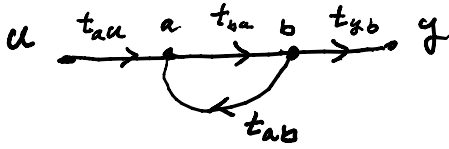


Feedback



$$\begin{aligned} x_b &= t_{ba} x_a & 1) \\ x_a &= t_{au} u + t_{ab} x_b & 2) \\ y &= t_{yb} x_b & 3) \end{aligned}$$

2)  $\times t_{ba}$  & 1)

$$t_{ba} x_a = x_b = t_{ba} t_{au} u + t_{ba} t_{ab} x_b \quad \text{solve for } x_b$$

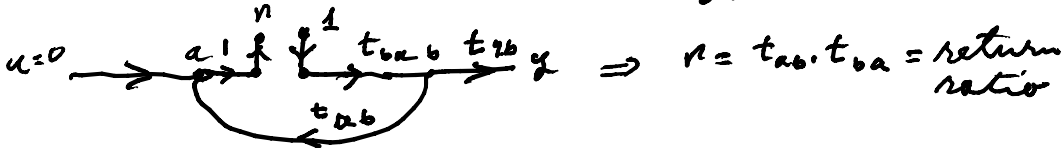
$$x_b = (1 - t_{ba} t_{ab})^{-1} t_{ba} t_{au} u$$

3)

$$y = t_{yb} (1 - t_{ba} t_{ab})^{-1} t_{ba} t_{au} u$$

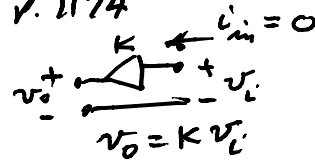
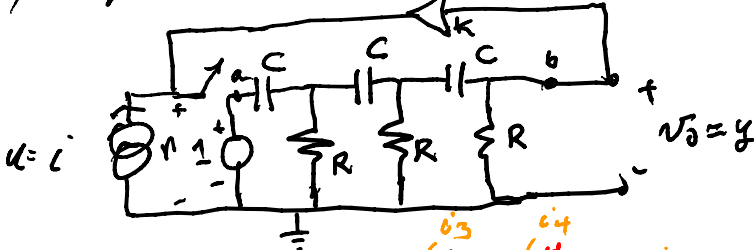
$$T = t_{yb} (1 - t_{ba} t_{ab})^{-1} t_{ba} t_{au}$$

For the return ratio & return difference:



$$\begin{aligned} d &= 1 - r = \text{return difference} \\ &= 1 - t_{ab} t_{ba} \Rightarrow \text{in denominator of } T \\ &\quad \text{its zeros give the poles of } T \end{aligned}$$

Example: phase shift oscillator, p. 1174



2-port  $Y = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix}$ ; port 1 = a/1

port 2 = b/1

$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = Y \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} v_{in} \\ v_0 \end{bmatrix}$$

derive  $\frac{v_0}{v_{in}} \Big|_{i_2=0}$   
 $i_2 = 0 = \text{amplifier current input}$

$$0 = y_{21} v_1 + y_{22} v_2 \Rightarrow \frac{v_2}{v_1} = -y_{21}/y_{22}$$

$$G = 1/R$$

$\neq 0$

one way: find indefinite  $Y$ , move  $\frac{1}{s}$  to node 5  
(5x5)

Other  $Y_{indef}$  = find the currents into the 5 nodes when short voltage sources from nodes to  $\frac{1}{s}$

$$= \begin{bmatrix} sC & 0 & -sC & 0 & 0 \\ 0 & sC+G & 0 & -sC & -G \\ -sC & 0 & 2sC+G & -sC & -G \\ 0 & -sC & -sC & 2sC+G & -G \\ 0 & -G & -G & -G & 3G \end{bmatrix} \quad \begin{array}{l} \text{row 5} = 0 \\ \text{col 5} = 0 \end{array} \quad \text{quite singular}$$

move ground to node 5  $\rightarrow v_5 = 0$  & ignore  $i_5$  as it sums all other currents  
scratches out the rows & columns associated with the ground node:

$$Y_{def} = \left[ \begin{array}{cc|cc} sC & 0 & -sC & 0 \\ 0 & sC+G & 0 & -sC \\ \hline -sC & 0 & 2sC+G & -sC \\ 0 & -sC & -sC & 2sC+G \end{array} \right] = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \quad \begin{array}{l} \text{next for } i_3 = i_4 = 0 \\ \text{all } Y_{ij} \text{ are } 2 \times 2 \end{array}$$

$$\begin{bmatrix} i_1 \\ i_2 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \end{bmatrix} \Rightarrow \begin{bmatrix} 0 \\ 0 \end{bmatrix} = Y_{21} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + Y_{22} \begin{bmatrix} v_3 \\ v_4 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} v_3 \\ v_4 \end{bmatrix} = -Y_{22}^{-1} Y_{21} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \quad \text{if } Y_{22}^{-1} \text{ exists}$$

$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = Y_{11} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + Y_{12} (-Y_{22}^{-1} Y_{21}) \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}; \quad \underline{Y_{2port} = Y_{11} - Y_{12} Y_{22}^{-1} Y_{21}}$$

need  $Y_{22}^{-1}$ :  $\det \begin{bmatrix} 2sC+G & -sC \\ -sC & 2sC+G \end{bmatrix} = 4s^2C^2 + 4sCG + G^2 - s^2C^2 = 3s^2C^2 + 4sCG + G^2$

$$Y_{21} \text{ \& } Y_{22} \quad Y_{2port} = \frac{\begin{bmatrix} sC & 0 \\ 0 & sC+G \end{bmatrix} - \begin{bmatrix} -sC & 0 \\ 0 & -sC \end{bmatrix} \begin{bmatrix} 2sC+G & sC \\ sC & 2sC+G \end{bmatrix} \begin{bmatrix} -sC & 0 \\ 0 & -sC \end{bmatrix}}{3s^2C^2 + 4sCG + G^2}$$

$$\text{return ratio} = -\frac{Y_{21}}{Y_{22}} \Big|_{\substack{v_2=0 \\ i_2=0}} = \frac{-[-sC^3] / \det}{(sC+G)[3s^2C^2 + 4sCG + G^2] - (s^2C^3)(2sC+G)} = \frac{1}{K}$$

When we close the loop desire  $d = 1 - N$

desire zero of  $d$  to get poles of transfer function

$$d = 1 - \frac{[+sC^3K]}{(sC+G)[3s^2C^2 + 4sCG + G^2] - s^2C^2(2sC+G)} = \frac{aA^3 + \dots}{bA^3 + \dots}$$

desire the numerators to have a factor  $s^2 + \omega_0^2$   
 (without the feedback all zeros are on the negative  
 real axis so the RC ladder will not oscillate)

Problem: To control the amplitude? How?

Look at the Van der Pol oscillator

$$\ddot{x} + \epsilon(x^2 - 1)\dot{x} + \omega_0^2 x = 0$$

this one is a  
 structurally stable  
 oscillator

1) Let  $\frac{dy}{dt} = \omega_0^2 x$

2)  $\frac{d^2x}{dt^2} + \epsilon(x^2 - 1)\frac{dx}{dt} = -\omega_0^2 x = -\frac{dy}{dt}$

integrate 2)

3)  $\frac{dx}{dt} + \epsilon\left(\frac{x^3}{3} - x\right) = -y$

$$\left\{ \begin{array}{l} \frac{dy}{dt} = \omega_0^2 x \\ \frac{dx}{dt} = -y + \epsilon\left(x - \frac{x^3}{3}\right) \end{array} \right\} \text{state equations}$$