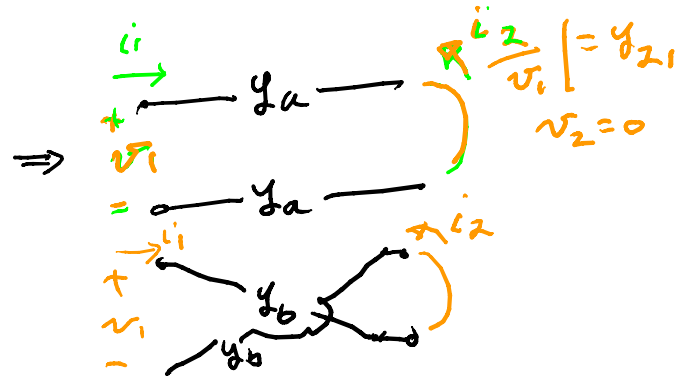
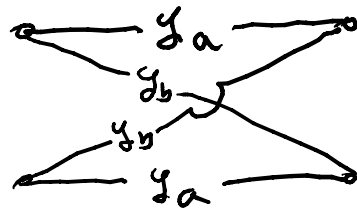


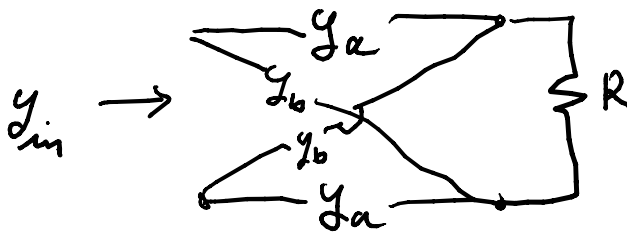
Lattice: (symmetric)



$$Y_a = \begin{bmatrix} Y_a/2 & -Y_a/2 \\ -Y_a/2 & Y_a/2 \end{bmatrix}$$

$$Y_b = \begin{bmatrix} Y_b/2 & +Y_b/2 \\ Y_b/2 & Y_b/2 \end{bmatrix}$$

$$\Rightarrow Y = \frac{1}{2} \begin{bmatrix} Y_b + Y_a & Y_b - Y_a \\ Y_b - Y_a & Y_b + Y_a \end{bmatrix}$$



$$Y_{in} = Y_{11} - Y_{12} \frac{1}{Y_{22} + G} Y_{21}$$

$$= \frac{\Delta Y + Y_{11} G}{Y_{22} + G} = G \left(\frac{Y_{11} + \frac{\Delta Y}{G}}{Y_{22} + G} \right)$$

$$\Delta = \left(\frac{Y_b + Y_a}{2} \right)^2 - \left(\frac{Y_b - Y_a}{2} \right)^2$$

$$= (Y_b^2 + Y_a^2 + 2Y_a Y_b - Y_b^2 - Y_a^2 + 2Y_a Y_b) / 4 = Y_a Y_b$$

$$Y_{in} = G \left(\frac{Y_{11} + Y_a Y_b / G}{Y_{11} + G} \right)$$

choose \$Y_a Y_b = G^2 \Rightarrow Y_{in} = G\$
gives the constant R lattice

$$\frac{Y_a}{G} = \frac{G}{Y_b} \Rightarrow \text{duals for the two arm types}$$

Look at the voltage transfer ratio: $-G \frac{V_2}{V_1} = i_2 = Y_{21} V_1 + Y_{22} V_2$

$$\frac{V_2}{V_1} = \frac{-Y_{21}}{Y_{22} + G} = \frac{-(Y_b - Y_a)/2}{(Y_b + Y_a)/2 + G}$$

$$\frac{v_2}{v_1} = \frac{y_a - y_b}{y_a + y_b + 2G} = \frac{G^2/y_b - y_b}{G^2/y_b + y_b + 2G} = \frac{G^2 - y_b^2}{y_b^2 + 2Gy_b + G^2}$$

$$= \frac{(G - y_b)(G + y_b)}{(G + y_b)^2} = \frac{G - y_b}{G + y_b} = \frac{1 - y_b/G}{1 + y_b/G} = A_v$$

