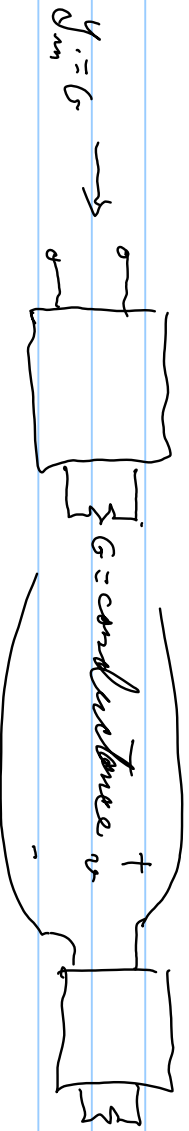


Constant R



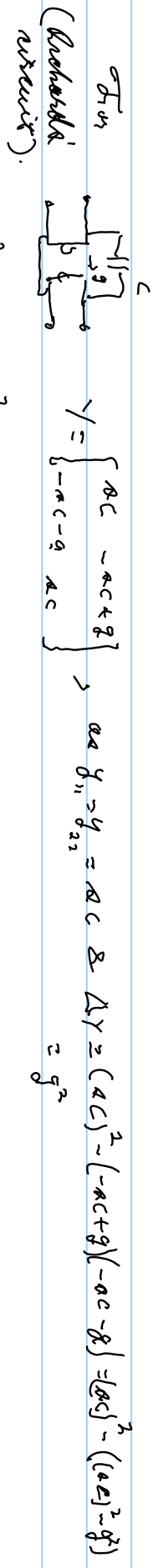
$$y_m = y_{R1} - y_{R2} \cdot \frac{y_{R2} \cdot y_{R1}}{y_{R2} + y_{R1}} \cdot y_{R2} \approx \frac{y_{R1} y_{R2} + y_{R1} y_{R1} - y_{R2} y_{R1}}{y_{R2} + y_{R1}} = \frac{\Delta Y + y_{R1} y_{R1}}{y_{R2} + y_{R1}}$$

for Constant R:  $y_L \approx G = y_{R1}$

$$G = \frac{\Delta Y + y_{R1} G}{y_{R2} + G} \Rightarrow y_{R2} G + G^2 = \Delta Y + y_{R1} G$$

If  $y_{R1} = y_{R2}$  then  $y_{R1} G = y_{R2} G$

$$G^2 = \Delta Y$$



$\therefore$  as  $G^2 = \Delta Y = g^2$  then  $\pm g = G \Rightarrow G = |g| > 0$

∴ Look @  $\frac{V_2}{V_1}(s)$  for const. R

$$\frac{V_2}{V_1} = \frac{-g_{21}}{g_{22} + G}$$

for the Richards' circuit

$$\frac{V_2}{V_1} = \frac{AC + g}{AC + G}, \text{ so if } g = -G$$

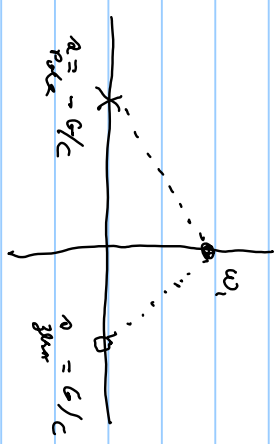
$$\text{Then } \frac{V_2}{V_1} = \frac{AC - G}{AC + G} = \frac{A - G/C}{A + G/C}$$

∴ can get an all-pass  $\frac{V_2}{V_1} = \frac{A - \alpha}{A + \alpha}$ ,  $\alpha \text{ real} = G/C$

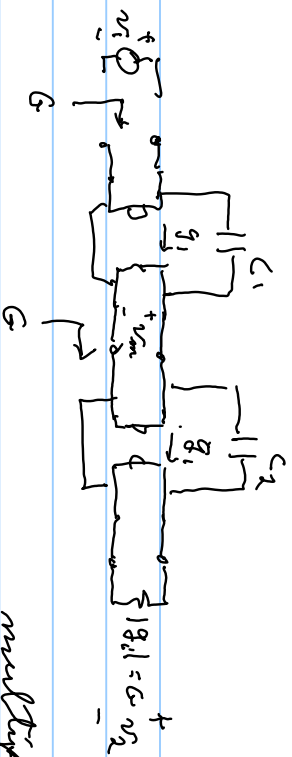
$$\left| \frac{V_2}{V_1}(j\omega) \right| = \left| \frac{j\omega - \alpha}{j\omega + \alpha} \right| = \frac{\sqrt{\omega^2 + (-\alpha)^2}}{\sqrt{\omega^2 + \alpha^2}} = 1$$

∴ use to phase shift

generalises to  $\frac{V_2}{V_1} = \frac{D(-\alpha)}{D(\alpha)} = \frac{\tilde{\epsilon}_1 D - \theta \alpha D}{\tilde{\epsilon}_2 D + \theta \alpha D}$



