

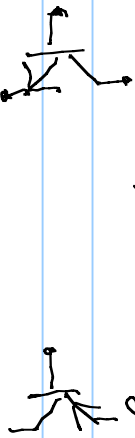
EE 303H
09/16/14

BJT Fig. 6.3, p. 354 = mon, Fig. 6.10, p. 364 = PNP
large signal Fig. 6.5, p. 358, T model, small signal, p. 410
Bode, Sp. 6.10, p. 390

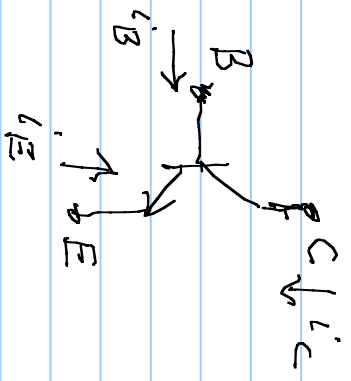
(Agris) ~~shows the~~ Bode plots, p. 372, Fig. 6.17

CE amp, p. 427, Fig. 6.50

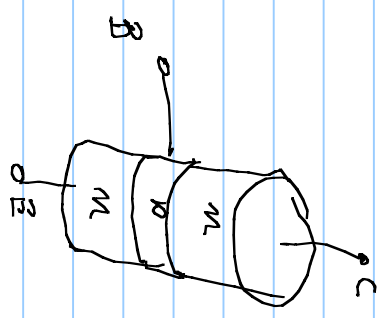
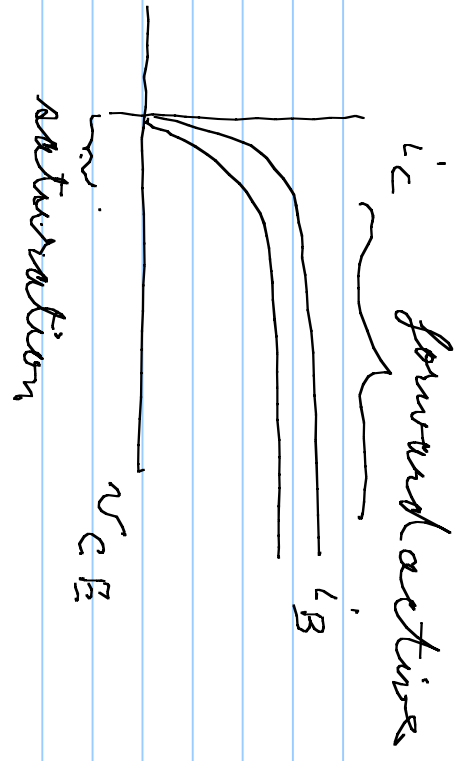
BJT = bipolar junction transistor



