{\alpha}}{dx} - v_{\text{out}}^T d^{\text{want}}$$

$$0 \equiv \frac{d^i_1}{dx} \cdot 0 + i_1 \cdot 0 + 0 \cdot v_1^\alpha + 0 \cdot \frac{dv_1}{dx} - 0 \cdot v_2 - i_2 \cdot \frac{dv_2}{dx}$$

$\approx$  determined  
distribution

$$+ d^{\text{want}} \gamma^T v_{\text{out}} + v_{\text{out}}^T \frac{dy^T v^{\alpha}}{dx} + v_{\text{out}}^T d^{\text{want}}$$

desired

$$0 \cdot \gamma^T v_{\text{out}} = v_{\text{out}}^T \cdot 0 \cdot \gamma^T v_{\text{out}} = v_{\text{out}}^T \gamma^T$$

$\Downarrow$   $\frac{dy^T v^{\alpha}}{dx} \approx$  see the  
-  $(d^{\text{want}} \gamma^T v^{\alpha})$  transpose of  
a matrix is  
the same as  
the original

cancel  $\gamma^T v^{\alpha} + \gamma^T = 0$  matrix  $\Rightarrow$  choose  $\gamma^{\alpha} = \gamma^T$

fixed circuit no changes with  $\alpha$

$$\frac{d^i_1}{dx} = 0$$

$$\frac{d^i_2}{dx} = 0$$

$$0 = V_{int} \frac{dY^T}{dX} \cdot V_{int} + i_{2a} \cdot \frac{dV_a}{dY} \implies \frac{dV_{int}}{dX} = \frac{-1}{i_{2a}} \cdot V_{int} \cdot \frac{dY}{dX} \cdot V_{int}$$

choose  $i_2^a \approx -1$  & transpose product

$$Y = \begin{bmatrix} 0 & g & 0 \\ -g & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad Y^T = \begin{bmatrix} 0 & -g & 0 \\ g & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}; \quad \frac{dY}{dC} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad \frac{dY}{dg} = \begin{bmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$(V) \quad i_1 \rightarrow i_2 = -g v_{13} = 0 \Rightarrow v_{13} = 0$$

$$v_1 = 1 \quad i_1 = g v_{23} \approx ac v_3 \Rightarrow v_{23} = \frac{ac}{g} v_3 \Rightarrow v_{23} = \frac{ac}{g}$$

$$\begin{bmatrix} 0 \\ ac/g \\ 1 \end{bmatrix}$$

$$0 = -v_1 + v_{13} + v_3 \Rightarrow 0 = -1 + 0 + v_3 \Rightarrow v_3 = 1$$

$$v_1 = 1$$

$$i_1^a = -1 \quad v_{13}^a = -v_3^a \quad i_1 = -g v_{23}^a$$

$$i_2^a = g v_{23}^a = -g v_3^a = 0$$

$$\begin{cases} i_1^a + i_{2a} = i_c^a = ac v_3^a \\ i_2^a = -g v_3^a \end{cases} \quad -g v_{23}^a = (g + ac)v_3^a \Rightarrow v_{23}^a = -\frac{g+ac}{g} \cdot v_3^a$$

$$-g v_{23}^a$$

$$-g v_3^a$$

$$\frac{d\sigma_2/\sigma}{dc} = \left[ 0 \quad 1 \right] \cdot \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} -1/q \\ g \\ g/(g+ac) \end{bmatrix} = \frac{d\sigma_2/\sigma}{dq} = \begin{bmatrix} -1 \\ g \\ g/(g+ac) \end{bmatrix} \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & ac/g \end{bmatrix} = \frac{ac}{g^2}$$

$$Y'' = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 & 0 & 1 \\ 0 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix}$$