

ASSIGNMENT-3

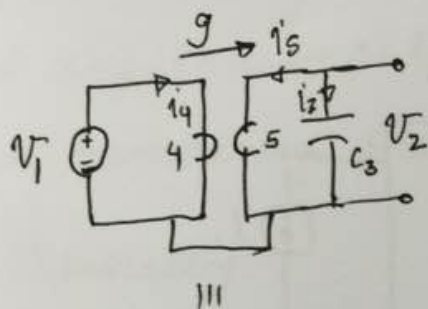
1.

SIDDHARTH TYAGI

ENEE-610 : NETWORK THEORY.

I

(a) given circuit:



Using notation used in class:-
we can obtain the Y_{b-2} of the two port network with V_1 as ~~input~~ and V_2 as the two ports:-

we know:

$$V_3 = \left(\frac{1}{sC_3}\right) i_3 \Rightarrow i_3 = (sC_3) \cdot V_3$$

$$\begin{bmatrix} i_4 \\ i_5 \end{bmatrix} = \begin{bmatrix} 0 & -g \\ g & 0 \end{bmatrix} \begin{bmatrix} V_4 \\ V_5 \end{bmatrix}$$

This yields the Y_{b-2} of the two port network as:-

$$Y_{b-2} = \begin{bmatrix} sC_3 & 0 & 0 \\ 0 & 0 & -g \\ 0 & g & 0 \end{bmatrix}$$

Now; we saw, the Y_{b-2}^a of the adjoint needs to be such that:-

$$Y_{b-2}^a = Y_{b-2}^T = \begin{bmatrix} sC_3 & 0 & 0 \\ 0 & 0 & g \\ 0 & -g & 0 \end{bmatrix}$$

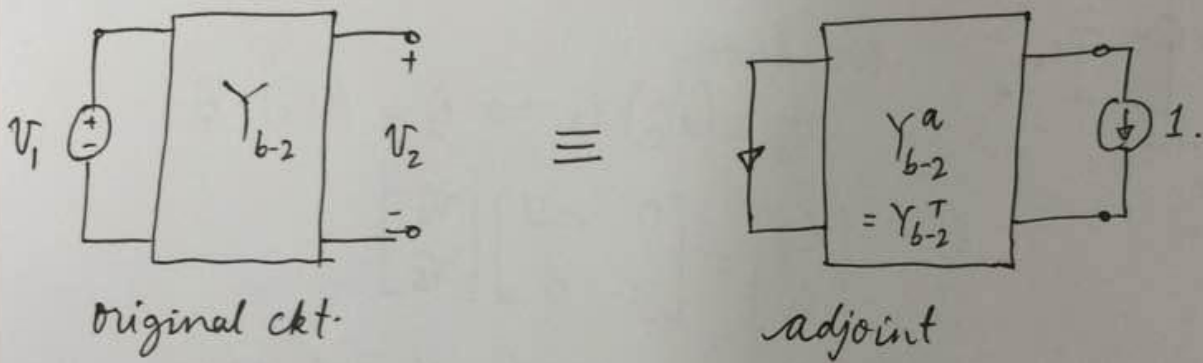
clearly, branch 3 will remain capacitor

branch 4/5 : a gyrator with inverted direction.

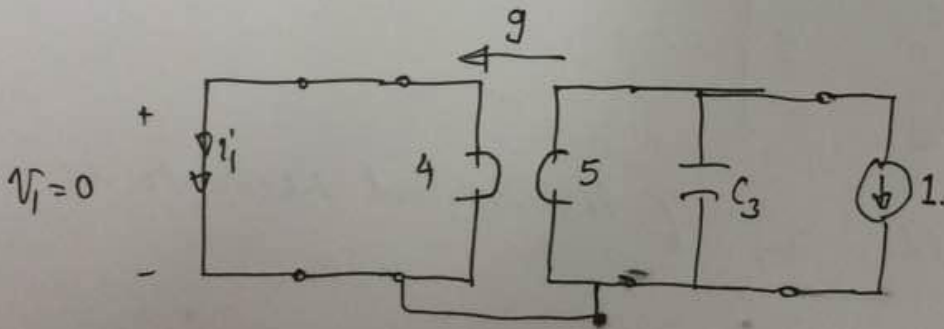
Thus: to obtain the adjoint circuit: the 2-port network (b) is given by Y_{b-2}^a .