@  $A = j\omega$ ,  $\tilde{\epsilon}_1 D = \text{real part}$  &  $\theta \alpha D = \text{imaginary}$  ⇒  $\left| \frac{D(-j\omega)}{D(j\omega)} \right| = 1$



$$\frac{V_m}{V_1} = \frac{A - C_1/G}{A + C_1/G}$$

$$\frac{V_2}{V_m} = \frac{A - C_2/G}{A + C_2/G}$$

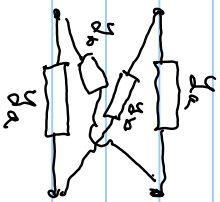
$$S \left[ \frac{V_2}{V_1} \right] = 2 \text{ near } 2c'a$$

multiply

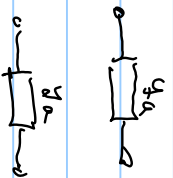
$$\frac{V_2}{V_m} \times \frac{V_m}{V_1} = \frac{V_2}{V_1} = \left( \frac{A - C_2/G}{A + C_2/G} \right) \left( \frac{A - C_1/G}{A + C_1/G} \right)$$

gives higher order but only with real zeroes and poles

another way to get all-pass (the classical way), the constant R lattices



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$$Y_a = Y_b$$

$$Y_a = \begin{bmatrix} y_a/2 & -y_a/2 \\ -y_a/2 & y_a/2 \end{bmatrix}, Y_b = \begin{bmatrix} y_b/2 & +y_b/2 \\ y_b/2 & y_b/2 \end{bmatrix}$$

$$Y = Y_a + Y_b = \frac{1}{2} \begin{bmatrix} y_a + y_b & y_b - y_a \\ y_b - y_a & y_a + y_b \end{bmatrix}, \Delta Y = (y_a + y_b)^2 - (y_b - y_a)^2 = 4y_a y_b \Rightarrow \Delta Y = y_a y_b = G^2$$

determinant

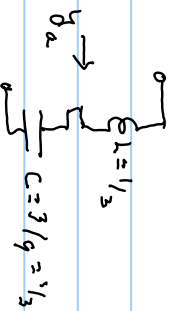
∴ for constant R;  $y_a y_b = G^2 \Rightarrow y_b = G^2 / y_a$

$$\frac{V_2}{V_1} = \frac{-y_{21}}{y_{22} + G} = \frac{-(y_b - y_a)/2}{2G + (y_a + G^2/y_a)} = \frac{y_a^2 - G^2}{y_a (2Gy_a + y_a^2 + G^2)} = \frac{y_a^2 - G^2}{(y_a + G)^2} = \frac{y_a - G}{y_a + G}$$

all  $y_a = \text{LPR} = \frac{m_a}{d_a} \Rightarrow \frac{V_2}{V_1} = \frac{m_a - G d_a}{m_a + G d_a} \Rightarrow$  all-ports of degree of  $y_a \Rightarrow S[y_a] = S \left[ \frac{V_2}{V_1} \right]; S.T. = \text{degree of}$

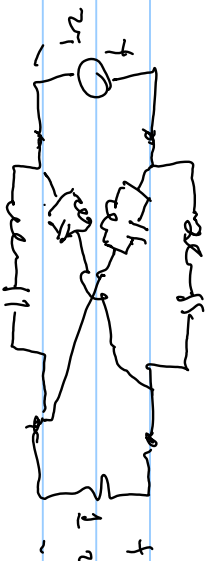
$$E_L: \frac{R^2 - 3R + 9}{R^2 + 3R + 9} = \frac{V_2}{V_1} \Rightarrow \frac{V_2}{V_1} = \frac{(R^2 + 9)(1 - 3R/(R^2 + 9))}{(R^2 + 9)(1 + \frac{3R}{R^2 + 9})} = \frac{\left(\frac{3R}{R^2 + 9} - 1\right)}{\left(\frac{3R}{R^2 + 9} + 1\right)} \quad | \quad G = 1$$

$$y_a = \frac{3R}{R^2 + 9} = \frac{1}{\frac{R}{3} + \frac{9}{3R}} \Rightarrow$$



$$y_b = \frac{G^2}{y_a} = \frac{1}{\frac{3R}{R^2 + 9}} = \frac{R^2 + 9}{3R} = \frac{R}{3} + \frac{3}{R}$$





$$v_2 = \frac{R^2 - 3a + 9}{R^2 + 3a + 9} v_1 \quad | \quad s \left[ \frac{v_2}{v_1} \right] = 2 \quad | \quad s \left[ y_2 \right] = 2 \quad | \quad y_2 = \frac{3a}{a^2 + 9}$$

ruota s'c'a, 4L'K & 4C'a

$$pola @ a_{1,2} = -\frac{3}{R} + \frac{1}{2} \sqrt{9 - 36} = -\frac{3}{2} \pm \frac{1}{2} \sqrt{27}$$



in all-pass