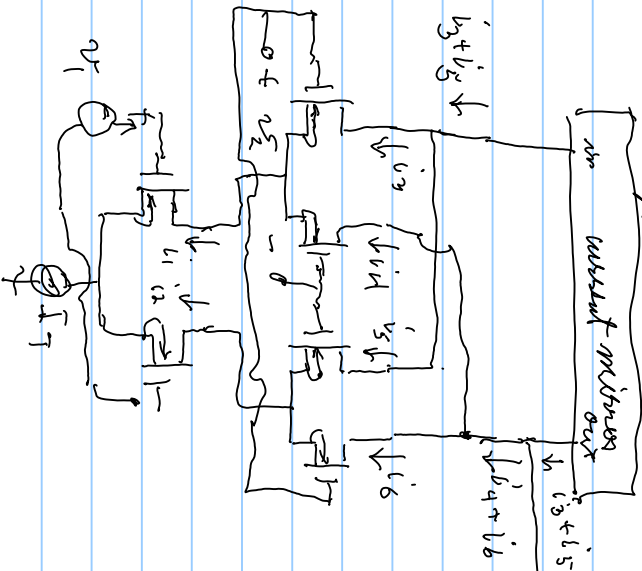


Diode multiplier



$$(i_4 + i_6) - (i_3 + i_5)$$

$$i_3 = \frac{i_1}{2} (1 + \sin \alpha)$$

$$i_4 = \frac{i_1}{2} (1 - \sin \alpha)$$

$$i_5 = \frac{i_2}{2} (1 - \sin \alpha)$$

$$i_6 = \frac{i_2}{2} (1 + \sin \alpha)$$

$$i_1 = \frac{I_T}{2} (1 + \sin \alpha)$$

$$i_2 = \frac{I_T}{2} (1 - \sin \alpha)$$

EE 610
10/20/16

$$i_3 = \frac{I_T}{4} (1 + f(v_1))(1 + f(v_2)) = \frac{I_T}{4} (1 + f(v_1) + f(v_2) + f(v_1)f(v_2))$$

$$i_4 = \frac{I_T}{4} (1 + f(v_1))(1 - f(v_2)) = \frac{I_T}{4} (1 + f(v_1) - f(v_2) - f(v_1)f(v_2))$$

$$i_5 = \frac{I_T}{4} (1 - f(v_1))(1 - f(v_2)) = \frac{I_T}{4} (1 - f(v_1) - f(v_2) + f(v_1)f(v_2))$$

$$i_6 = \frac{I_T}{4} (1 - f(v_1))(1 + f(v_2)) = \frac{I_T}{4} (1 - f(v_1) + f(v_2) - f(v_1)f(v_2))$$

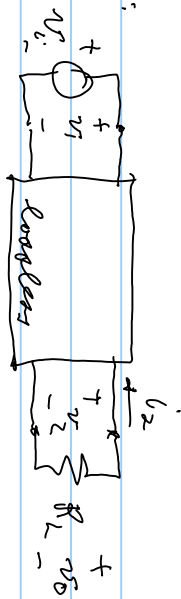
$$i_3 + i_5 = \frac{I_T}{4} (2 + 2f(v_1)f(v_2)), \quad i_4 + i_6 = -\frac{I_T}{4} (2 - 2f(v_1)f(v_2))$$

$$(i_3 + i_5) - (i_4 + i_6) = \frac{I_T}{4} (4f(v_1)f(v_2)) = I_T f(v_1)f(v_2)$$

$$\text{near origin} \approx I_T \cdot (k) v_1 v_2 \sqrt{1 - 2v_1^2} \sqrt{1 - 2v_2^2}$$

gives a very good multiplexer

Synthesis of $\frac{v_0}{v_i}$:



$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}, \quad \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} v_i \\ v_0 \end{bmatrix}; \quad v_0 = -R_L i_2, \quad G_L = 1/R_L$$

$$\begin{bmatrix} i_1 \\ -G_L v_0 \end{bmatrix} = \begin{bmatrix} y_{11} v_i + y_{12} v_0 \\ y_{21} v_i + y_{22} v_0 \end{bmatrix} \Rightarrow (-G_L - y_{22}) v_0 = y_{21} v_i$$

$$\frac{v_0}{v_i} = \frac{-y_{21}}{G_L + y_{22}} = \frac{-y_{21}/G_L}{1 + y_{22}/G_L} = \frac{-y_{21}}{1 + y_{22}}$$

If $G_{22}(s) = \frac{N_{22}(s)}{D_{22}(s)}$ then $1 + y_{22} = \frac{N_{22}(s) + D_{22}(s)}{D_{22}(s)}$

$$\begin{aligned}
 \frac{N_0}{N_1} &= \frac{-y_{21}(a), D_{22}(a)}{N_{22}(a) + D_{22}(a)} = \frac{K}{P(a)} \quad \leftarrow \text{if low-pass} \\
 P(a) &= \text{Hurwitz}
 \end{aligned}$$

create $y_{22} = \frac{E_{22} P(a)}{D_{22} P(a)}$ then y_{22} is an lossless PR function

also if poles of y_{21} are in y_{22} & if zeros of y_{22} are poles of y_{21} , to get the numerator or a constant: if low-pass synthesis y_{22} by 1st case

$$\frac{E_{21}}{N_1} = \frac{N_0(a)}{K} = \frac{a^6 + a^5 + 9a^4 + 6a^3 + 23a^2 + 8a + 15}{K}$$

