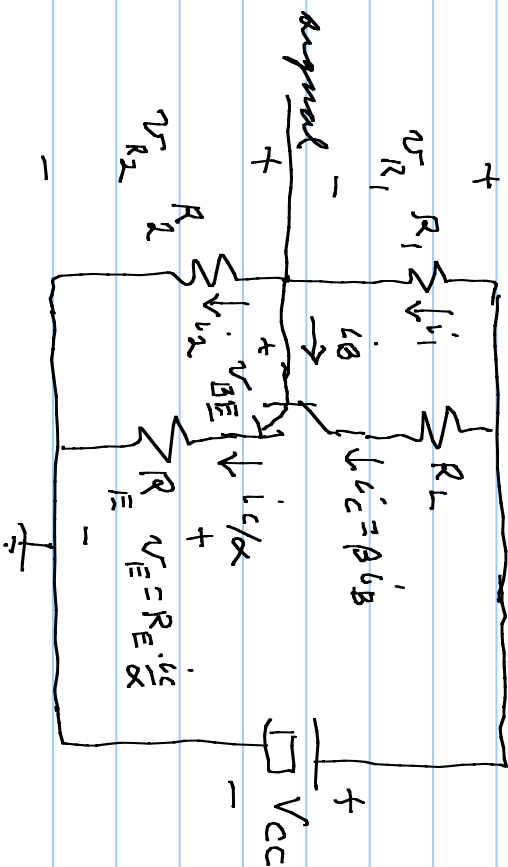


EE303H  
09/29/15

# BJT Biasing



assume  $V_{BE} = 1V$

choose  $R_2$  say  $10M\Omega$

$$I_2 = \frac{1.65}{R_2} = 0.165 \mu A$$

$I_B = 5 \mu A$  need  $I_C$  choose  $= 1mA \Rightarrow g_m = \frac{1 \times 10^{-3}}{26 \times 10^{-3}} = \frac{I_C}{V_T}$

need  $\beta$ , assume  $\beta = 200$

$$V_{R2} = V_{BE} + V_E$$

$$= 0.65$$

$$I_1 = I_B + I_2 = \frac{I_C}{\beta} + I_2$$

$$I_2 = \frac{0.65 + V_E}{R_2}$$

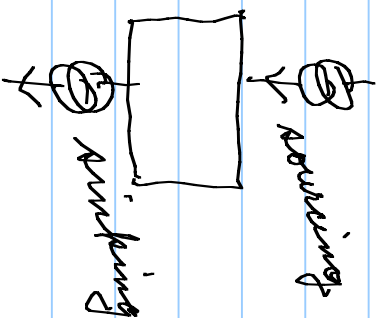
$$I_B = \frac{I_C}{\beta} = \frac{10^{-3}}{2 \times 10^2} = 0.5 \times 10^{-5} = 5 \mu A$$

$$I_1 = I_B + I_2 = (5 + 0.165) \times 10^{-6} = 5.165 \mu A$$

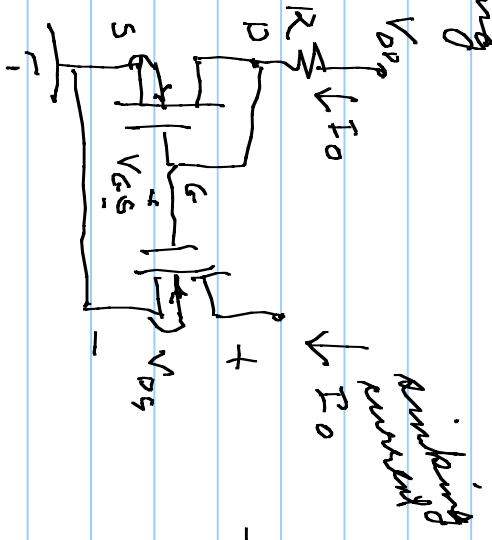
assuming  $V_{CE} = 6V$  then  $V_{R_1} = V_{CE} - V_{R_2} = 6 - 1.65 = 4.35V$

$$R_1 = \frac{V_{R_1}}{I_1} = \frac{4.35}{5.165 \times 10^{-6}} \approx 0.8 \times 10^6 = 800k\Omega$$

