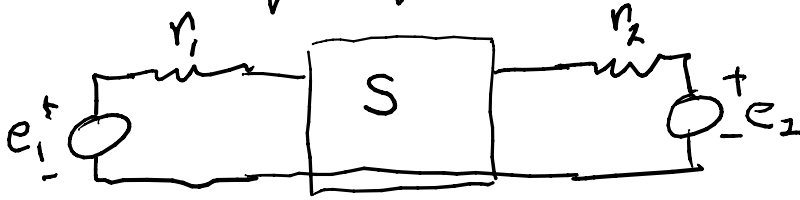


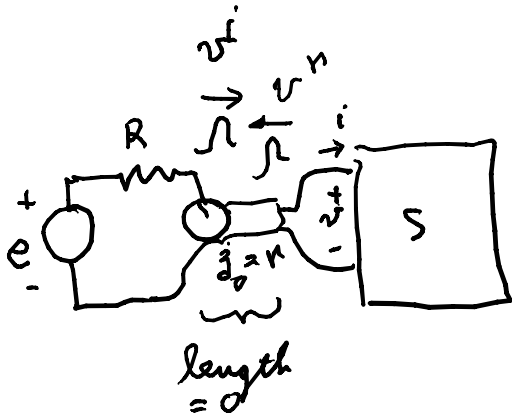
EE 610  
09/16/10 → 09/17/10

Scattering matrix  
(useful for microwaves, wireless)



$$R = r_1 r_2$$

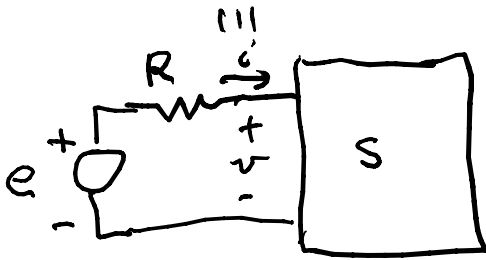
$$V = r_1 = r_2$$



$$v^r = S v^i$$

$$e = v + Ri = 2\sqrt{R} a = 2v^i$$

$$v - Ri = 2\sqrt{R} b = 2v^r$$

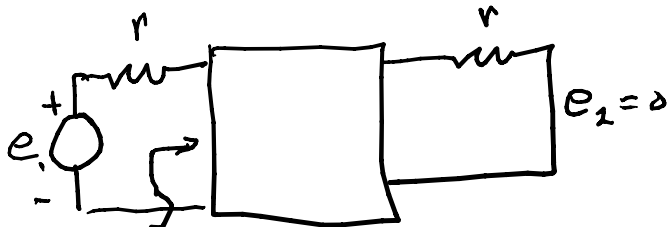


$$b = S a \equiv v^r = S v^i$$

$$\begin{bmatrix} b_1 \\ b_2 \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \end{bmatrix}$$

$$S_{11} = \left. \frac{b_1}{a_1} \right|_{a_2=0} = \frac{v_r - r l_1}{(2\sqrt{r})(v_i + r l_1)} \cdot \frac{1}{2\sqrt{r}}$$