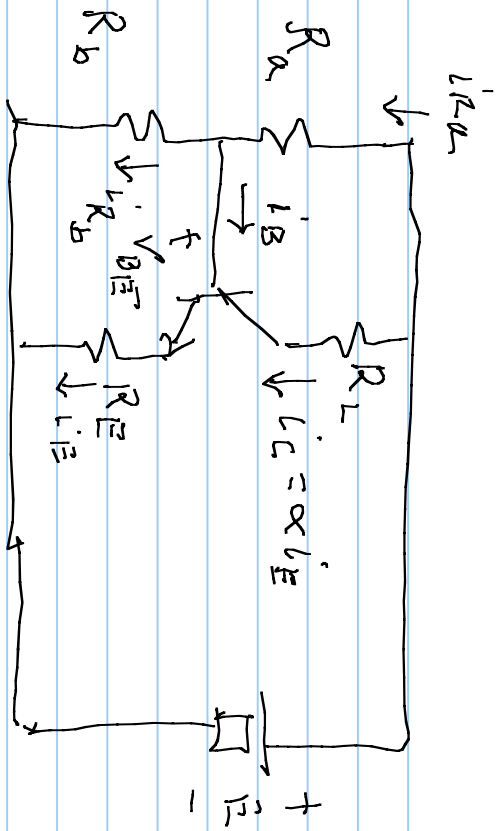
mpm



$$i_C \approx \beta i_B$$



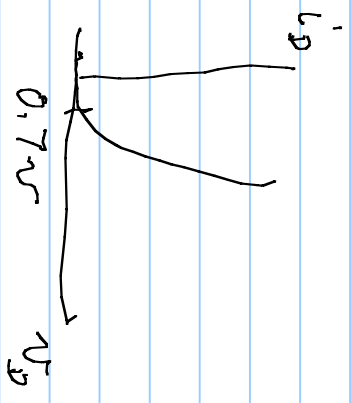
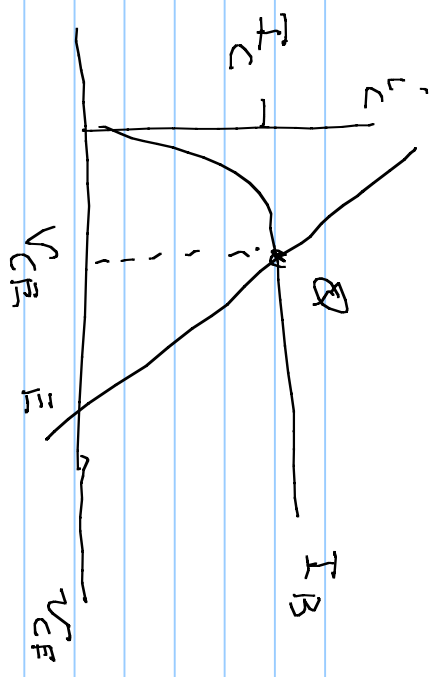
$i_C = -\alpha i_E$
 we take base, C-B diode
 & forward bias B-E diode



$$I_C + I_E + I_B = 0 \quad \text{by KCL}$$

$$I_C = \beta I_B \Rightarrow (\beta + 1) I_B = -I_E$$

$$\Rightarrow (\beta + 1) \frac{1}{\beta} I_C = -I_E$$



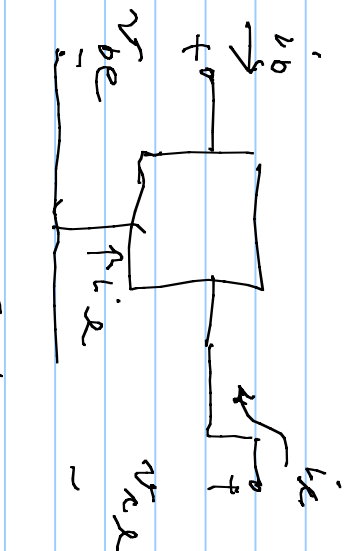
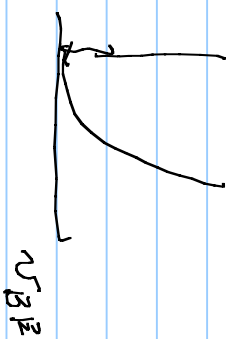
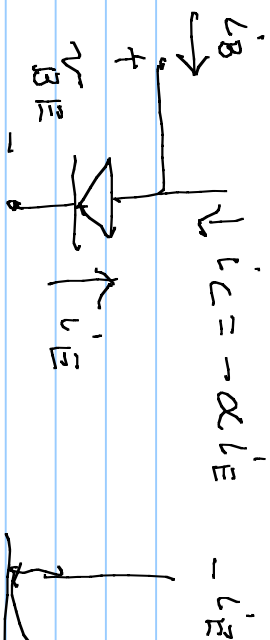
$$l'_C = -\frac{\beta}{\beta+1}, \quad l'_E = -\alpha l'_E, \quad \alpha = \frac{\beta}{1+\beta} \quad \text{if } \beta = 100 \Rightarrow \alpha = \frac{100}{101} \approx 0.98$$

Observing: need to find the Ricardian model constraints
 let look at Ricardian signals

$$l'_C = f(V_{CE}, l'_B) = I_C + \underbrace{\frac{\partial f}{\partial V_{CE}}}_{\substack{\text{Ricardian} \\ \text{signal}}} (V_{CE} - V_{CE}) + \underbrace{\frac{\partial f}{\partial l'_B}}_{\substack{\text{Ricardian} \\ \text{signal}}} (l'_B - I_B) + \dots$$

$$l'_E = l'_C - I_C = \theta_0 \cdot r_x + \beta \cdot l'_B$$

base to emitter



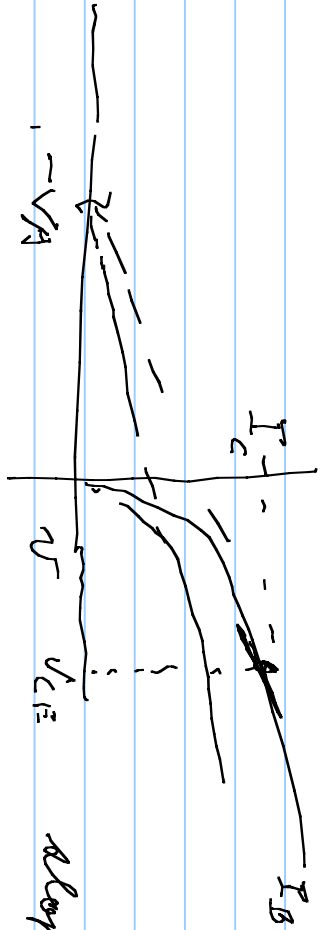
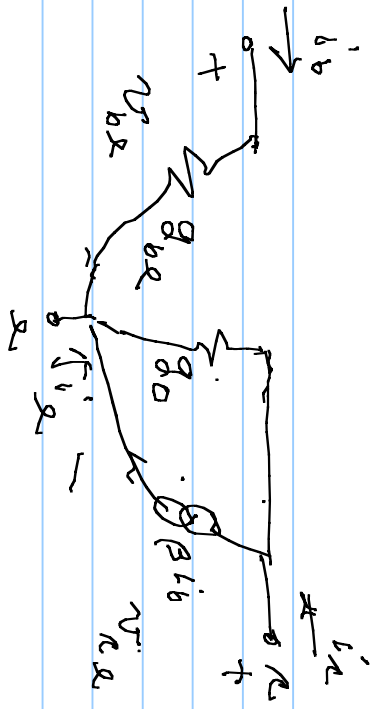
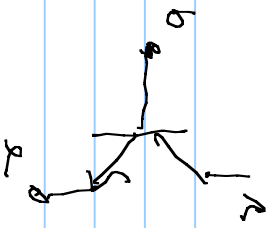
$$i_B = \frac{1}{\beta} i_C = -\frac{\alpha}{\beta} i_E \quad \text{but } \alpha = \frac{\beta}{\beta+1}$$