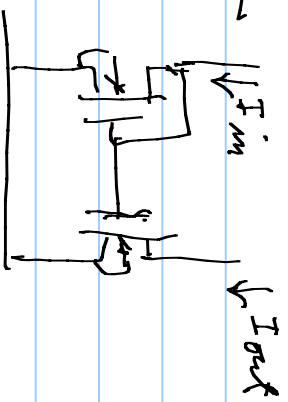
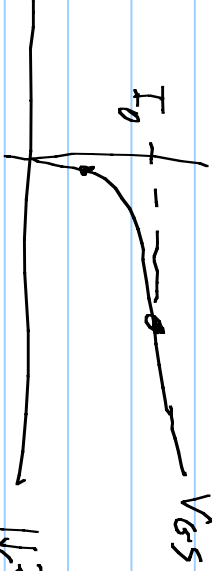
Current mirrors



amplifier

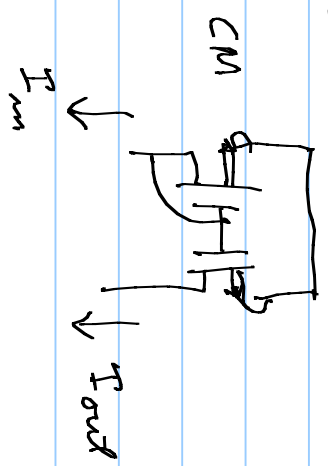
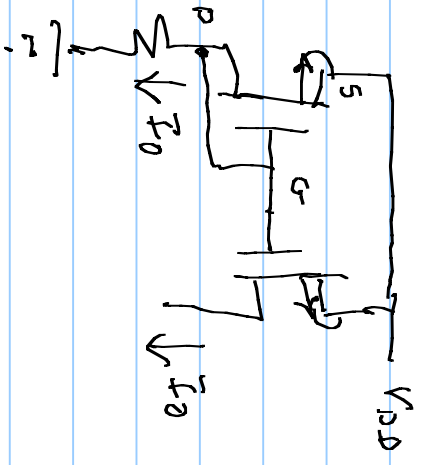