$$= \frac{v_r - v_i}{v_i + r l_1}$$



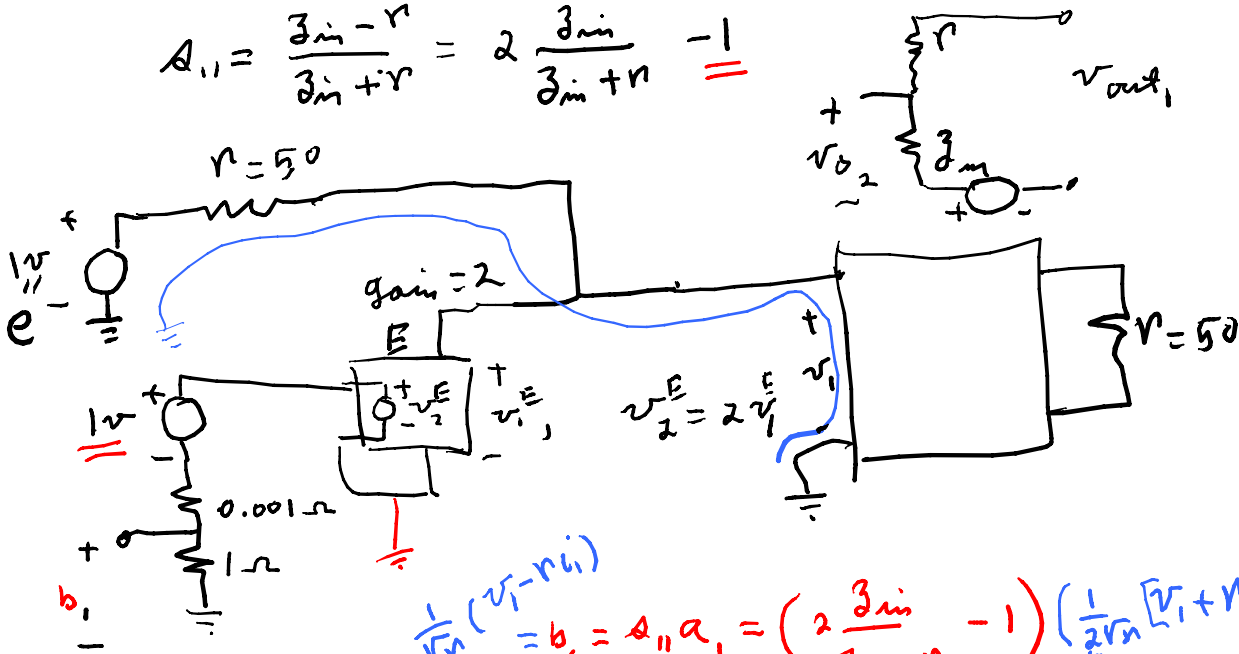
$$v_i = Z_{in} i_1 \quad | \quad e_2 = 0$$

if  $Z_{in}$  for the loaded 2-port exists

$$S_{11} = \frac{(v_i / i_1 - r) i_1}{(v_i / i_1 + r) i_1}$$

$$= \frac{Z_{in} - r}{Z_{in} + r} ; r = Z_0$$

$$A_{11} = \frac{3i_{in} - r}{3i_{in} + r} = 2 \frac{3i_{in}}{3i_{in} + r} - 1 = -1$$



$$\frac{1}{2r} (v_1 - r i_1) = b_1 = A_{11} a_1 = \left( 2 \frac{3i_{in}}{3i_{in} + r} - 1 \right) \left( \frac{1}{2r} [v_1 + r i_1] \right)$$

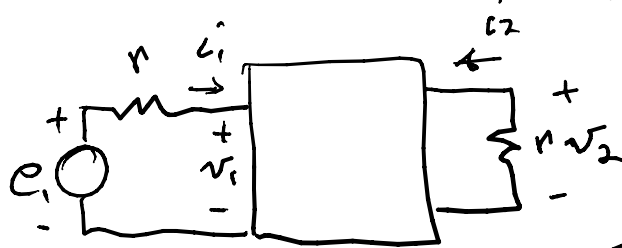
$\downarrow$   
 $v_1 - r i_1$

$\downarrow$   
 $e = 1V$

gives  $A_{11}$  as the voltage on the  $1\Omega$  resistor

since the input to E is  $v_{in}$   $3i_{in}$  and the output at  $b_1$  is  $2v_{in} i_{in}^{-1}$   
for 1V for  $e \Rightarrow$   
 $v_{out} = \frac{3i_{in}}{r} \times 1$   
 $\Rightarrow$  V for  $b_1$  is  $\frac{2 \cdot 3i_{in}}{r} \times 1 - 1$   
/09/17

For  $A_{21}$ :  $A_{21} = \frac{b_2}{a_1} = \frac{v_2^r}{v_1^i}$   
 $a_2 = v = v_2^i$



$$2v_2^r = v_2 - r i_2 = 2v_2$$

but  $v_2 = -r i_2$

$$e_1 = v_1 + r i_1 = 2v_1^i$$

$$A_{21} = \frac{v_2^r}{v_1^i} = \frac{2v_2}{e_1/2} = \frac{2}{4} \frac{v_2}{e_1} = 2 \times \text{terminated voltage gain}$$