Also; a voltage-source (input v_1) becomes a short-circuit in adjoint, and the open-part (v_2) becomes a current-source of value 1.

is



∴ The adjoint can be drawn as:-



Let
and
∴ Se
(v_{b1})
If
 x'
we g
 $\int \frac{dv_b}{dx}$
also
if
and

(b) To obtain the sensitivity using adjoint:-

Since both adjoint and original circuit have the same graph:

$$\boxed{V_b^T i_b^a - (V_b^a)^T i_b = 0}$$

Let input-and-output ports (v_1 and v_2) be $\underline{v_{b1}}$ and $\underline{v_{b2}}$ and remaining branches be $\underline{v_{b-2}}$.

∴ Separating:

$$(v_{b1} i_{b1}^a + v_{b2} i_{b2}^a + v_{b-2}^T i_{b-2}^a) - (v_{b1}^a i_{b1} + v_{b2}^a i_{b2} + (v_{b-2}^a)^T i_{b-2}) = 0$$

If 'x' be a parameter; taking ~~the~~ derivative of above eqⁿ wrt 'x' and noting that derivatives of all adjoint terms = 0

we get:-

$$\left\{ \frac{dv_{b1}}{dx} i_{b1}^a + \frac{dv_{b2}}{dx} i_{b2}^a + \left(\frac{d}{dx} v_{b-2}^T \right) i_{b-2}^a \right\} - \left\{ v_{b1}^a \frac{di_{b1}}{dx} + v_{b2}^a \frac{di_{b2}}{dx} + (v_{b-2}^a)^T \frac{di_{b-2}}{dx} \right\} = 0$$

also $i_{b2} = 0$ [∵ open]

$$\text{if } v_{b1} = 1 \text{ (constant)} \Rightarrow T = \frac{v_{b2}}{v_{b1}} = v_{b2}$$

and if we choose $i_{b2}^a = 1$, above simplifies to:

$$\therefore \frac{dv_{b2}}{dx} = v_{b1}^a \frac{di_{b1}}{dx} + \left[(v_{b-2}^a)^T \frac{di_{b-2}}{dx} - \frac{d}{dx} (v_{b-2}^a)^T i_{b-2}^a \right]$$

using: $i_{b-2} = Y_{b-2} v_{b-2}$; $i_{b-2}^a = Y_{b-2}^a v_{b-2}^a$; above can be expressed as:-

$$\frac{dv_{b-2}}{dx} = v_{b-2}^a \frac{di_{b-2}}{dx} + \frac{dv_{b-2}^T}{dx} [Y_{b-2}^a - Y_{b-2}^T] \cdot v_{b-2}^a + \left[(v_{b-2}^a)^T \frac{dY}{dx} v_{b-2} \right]$$

If $v_{b-2}^a = 0$; and $Y_{b-2}^a = Y_{b-2}^T$

$$\Rightarrow \boxed{\frac{dT}{dx} = + (v_{b-2}^a)^T \frac{dY_{b-2}}{dx} v_{b-2}}$$

($\because v_{b-2} = T$ when $v_{b-2} = 1$)

(c) The given $T = \frac{v_2}{v_1}$;

When $x = C_3$: $v_{b-2}^a = \begin{bmatrix} v_3^a \\ v_4^a \\ v_5^a \end{bmatrix}$ $v_{b-2} = \begin{bmatrix} v_3 \\ v_4 \\ v_5 \end{bmatrix}$

$$\therefore \frac{dT}{dC_3} = - [v_3^a \ v_4^a \ v_5^a] \cdot \frac{d}{dC_3} \begin{bmatrix} sC_3 & 0 & 0 \\ 0 & 0 & -g \\ 0 & g & 0 \end{bmatrix} \begin{bmatrix} v_3 \\ v_4 \\ v_5 \end{bmatrix}$$

$$= - [v_3^a \ v_4^a \ v_5^a] \begin{bmatrix} s & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} v_3 \\ v_4 \\ v_5 \end{bmatrix}$$

$$= -s \cdot v_3^a v_3 = v_3 = -g \cdot \left(\frac{1}{sC_3} \right) = -\frac{g}{sC_3}$$

$$v_3^a = -\frac{1}{sC_3}$$

$$\therefore \boxed{\frac{dT}{dC_3} = + \frac{g}{sC_3^2}}$$

$$\therefore S_{g_3}^T = \left(\frac{\frac{dT}{dg_3}}{\frac{T}{g_3}} \right) = \frac{-\frac{g}{sc_3^2}}{-\frac{g}{sc_3^2}} \quad (\because T = -\frac{g}{sc_3^2})$$

$$\boxed{S_{g_3}^T = -1}$$

When $x = g$

$$\therefore \frac{dT}{dg} = + [v_3^a \ v_4^a \ v_5^a] \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} v_3 \\ v_4 \\ v_5 \end{bmatrix}$$

