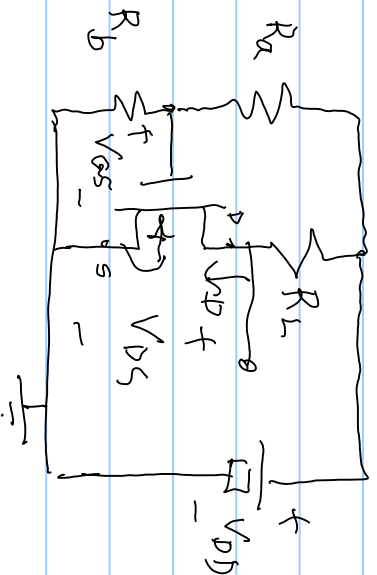


Given a transistor (MOS), & I_D & A_v & V_{DD}

$$I_D = \beta (V_{GS} - V_{TO})^2 (1 + \lambda V_{DS}) \quad \beta = \frac{\mu_n C_{ox} W}{2L}, \quad V_{TO}, \lambda \text{ known}$$

$$A_v = -g_m R_L \quad \text{actually } g_m + G_L \Rightarrow 1/R_L$$



Let $\lambda \rightarrow 0$

$$I_D = \beta (V_{GS} - V_{TO})^2 \Rightarrow V_{GS} = V_{TO} + \sqrt{\frac{I_D}{\beta}}$$

$$\frac{R_b}{R_a + R_b} V_{DD} = V_{GS} \Rightarrow R_a = \left(\frac{V_{DD}}{V_{GS}} - 1 \right) \frac{R_b}{\beta}$$

choose R_b large

$$g_m = \frac{\partial I_D}{\partial V_{GS}} \Big|_Q \approx \frac{2 I_D}{(V_{GS} - V_{TO})}$$

known if $\lambda = 0$ we found V_{GS}

$$\Rightarrow R_L = -\frac{A_v}{g_m} = \frac{(V_{GS} - V_{TO})}{2 I_D}$$

$$V_{DS} = V_{DD} - R_L I_D \quad \text{need } V_{GS} > (V_{GS} - V_{TO})$$

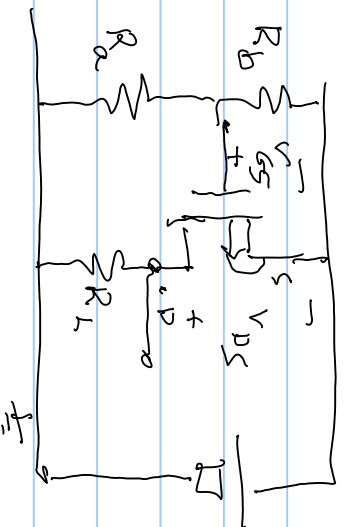
If $\lambda \ll 0$ then $I_D \cdot R_L = \frac{(V_{GS} - V_{TO})}{\lambda} = \beta (V_{GS} - V_{TO})^2 (1 + \lambda V_{DS}) \cdot R_L$

$$(V_{GS} - V_{TO}) \approx \beta (V_{GS} - V_{TO})^2 \cdot (1 + \lambda [V_{DD} - R_L I_D]) \cdot R_L$$

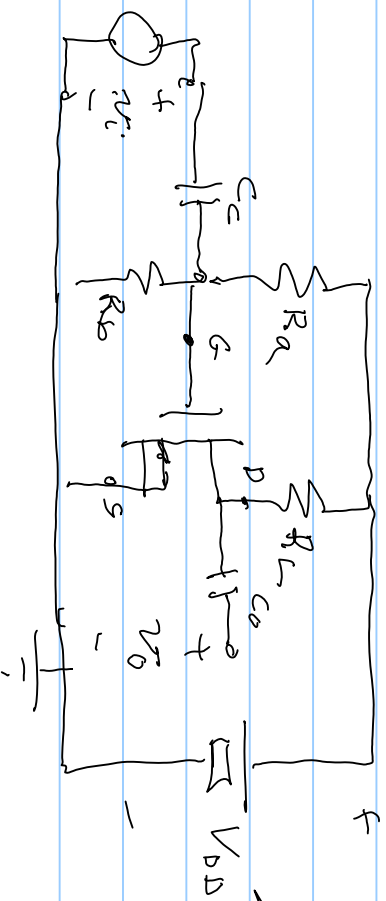
$$\Rightarrow 1 = \beta (V_{GS} - V_{TO}) (1 + \lambda [V_{DD} - R_L \beta (V_{GS} - V_{TO})^2 (1 + \lambda V_{DS})]) \cdot R_L$$

\Rightarrow use 1st order approximation & iterate via CAP
Series \Rightarrow PARAM

