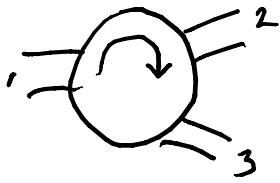


3-port circulator

EE610
09/23/10



$$V^n = \begin{bmatrix} V_1^n \\ V_2^n \\ V_3^n \end{bmatrix} = S V^i = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} V_1^i \\ V_2^i \\ V_3^i \end{bmatrix}$$

$$b = Sa$$

$$S_{\text{circ}} = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}$$

$$I_3 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} = I_3 - S_{\text{circ}}^T S_{\text{circ}} = I_3 - \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} = 0_3$$

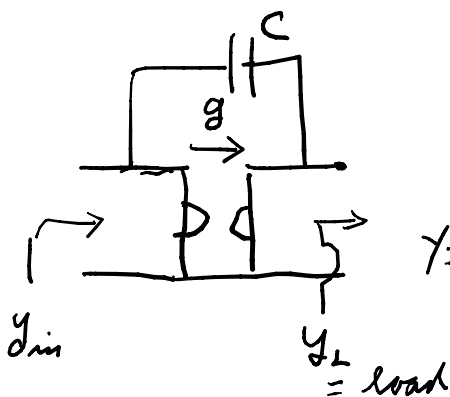
$$S_{\text{circ}}^{-1} = S_{\text{circ}}^T$$

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Next Richards' functions \Rightarrow gives a positive real function of a positive real function
 immittance = γ or a Z

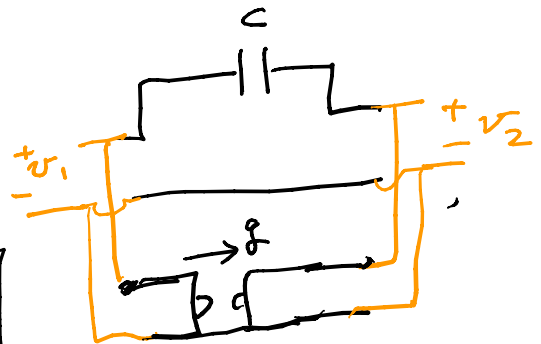
for a passive circuit an immittance is positive real

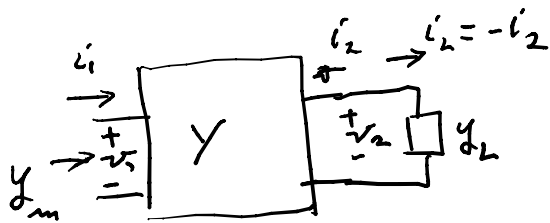
we will use for passive synthesis



$$\gamma_{in} + \gamma_c = \gamma$$

$$\gamma = \begin{bmatrix} C\alpha & -C\alpha + g \\ -C\alpha - g & C\alpha \end{bmatrix}$$





$$-\mathbf{I}_2 = \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$\downarrow$$

$$-y_L v_2$$

$$-y_L v_2 = y_{21} v_1 + y_{22} v_2 \Rightarrow v_2 = -(y_L + y_{22})^{-1} y_{21} v_1$$

$$\mathbf{I}_1 = y_{11} v_1 + y_{12} v_2 = y_{11} v_1 - y_{12} (y_L + y_{22})^{-1} y_{21} v_1$$

$$\mathbf{I}_1 = y_{in} v_1$$

$$\Rightarrow y_{in} = y_{11} - y_{12} (y_L + y_{22})^{-1} y_{21}$$

determinant

as y_{22} is a scalar for Y 2×2 ,

$$y_{in} = \frac{y_{11} y_L + y_{11} y_{22} - y_{12} y_{21}}{y_L + y_{22}} = \frac{y_{11} y_L + \Delta Y}{y_L + y_{22}}$$

here $\begin{vmatrix} c_a & -c_a + g \\ -c_a - g & c_a \end{vmatrix} = (c_a)^2 - (-c_a + g)(-c_a - g) = g^2$

for our C "loaded" gyrator

$$y_{in} = \frac{c_a y_L + g^2}{y_L + c_a} \Rightarrow y_{in} y_L + y_{in} c_a = c_a y_L + g^2$$