$$1 - y_b/G = A_v + (y_b/G)A_v \Rightarrow (1 + A_v) \frac{y_b}{G} = 1 - A_v$$

$$\frac{y_b}{G} = \frac{1 - A_v}{1 + A_v}; \quad \text{Re}\left(\frac{y_b}{G}\right) = \text{Re}\left(\frac{1 - A_v}{1 + A_v}\right) \text{ in } \sigma > 0$$

$$= \frac{\text{Re}((1 - A_v)(1 + A_v)^*)}{|(1 + A_v)|^2}$$

$$= \frac{\text{Re}(1 - A_v + A_v^* - |A_v|^2)}{|(1 + A_v)|^2}$$

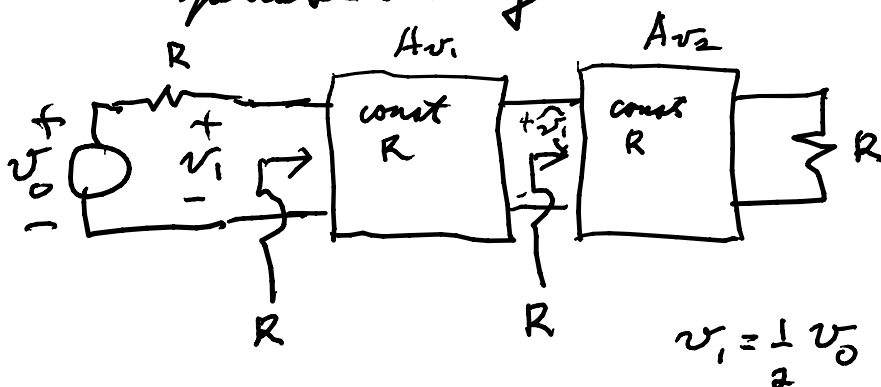
$$= \frac{1 - |A_v|^2}{|1 + A_v|^2} \quad \text{desired } > 0 \text{ in } \sigma > 0$$

for y_b/G to be PR

for y_b/G to be PR we need $|A_v| \leq 1$ in $\sigma \geq 0$

& then we can synthesize y_b (and y_a via the dual) by a passive. If lossless then can use Cauer or Foster forms. y_b will be lossless if $|A_v(j\omega)| = 1$

This will be an all-pass circuit \Rightarrow gives phase changes.



$$v_2 = A_{v2} \cdot \hat{v}_1 = A_{v2} \cdot A_{v1} \cdot v_1$$

$$A_v = A_{v2} \cdot A_{v1}$$

$$v_1 = \frac{1}{2} v_0$$

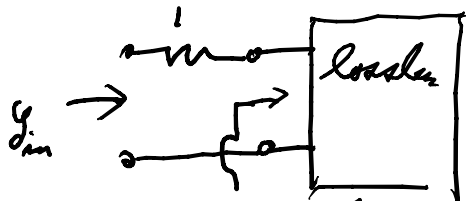
Look at Hurwitz polynomial

$$P(s) = \sum_{i=1}^n a_i s^i$$

(strictly Hurwitz if no zeros in $\sigma \geq 0$)

Hurwitz if all zeros are in $\sigma < 0$ & those on $\sigma = 0$, = jw axis, all simple

⇒ stable circuit, characteristic "functions"



$$\Rightarrow y_{in} = \frac{i \times y}{1 + y} \Rightarrow \text{denominator is Hurwitz}$$

$$y = \frac{\text{Od} \cdot P(s)}{\text{Ev} \cdot P(s)} = \frac{N}{D} = \frac{N/D}{1 + N/D} = \frac{N}{N + D} = \frac{N}{P(s)} \text{ Hurwitz}$$

$$= \frac{P(s) - P(-s)}{P(s) + P(-s)}$$

given $P(s)$ a Hurwitz polynomial

$$\text{Given } P(s) = \underbrace{\left(\frac{P(s) + P(-s)}{2} \right)}_{\text{Ev } P} + \underbrace{\left(\frac{P(s) - P(-s)}{2} \right)}_{\text{Od } P}$$

then divide $\frac{\text{Od } P}{\text{Ev } P} =$ a lossless admittance (reactance function & can synthesize)

Richard's function

8.2.61

$$R(s) = \frac{k z(s) - a z(k)}{k z(k) - a z(s)} \quad \text{eq. (8.6-1)}$$

is PR if $z(s)$ is PR & k is real $k > 0$

note a pole seems to be at $s = k$; $k z(k) - k z(k) = 0$

but at $s = k$ also have 0; $k z(k) - k z(k)$ which cancels.