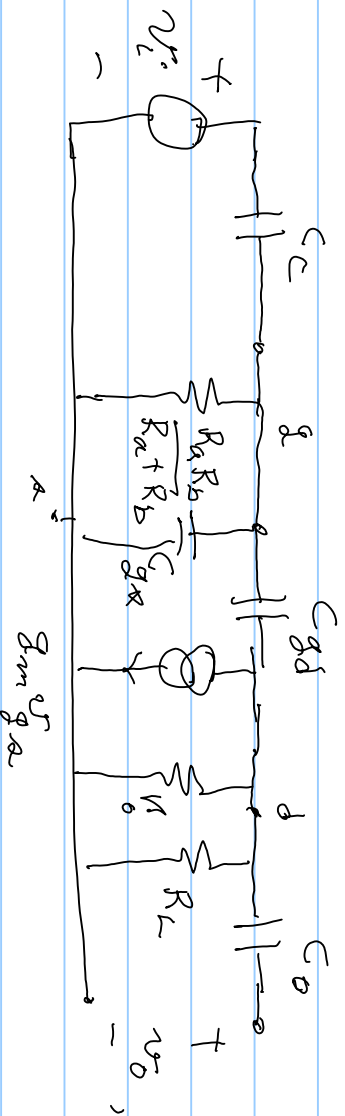
for PMOS



to signal we insert capacitors to decouple
 bias from signal



short for small
 ac signals

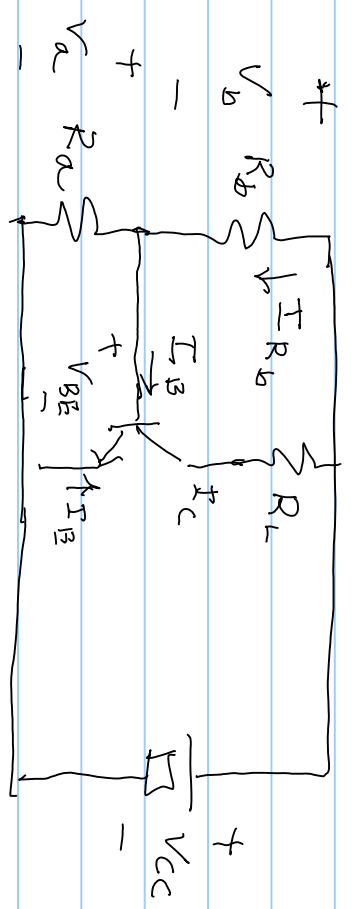


$$R_L' = V_{DD} || R_L = \frac{1}{g_d + g_L}$$

$$A_{v'} = \frac{v_o}{v_i} (A) = -g_m R_L' \quad \text{@ } \omega = \omega_c$$

choose C_c & C_o large so they are shorts @ signal frequency

for m.p.m.: know $I_B \neq 0 \Rightarrow$ if know I_C , $I_B = \frac{1}{\beta} I_C$



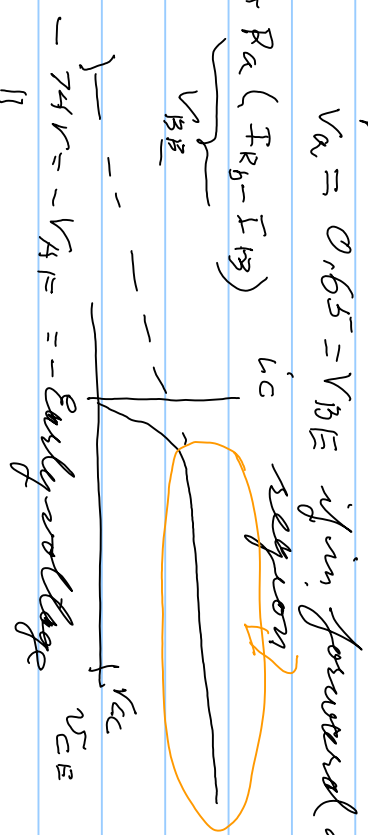
assume $V_{BE} \approx 0.65V$

know $V_{CC} = R_b I_{R_b} + R_a (I_{R_b} - I_B)$

if know $R_b \Rightarrow I_{R_b}$ if in forward active

if know R_a know $V_{CC} = V_b + R_a (I_{R_b} - I_B)$

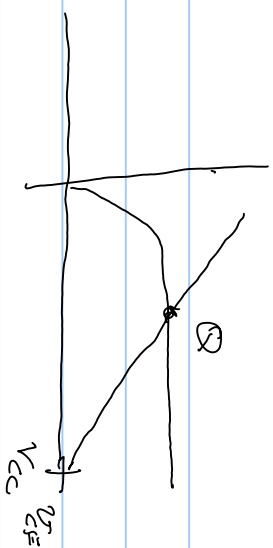
$$R_a = \frac{V_{BE}}{I_{R_b} - I_B}$$



2N3904

$$A_{v2} = -g_m R_L \approx -\frac{I_C}{V_T} R_L \Rightarrow R_L = -\frac{A_{v2}}{g_m}$$

or some difficulties



$$g_m = \frac{I_C}{V_T} \approx \frac{1}{r_{be}} = \frac{g_m}{r_{be}}$$

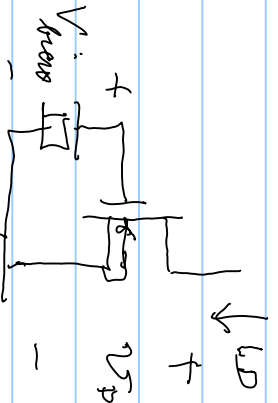
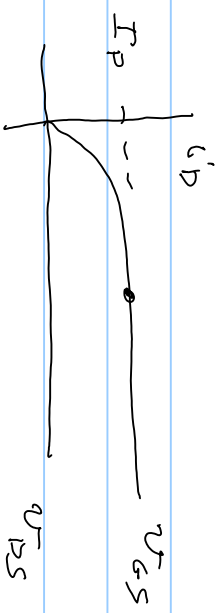
data sheet gives $\beta_{FE} = \frac{I_C}{I_B}$

$\beta \Rightarrow$ constant $V_{CE} = a$ sketch

comes from H parameters

$$\begin{bmatrix} v_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} i_1 \\ v_2 \end{bmatrix}$$

Current mirrors & sources



V_{DS} constant \Rightarrow looks like current source
 needs $V_{DS} \geq (V_{bias} - V_{th})$
 $I_D = I_{bias}$

For mirrors