$$(y_{in} - c_a) y_L = g^2 - y_{in} c_a$$

$$y_L = \frac{g^2 - c_a y_{in}}{y_{in} - c_a}$$

$$= \frac{(g^2/c) - A y_{in}(c)}{(\frac{1}{c}) y_{in}(c) - A}$$

see p. 361 for a Richards' function

$$F(a) = \frac{kz(a) - Az(k)}{kz(k) - Az(a)}$$

$$R_2(a) = \frac{kz(a) - Az(k)}{kz(k) - Az(a)}$$

change $R_2(s)$ into $y(s)R_2(s) = \frac{ky(s) - ay(s)}{\frac{k}{y(s)}y(s) - a}$

identify y_L with $y(s)R_2(s)$

$y = y_{in}$ 1)

$ky(s) = g^2/c$ 2)

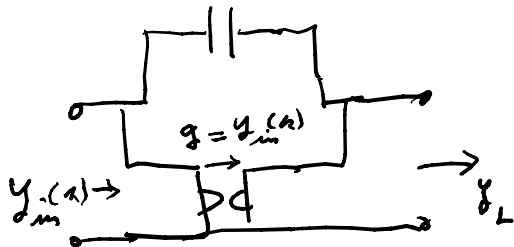
$\frac{k}{y(s)} = \frac{1}{c}$ 3)

3) $c = \frac{y(k)}{k}$

2) $ky(k) = g^2/c$

$= g^2 \cdot \frac{k}{y(k)} \Rightarrow g^2 = y_{in}^2(k)$

$c = y_{in}(k)/k$



choose $k =$ zero of even part of $y_{in}(s)$ then

$\delta[y_L] = \delta[y_{in}] - 1$

degree

$2E - y(s) = y(s) + y(-s)$ if $s=k$ is a zero of this

$y(k) = -y(-k)$

$y_L(s) = y_{in}(s) \left[\frac{ky(k) - ay_{in}(s)}{ky(s) - ay_{in}(s)} \right] = y_{in}(s) \left[\frac{ky(s) - (-k)y_{in}(-s)}{ky(-s) - (-k)y_{in}(s)} \right]$

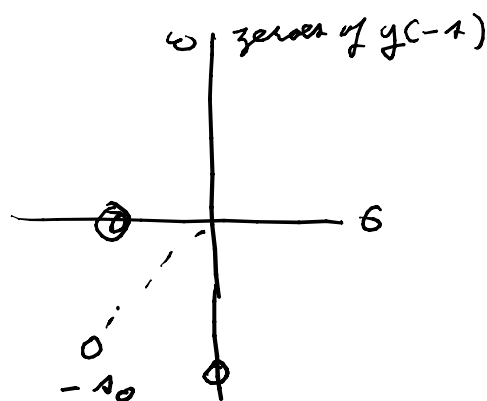
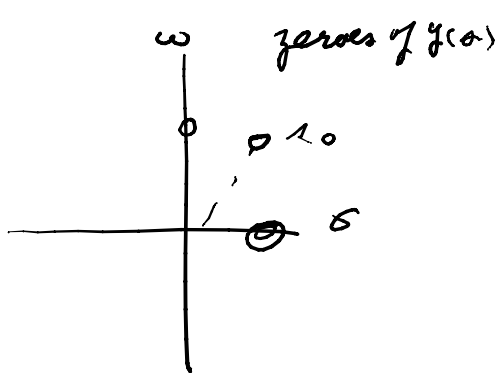
evaluate

at $s = -k$
 $= y_{in}(s) \left[\frac{ky(s) + ky_{in}(-s)}{0} \right]$

$\therefore s-k \approx s+k = 0/0$

both cancel numerator & denominator

\therefore choose $k =$ a zero of $E - y_{in}(s) = \frac{y(s) + y(-s)}{2}$



$$P_{ave} = \operatorname{Re} V(j\omega)^T I(j\omega) = \operatorname{Re} [V(j\omega)^T [y(j\omega) V(j\omega)]]$$

SSS
sinusoidal steady state

$$= \operatorname{Re} y(j\omega) \cdot V(j\omega)^* V(j\omega) \text{ for a 1-port}$$