Reference Cadence

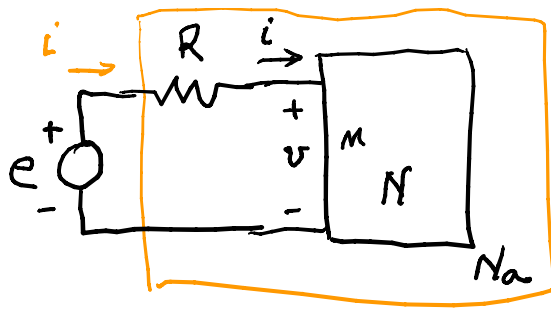
application note:

[http://www.cadence.com/rel/Resources/application\\_notes/S-Parameter\\_Data\\_application.pdf](http://www.cadence.com/rel/Resources/application_notes/S-Parameter_Data_application.pdf)

needs ground on E component

&  $\sqrt{Z}$  in eqs. (1)-(4) is best as  $\sqrt{Z_0}$

or even set to 1. [E component of Spice = voltage controlled voltage source]



$$e \Rightarrow i = Y_a e$$

$$e = v + Ri = v + RY_a e$$

$$\left. \begin{aligned} (1_m - RY_a)e &= v \\ Y_a e &= i \end{aligned} \right\}$$

choose  $R = \mathbb{1}_m \Rightarrow RY_a = Y_a R$

$$Y_a (1_m - RY_a) e = Y_a v$$

$$(1_m - RY_a) Y_a e = (1_m - RY_a) i$$

$$(Y_a - Y_a R Y_a) e$$

$$(Y_a - R Y_a Y_a) e = (Y_a - Y_a R Y_a) e \Rightarrow Y_a v = (1_m - R Y_a) i$$

$$A v = B i \Rightarrow A = Y_a, B = 1_m - R Y_a = 1_m - Y_a R$$

$$\text{But } \left. \begin{aligned} 2v^i &= v + Ri \\ 2v^n &= v - Ri \end{aligned} \right\} \left. \begin{aligned} 2v &= 2v^i + 2v^n \\ 2Ri &= 2v^i - 2v^n \end{aligned} \right\} \left. \begin{aligned} v &= v^i + v^n \\ Ri &= v^i - v^n \end{aligned} \right\}$$

$$A v = B i \Rightarrow A(v^i + v^n) = (BR^{-1})(\underbrace{v^i - v^n}_{Ri})$$

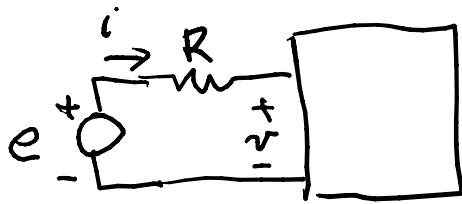
$$(A - BR^{-1})v^i = -(A + BR^{-1})v^n$$

$$v^n = (BR^{-1} + A)^{-1} (BR^{-1} - A) v^i$$

$$S = (BR^{-1} + A)^{-1} (BR^{-1} - A)$$

$$= (R^{-1} - RY_a R^{-1} + Y_a)^{-1} (R^{-1} - RY_a R^{-1} - Y_a)$$

$$= R(R^{-1} - 2Y_a) = 1_m - 2RY_a$$



$$e = v + Ri$$

$$p(t) = v^T i(t)$$

$$e^T i(t) = (v + Ri)^T (v + Ri) = v^T v(t) + \underbrace{i^T R v}_{+ i^T R R i} + \underbrace{v^T R i}$$

$$(i^T R v)^T = i^T R v = v^T R i$$

$$e^T e = \underbrace{v^T v}_{\Sigma 1 \text{ sys.}} + \underbrace{(Ri)^T Ri}_{\Sigma 1 \text{ sys.}} + \underbrace{2 v^T R i}_{2 v^T i \text{ sys.}} = \underbrace{2 v^T i}_{p(t)}$$

$$\int_{-\infty}^t e^T e(\tau) d\tau = \int_{-\infty}^t v^T v(\tau) d\tau + \int_{-\infty}^t (Ri)^T Ri + 2 \int_{-\infty}^t p(\tau) d\tau$$

if finite  $\Rightarrow e_i \in L_2$   $\Rightarrow v_i \in L_2$   $\Rightarrow i_i \in L_2$  if passive  $\geq 0$

$\Rightarrow$  eventually  $\Rightarrow S(s)$  is bounded-real for a passive  $N$