$$= + [v_3^a \ v_4^a \ v_5^a] \begin{bmatrix} 0 \\ -v_5 \\ v_4 \end{bmatrix}$$

$$\therefore \frac{dT}{dg} = + \left\{ -v_4^a v_5 + v_5^a v_4 \right\}$$

$$v_4^a = 0$$

$$v_5^a = -\frac{1}{sc_3}$$

$$v_4 = 1.$$

$$T = -\frac{g}{sc_3^2}$$

$$\therefore \boxed{\frac{dT}{dg} = +\frac{1}{sc_3}}$$

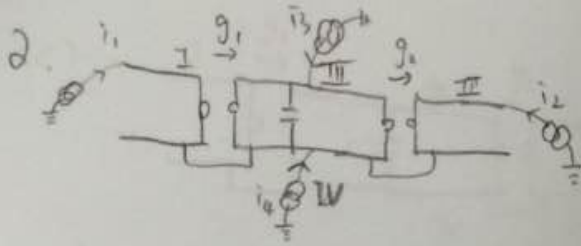
$$\therefore \boxed{S_g^T = \frac{\frac{dT}{dg}}{\frac{T}{g}} = \frac{+\frac{1}{sc_3}}{-\frac{g}{sc_3^2}} = +1.}$$

(d)

$$T = -\frac{g}{5C_3} \Rightarrow \boxed{\frac{dT}{dC_3} = \frac{g}{5C_3^2}} \quad (\text{as earlier})$$

$$\therefore S_{C_3}^T = \frac{\frac{g}{5C_3^2}}{-\frac{g}{5C_3^2}} = -1.$$

also, $\boxed{\frac{dT}{dg} = \frac{-1}{5C_3^2}} \quad (\text{as earlier})$



$$\begin{aligned}
 a) \quad i_1 &= g_1 (v_2 - v_4) \\
 i_2 &= -g_2 (v_3 - v_4) \\
 i_3 &= -g_1 (v_1 - v_4) + sc (v_2 - v_4) + g_2 (v_2 - v_4) \\
 i_4 &= -(i_1 + i_2 + i_3)
 \end{aligned}$$

$$\begin{bmatrix} i_1 \\ i_2 \\ i_3 \\ i_4 \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 0 & g_1 & -g_1 \\ 0 & 0 & -g_2 & g_2 \\ -g_1 & g_2 & sc & g_1 - g_2 - sc \\ g_1 & -g_2 & g_2 - g_1 - sc & sc \end{bmatrix}}_{Y_{4 \times 4}} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix}$$

$$b) \quad \text{Ground node IV, } v_4 = 0, \quad i_4 = -(i_1 + i_2 + i_3)$$

$$\begin{bmatrix} i_1 \\ i_2 \\ i_3 \end{bmatrix} = \begin{bmatrix} 0 & 0 & g_1 \\ 0 & 0 & -g_2 \\ -g_1 & g_2 & sc \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix}$$

$$\text{eliminate III, } i_3 = 0$$

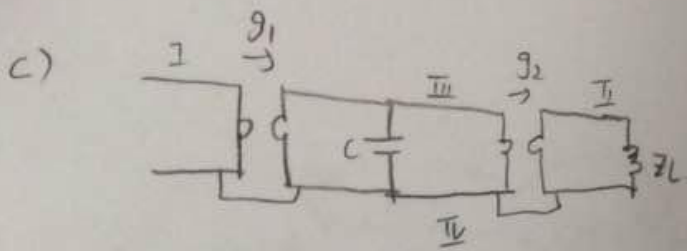
$$i_3 = [g_1 \quad g_2] \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + [sc] [v_3] = 0$$

$$v_3 = -\frac{1}{sc} [g_1 \quad g_2] \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + \begin{bmatrix} -g_1 \\ -g_2 \end{bmatrix} \cdot \left(-\frac{1}{sc}\right) \cdot [g_1 \quad g_2] \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$Y_{2 \text{port}} = \left(\begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} - \frac{1}{sc} \begin{bmatrix} -g_1^2 & g_1 g_2 \\ g_1 g_2 & -g_2^2 \end{bmatrix} \right) \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$= \frac{1}{sc} \begin{bmatrix} g_1^2 & -g_1 g_2 \\ -g_1 g_2 & g_2^2 \end{bmatrix} \quad \text{where it is singular, no } Z_{in} \text{ exist}$$



$$i_1 = g_1 (V_3 - V_4)$$

$$i_2 = -g_2 (V_3 - V_4) + \frac{1}{z_L} (V_2 - V_4)$$

$$i_3 = -g_1 (V_1 - V_4) + sC (V_3 - V_4) + g_2 (V_2 - V_4)$$

$$i_4 = -(i_1 + i_2 + i_3)$$

$$Y_{4 \times 4} = \begin{bmatrix} 0 & 0 & g_1 & -g_1 \\ 0 & \frac{1}{z_L} & -g_2 & g_2 - \frac{1}{z_L} \\ -g_1 & g_2 & sC & g_1 - g_2 - sC \\ g_1 & g_2 - \frac{1}{z_L} & g_2 - g_1 - sC & \frac{1}{z_L} + sC \end{bmatrix}$$