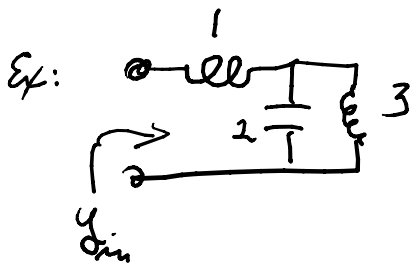
$$= \frac{1}{2} (y(j\omega) + y(-j\omega)) |V|^2$$

↑ if real coeff
 $y^*(j\omega)$

if lossless $P_{ave}(j\omega) = 0$

$y(j\omega) + y(-j\omega) \equiv 0$ for almost all ω
 this has $y(j\omega)$ analytic in $\sigma > 0$ so can extend $y(j\omega)$ to $\sigma > 0$ by $\omega = s/j$

$$y(s) + y(-s) = 0 \text{ identically}$$



$$\Rightarrow y_{in} = \frac{1}{3_{in}} = \frac{1}{2 + \frac{1}{2s + \frac{1}{3s}}} = \frac{1}{2 + \frac{3s}{6s^2 + 1}} = \frac{6s^2 + 1}{6s^2 + 4s}$$

$$= \frac{1}{2} \left(\frac{6s^2 + 1}{6s^2 + 4s} \right)$$

$$y_{in}(s) + y_{in}(-s) = \frac{1}{2} \left(\frac{6s^2 + 1}{6s^2 + 4s} \right) - \frac{1}{2} \left(\frac{6s^2 + 1}{6s^2 + 4s} \right) \equiv 0$$

∴ any complex k is a zero of $E_r y(a)$

$$C = \frac{y(k)}{k} = \frac{1}{k^2} \left(\frac{6k^2 + 1}{6k^2 + 4} \right)$$

Choose $k=2$ is a real zero of $E_r y(a) \Rightarrow C = \frac{1}{4} \left(\frac{25}{28} \right)$

$$g = y(k) = \frac{1}{2} \left(\frac{25}{28} \right)$$

$$y_{\partial_L} = y(a) \frac{ky(a) - ay(k)}{ky(a) - ky(k)}$$

we know that the polynomial $(a-k)(a+k) = a^2 - k^2 = a^2 - 4$ cancels in numerator & denominator

$$= \frac{1}{2} \left(\frac{25}{28} \right) \left[\frac{2 \left(\frac{1}{2} \right) \left(\frac{25}{28} \right) - \frac{6a^2 + 1}{6a^2 + 4}}{2 \frac{1}{2} \left(\frac{6a^2 + 1}{6a^2 + 4} \right) - \frac{a}{2} \left(\frac{25}{28} \right)} \right] = \frac{1}{2} \frac{25}{28} \left[\frac{\frac{25}{28}(6a^2 + 4) - (6a^2 + 1)}{\frac{a}{2}(6a^2 + 1) - \frac{a}{2} \left(\frac{25}{28} \right) (6a^2 + 4)} \right]$$

$$= \frac{1}{2} \frac{25}{28} a \left[\frac{6 \left(\frac{25}{28} - 1 \right) a^2 + \left(\frac{25}{28} \cdot 4 - 1 \right)}{-3 \left(\frac{25}{28} \right) a^4 + 12a^2 - 2 \left(\frac{25}{28} \right) a^2 + 2} \right]$$

$$= \frac{1}{2} \left(\frac{25}{28} \right) a \left[\frac{-\frac{18}{28} a^2 + \frac{72}{28}}{-\frac{75}{28} a^4 - \frac{236}{28} a^2 + \frac{56}{28}} \right] = \frac{-\frac{18}{28} (a^2 - 4) a}{(a^2 - 4)(-1) \left(\frac{75a^2 + 4}{28} \right)}$$

$$a^2 - 4 \left[\frac{-75a^4 + 286a^2 + 56}{-75a^4 + 300a^2} \right] = \frac{-75a^2 - 4}{-147a^2 + 56}$$

$$y_{\partial_L} = \frac{18}{28} a \frac{1}{(75a^2 + 4)(28)} = \frac{18a}{75a^2 + 4}$$

100
-27

12-50
28
12
56
18

300
-28