$$i_B = -\frac{\beta/(\beta+1)}{\beta} i_E = -\frac{1}{\beta+1} i_E \approx -\frac{1}{\beta} i_E$$

$$i_C = -i_E = I_S \left(e^{v_{BE}/V_T} - 1 \right) \approx I_S e^{v_{BE}/V_T} \approx \frac{i_C}{\alpha} \Rightarrow -i_E = \frac{I_C}{\alpha} v_{BE}$$

$$g_d = \frac{-i_E}{v_T} = + \frac{I_C}{\alpha v_T} \approx \frac{I_C}{v_T} \approx \beta \frac{I_B}{v_T} \Rightarrow i_b = g_{be} v_{be} \approx -\frac{\alpha}{\beta} i_e$$

we seen at the base $\Rightarrow i_b = \frac{\alpha}{\beta} \cdot \frac{I_C}{\alpha v_T} \cdot v_{be} = g_{be} v_{be} \Rightarrow g_{be} = g_d = \frac{I_C}{v_T} = \frac{g_m}{\beta}$



$V_A = \text{Early voltage}$

$$\text{slope} \approx \frac{I_C}{V_{CE} + V_A} \approx \frac{I_C}{V_A}$$

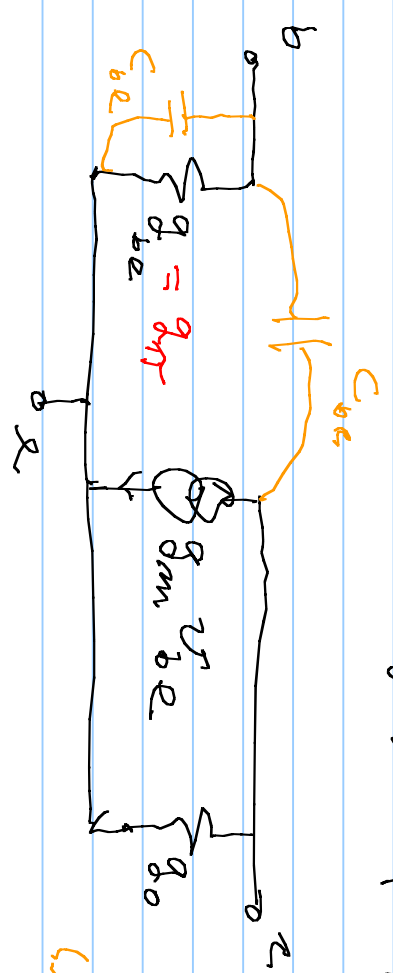
$$g_o \approx \frac{I_C}{V_{CE} + V_A}$$

$$\frac{\partial I_C}{\partial V_{CE}}$$

But $i_b = g_{be} \cdot v_{be} \Rightarrow \beta i_b = \beta g_{be} \cdot v_{be} \Rightarrow i_b = g_{be} v_{be}$

$i_c = \beta i_b = \beta g_{be} v_{be} \Rightarrow g_m = \frac{i_c}{v_{be}} = \beta g_{be}$

$g_m = \beta g_{be} \Rightarrow g_{be} = \frac{g_m}{\beta} = \frac{I_c}{\beta V_T}$



= π equivalent circuit

(hybrid π with ∞ load resistance)
 $i_{be} \rightarrow C_{be}$

$r_{\pi} = 1/g_{be} = \beta/g_m ; g_m = \frac{I_c}{V_T} \Rightarrow r_{\pi} = \frac{I_c}{\beta V_T}$

$$\text{if } I_C = 1 \text{ mA} \Rightarrow g_m = \frac{10^{-3}}{26 \times 10^{-3}} = \frac{1}{26} \text{ S}$$

$$I_B = I_C / \beta \quad \text{if } \beta = 100 \Rightarrow I_B = 10^{-5} \text{ A} = 10 \mu\text{A}$$

$$\text{Current gain} = 100$$