since $i_4 = -(i_1 + i_2 + i_3)$

$$\text{so } Y_{3 \times 3} = \begin{bmatrix} 0 & 0 & g_1 \\ 0 & \frac{1}{z_L} & -g_2 \\ -g_1 & g_2 & sC \end{bmatrix}$$

eliminate III $i_3 = 0$

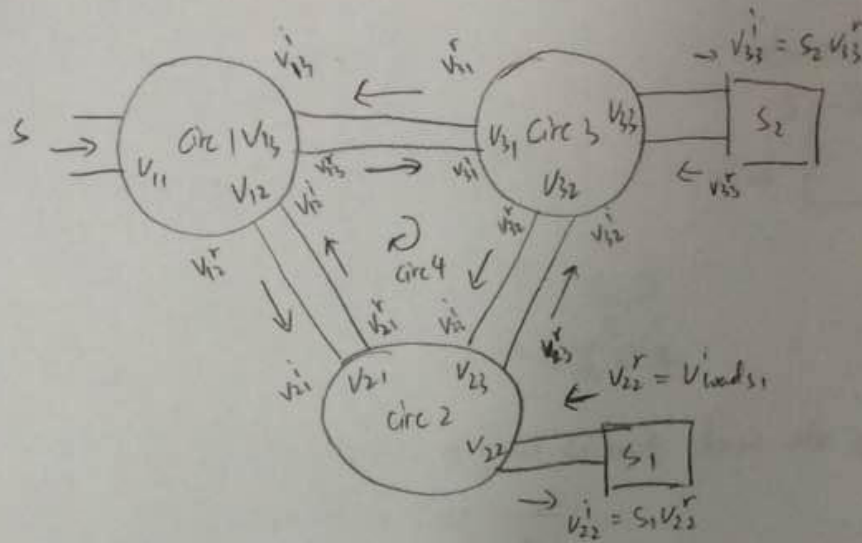
$$i_3 = \begin{bmatrix} -g_1 & g_2 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} + sC (V_3) = 0$$

$$V_3 = -\frac{1}{sC} \begin{bmatrix} -g_1 & g_2 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$Y_{2 \times 2} = \begin{bmatrix} 0 & 0 \\ 0 & \frac{1}{z_L} \end{bmatrix} - \frac{1}{sC} \begin{bmatrix} -g_1^2 & g_1 g_2 \\ g_1 g_2 & -g_2^2 \end{bmatrix} = \begin{bmatrix} \frac{g_1^2}{sC} & -\frac{g_1 g_2}{sC} \\ -\frac{g_1 g_2}{sC} & \frac{1}{z_L} + \frac{g_2^2}{sC} \end{bmatrix}$$

$$Z = Y^{-1}$$

$$\text{input impedance } z_{in} = \frac{1}{\Delta} \cdot \left(\frac{1}{z_L} + \frac{g_2^2}{sC} \right) = \frac{1}{\frac{g_1^2}{sC} \left(\frac{1}{z_L} + \frac{g_2^2}{sC} \right) - \left(\frac{g_1 g_2}{sC} \right)^2} \cdot \left(\frac{1}{z_L} + \frac{g_2^2}{sC} \right) = \frac{sC + z_L \cdot g_2^2}{g_1^2}$$



since all loads are normalized to $Z_0 = 1$, all terms can be depended only on incident V^i and reflected V^r .

counted counter clockwise

$$V_{12}^r = V_{11}^i \quad V_{22}^r = V_{21}^i \quad V_{32}^r = V_{31}^i, \quad V_{11}^r = V_{31}^i, \quad V_{12}^r = V_{32}^i, \quad V_{13}^r = V_{33}^i$$

and $V_{21}^i = V_{12}^r \quad V_{31}^i = V_{21}^r \quad V_{32}^i = V_{23}^r$

$$V_{11}^r = V_{13}^i = V_{31}^r = V_{33}^i = S_2 V_{33}^r = S_2 V_{32}^i = S_2 V_{23}^r = S_2 V_{22}^i = S_1 S_2 V_{22}^r$$

$$= S_1 S_2 V_{21}^i = S_1 S_2 V_{12}^r = S_1 S_2 V_{11}^i$$

so $S = S_1 S_2$
so it is lossless.

Anomaly there exist a circulator 4 which towards clockwise among the inner side of these three circulator, which will cause reduction of the efficiency.