amplifier current

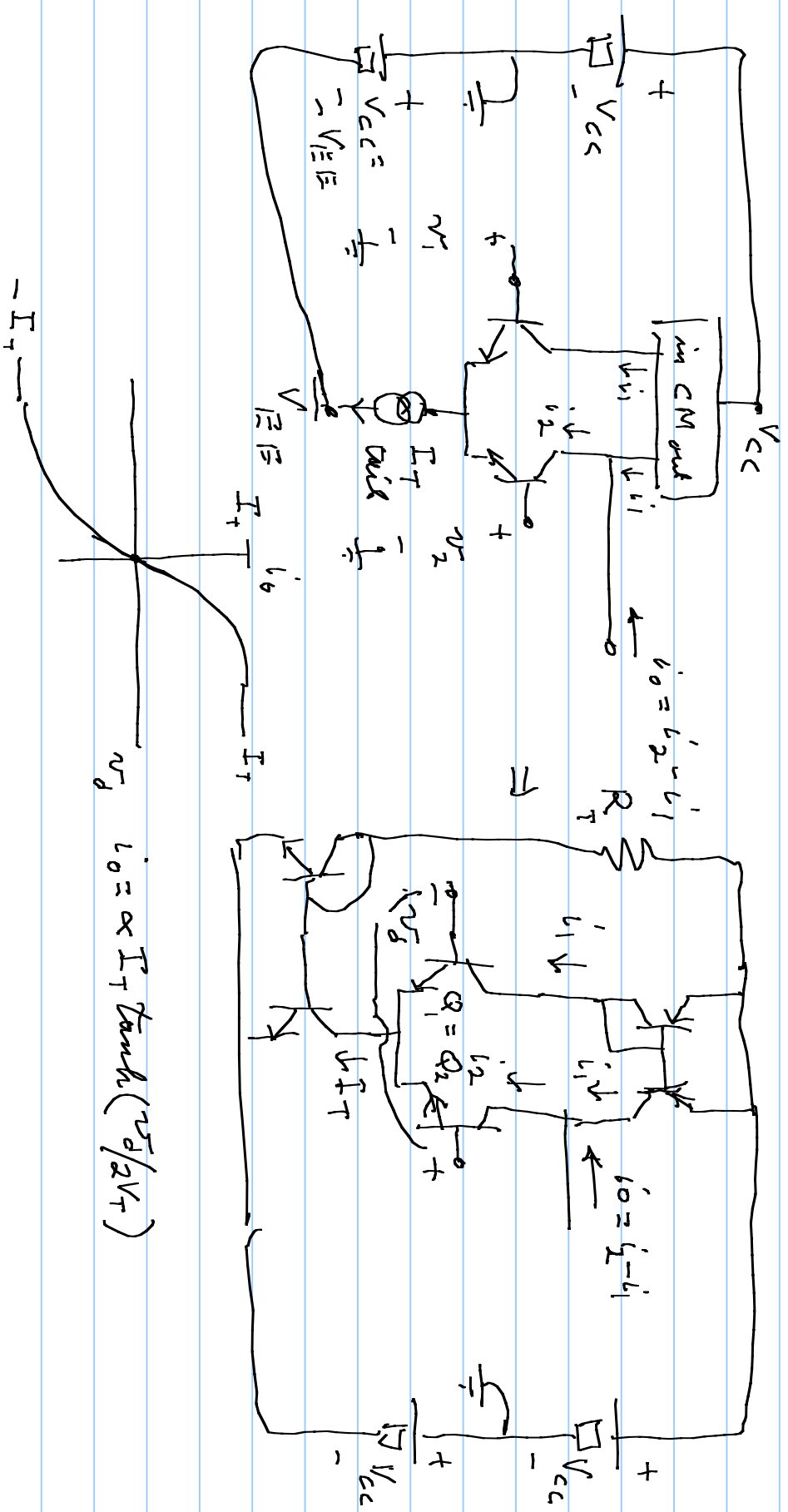


current mirror

Amplifier



differential pair  $\Rightarrow$  low  $\approx$  differential input



need  $i_1$  &  $i_2$  around in forward active region

$$I_T \text{ fixed } I_T = \frac{i_1}{\alpha} + \frac{i_2}{\alpha} \quad ; \quad v_D = v_{BE2} - v_{BE1}$$

$$\frac{i_1}{\alpha} = I_S e^{v_{BE1}/V_T} \quad ; \quad \frac{i_2}{\alpha} = I_S e^{v_{BE2}/V_T}$$

$$\ln\left(\frac{i_1/\alpha}{I_S}\right) = v_{BE1}/V_T \quad \ln\left(\frac{i_2/\alpha}{I_S}\right) = v_{BE2}/V_T$$

$$v_D = \ln\left(\frac{i_2/\alpha}{I_S}\right) - \ln\left(\frac{i_1/\alpha}{I_S}\right) = \ln\left(\frac{i_2/i_1}{1}\right) \Rightarrow \frac{i_2}{i_1} = e^{v_D/V_T}$$