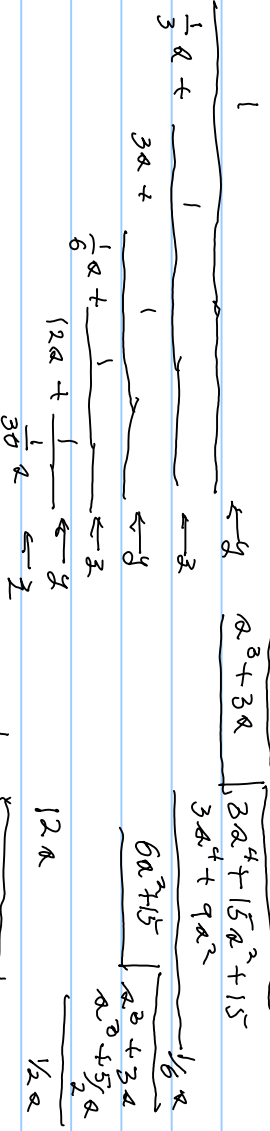
$$= \frac{K / (a^5 + 6a^3 + 8a)}{1 + \frac{(a^6 + 9a^4 + 23a^2 + 15)}{a^5 + 6a^3 + 8a}}$$

$$\Rightarrow y_{21}(a) = \frac{a^5 + 9a^4 + 23a^2 + 15}{a^5 + 6a^3 + 8a}$$

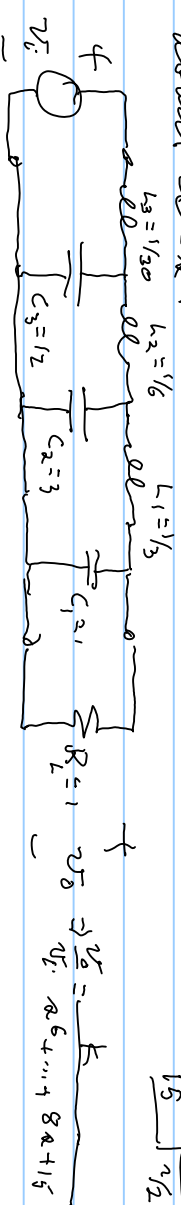
1st Layer

$$\frac{a^5 + 6a^3 + 8a}{a} \cdot \frac{a^6 + 9a^4 + 23a^2 + 15}{a^6 + 6a^4 + 8a^2} \cdot \frac{3a^4 + 15a^2 + 15}{a^5 + 6a^3 + 8a} \cdot \frac{1}{3} \cdot a$$

$Y_{12} = a^4$

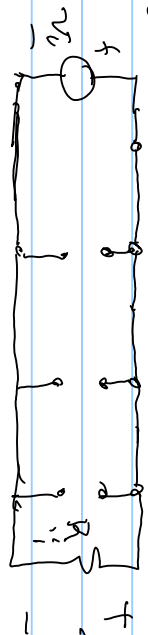


= continued fraction expansion about $a^0 = a$.

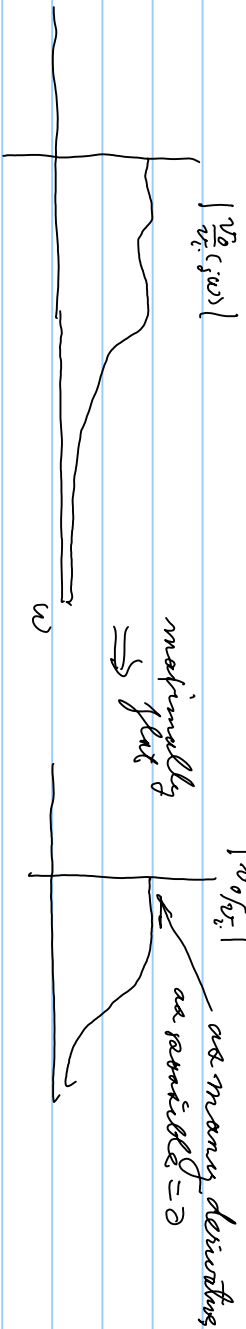


$$v_{01} v_1 (a=0) = \frac{K}{15}$$

at $R=0$



$$v_o = v_c \quad \frac{v_o}{v_c} = 1 = \frac{K}{15}, \quad K=15$$



Given that $T(s) = v_o/v_c =$ low-pass maximally flat of degree n

$$\frac{d^k |T(j\omega)|}{d\omega^k} \Big|_{\omega=0} ; T(s) = \frac{1}{s^n + a_{n-1}s^{n-1} + \dots + a_1s + a_0}$$

$$\frac{d(|1/T(j\omega)|)}{d\omega} \Big|_{\omega=0} \Rightarrow \frac{d\left(\frac{1}{|T(j\omega)|^2}\right)}{d\omega} \Big|_{\omega=0} = \frac{d}{d\omega} \left(\frac{1}{|T(j\omega)|^2} \right)$$

$$\overbrace{T(z)T(\bar{z})}^{K^2} = \omega^{2n} + b_{2n-2} \omega^{2n-2} + \dots + b_2 \omega^2 + b_0$$

$$\frac{d}{dz} \frac{1}{f(z)} = -\frac{1}{(f(z))^2} \cdot \frac{df(z)}{dz}$$

$$\frac{d}{dz} \left(\frac{K^2}{T(z)T(\bar{z})} \right) = 2n \omega^{2n-1} + 2n-2 \cdot b_{2n-2} \omega^{2n-3} + \dots + 2b_2 \omega^1$$

⋮