Note δ seems to go up by 1 but we cancelled one pole & 0 ⇒ $\delta R \leq \delta z$

∴ desire to cancel another pole with another 0.

We choose k properly.

df $\sum z(a) = \frac{z(a) + z(-a)}{2}$, choose k , $\sum z(k) = 0$

$z(k) = -z(-k)$

$R(a) = \frac{kz(a) - kz(k)}{kz(k) - kz(a)} \Bigg|_{a=-k} \Rightarrow \frac{kz(-k) - (-k)z(k)}{kz(k) - (-k)z(-k)} = \frac{k(z(-k) + z(k))}{k(z(k) + z(-k))} = 0$

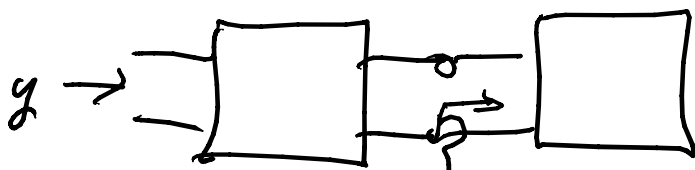
∴ there is no another pole & zero cancellation at $a = -k \Rightarrow \delta(R(a)) = \delta(z(a)) - 1$

∴ keep doing until $\delta(R_{...}(a)) = 0 \Rightarrow$ resistor (open or short)

∴ for lossless we can choose any k

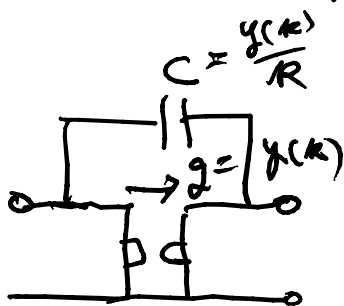
as the $y(a)$ or $z(a)$ has its even part $\equiv 0$ for all a .

∴ look for a circuit to given $y_{load}(a) =$ a Richards' function to synthesize a $y = y_{in}$



$y_L =$ a Richards' function

so $\delta(y_L) = \delta(y) - 1$



$Y = \begin{bmatrix} sC & -sC + g \\ -sC - g & sC \end{bmatrix}; \Delta Y = g^2$

$y_{in} = y_{11} - y_{12} \frac{1}{y_{22} + y_L} y_{21} = \frac{\Delta Y + y_{11} y_L}{y_{22} + y_L} = \frac{g^2 + sC y_L}{sC + y_L}$

$y_{in} sC + y_{in} y_L = g^2 + sC y_L$

$y_L = \frac{g^2 - sC y_{in}}{y_{in} - sC} = \frac{g^2 - sC y(a)}{y(a) - sC} = g^2 \left(\frac{1 - \frac{sC}{g^2} y(a)}{\frac{y(a) - sC}{y(a)}} \right)$

$\frac{y_L}{g} = \left(1 - \frac{sC}{g^2} y(a) \right) \Bigg| \left(\frac{y(a)}{g} - sC/g \right)$

In Richards' function replace $z(z) = \sqrt{y(z)}$

$$R(z) = \frac{k y(z) - a y(z)}{k y(z) - a y(z)} = y(z) \cdot k \left(1 - \frac{a}{k} \cdot \frac{y(z)}{y(z)} \right) = \frac{k \left(y(z) - \frac{a}{k} y(z) \right)}{k \left(y(z) - \frac{a}{k} y(z) \right)} =$$

$$= \left(\frac{1 - \frac{a}{k} \cdot \frac{y(z)}{y(z)}}{\frac{y(z)}{y(z)} - \frac{a}{k}} \right)$$

$$\frac{a}{k y(z)} = \frac{aC}{g^2} \quad \& \quad \frac{a}{k} = \frac{aC}{g}$$

$$\Rightarrow g = y(z), \quad C = \frac{g}{k} = \frac{y(z)}{k}$$

$$= \frac{y(z)}{g} = \left(\frac{1 - \frac{aC}{g^2} y(z)}{\frac{y(z)}{g} - \frac{aC}{g}} \right)$$

$$\Rightarrow \text{form } y_L(z) = g R(z) = y(z) \left(\frac{k y(z) - a y(z)}{k y(z) - a y(z)} \right)$$