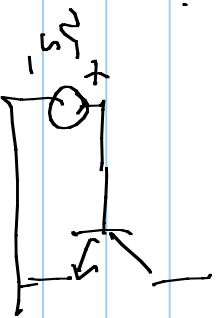
$$i_1 + i_2 = \alpha I_T \quad ; \quad i_2 = i_2 - i_1 \Rightarrow i_0 = i_1 \times \left(\frac{i_2}{i_1} - 1\right) \Rightarrow \frac{i_0}{\alpha I_T} = \frac{\left(\frac{i_2}{i_1} - 1\right)}{\left(\frac{i_2}{i_1} + 1\right)}$$

$$i_0 = \alpha I_T \left[ \frac{e^{v_D/V_T} - 1}{e^{v_D/V_T} + 1} \right] = \alpha I_T \frac{e^{v_D/2V_T} \left[ e^{v_D/2V_T} - e^{-v_D/2V_T} \right]}{e^{v_D/2V_T} \left[ e^{v_D/2V_T} + e^{-v_D/2V_T} \right]}$$

$$= \alpha I_T \tanh\left(\frac{v_D}{2V_T}\right)$$

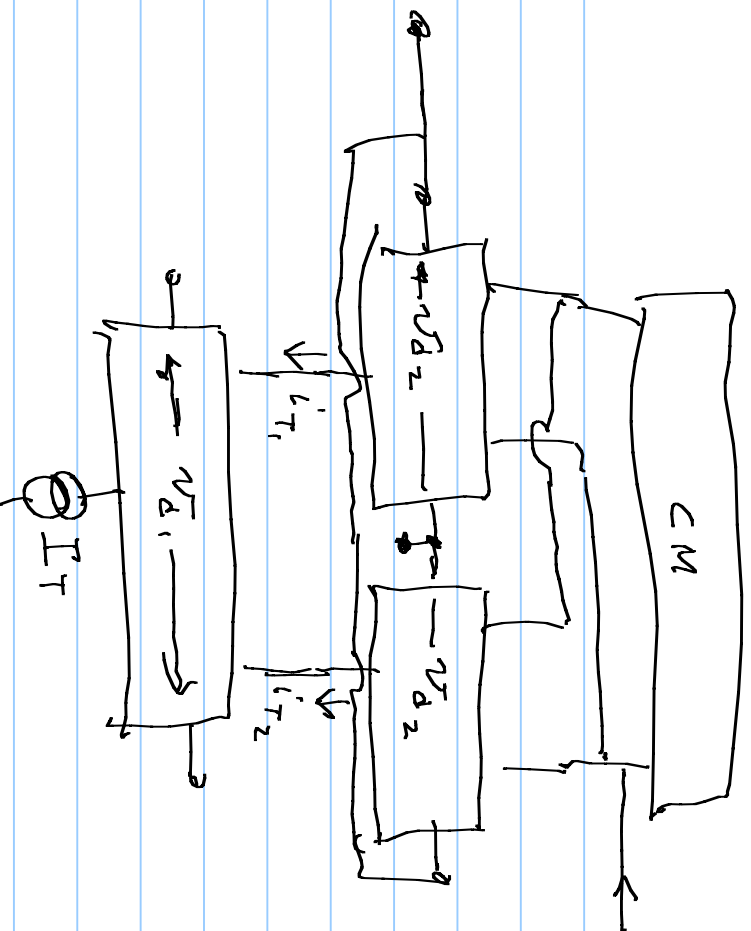
$$\begin{aligned}
 q_m &= \frac{q_{LO}}{2V_D} \Big|_{V_D=0} = \alpha I_T \cdot \frac{1}{2V_T} \frac{d \tanh(v_D/2V_T)}{d(v_D/2V_T)} \Big|_{V_D=0} = \frac{\alpha I_T}{2V_T} (1 - \tanh^2(v_D/2V_T)) \Big|_{V_D=0} \\
 &= \frac{\alpha}{2} \frac{I_T}{V_T}
 \end{aligned}$$

a multiplier make  $I_T$  vary with another signal  
 i.e. but  $I_T$  needs to be  $\gg 0$



for a 4-quadrant multiplier

} gives a 2  
 quadrant  
 multiplier



$$i'_0 = I_T \tanh\left(\frac{V_{D1} - V_{D2}}{2V_T}\right) = \tanh\left(\frac{V_{D2} - V_{D1}}{2V_T}\right)$$