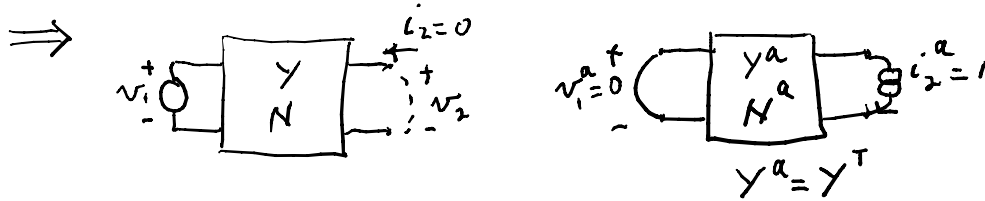
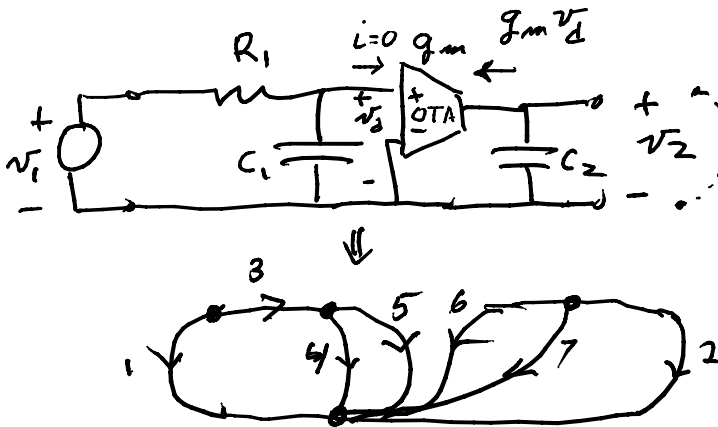


$\therefore \text{set } i_2^a = 1 \Rightarrow \Delta v_2 = v_0^{aT} \Delta Y v_0$



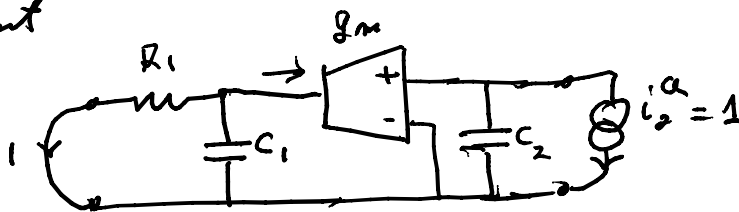
$S_x^{T(a)}$ = sensitivity of $T(a)$ = transfer function to the parameter x
 = % change in $T(a)$ vs % change in x (in differential form)
 = $\frac{x}{T(a)} \frac{dT(a)}{dx}$ will get $\frac{dT(a)}{dx}$ from the circuits using the adjoint



$$Y_{OTA} = \begin{bmatrix} 0 & 0 \\ g_m & 0 \end{bmatrix}$$

$$Y_{OTA}^a = Y_{OTA}^T = \begin{bmatrix} 0 & g_m \\ 0 & 0 \end{bmatrix}$$

\Rightarrow adjoint



if we desire $S_{g_m}^{v_2/v_1}$; need $\frac{v_2}{v_1}(a)$ use $v_1 = 1v$

$$v_d = \frac{1/AC_1}{R_1 + 1/AC_1} \cdot v_1 = \frac{1}{1 + AR_1C_1} \cdot v_1, \quad v_2 = -g_m v_d \cdot \frac{1}{AC_2}$$

$$v_2 = -\frac{g_m}{AC_2} \cdot \frac{1}{1 + AR_1C_1} \cdot v_1 \Rightarrow \frac{v_2}{v_1} = \frac{-g_m}{AC_2(1 + AR_1C_1)}$$

$$S_{g_m}^{v_2/v_1} = \frac{v_2/v_1}{g_m} \cdot \frac{d(v_2/v_1)}{dg_m} = \frac{g_m}{-g_m} \cdot \frac{-1}{AC_2(1 + AR_1C_1)} = 1$$

$$Y_{b \times b} = \begin{bmatrix} G_1 & 0 & 0 & 0 & 0 \\ 0 & AC_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & g_m & 0 & 0 \\ 0 & 0 & 0 & 0 & AC_2 \end{bmatrix} \begin{matrix} \leftarrow v_3 \\ \vdots \\ \leftarrow v_7 \end{matrix} \quad G_1 = 1/R_1$$

$\Delta Y_{b \times b}$ when change $g_m \rightarrow \Delta g_m$

$$\Delta Y_{b \times b} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \Delta g_m & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \text{desire } v_b^a \Delta Y_{b \times b} v_b$$

$$= v_b^a \Delta g_m v_b$$

$$\Delta v_2 = [v_{b_3}^a \ v_{b_4}^a \ v_{b_5}^a \ v_{b_6}^a \ v_{b_7}^a] \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & \Delta g_m & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} v_{b_3} \\ v_{b_4} \\ v_{b_5} \\ v_{b_6} \\ v_{b_7} \end{bmatrix} = v_{b_6}^a \cdot \Delta g_m \cdot v_{b_5}$$

$$\frac{\Delta v_2}{\Delta g_m} = v_{b_6}^a \cdot v_{b_5}$$

$$= \frac{\Delta(v_2/v_1)}{\Delta g_m} = \frac{d(v_2/v_1)}{dg_m} \quad \therefore \text{solve } N \text{ for } v_{b_5} \text{ \& } N^a \text{ for } v_{b_6}$$

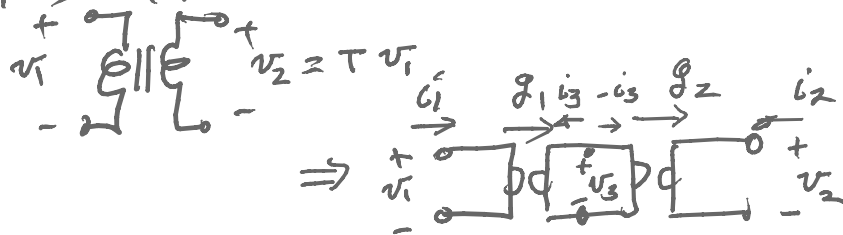
$$\text{but } v_{b_5} = v_d = \frac{1/AC_1}{R_1 + 1/AC_1} \cdot v_1 = \frac{1}{1 + AR_1C_1}$$

$$\& \ v_{b_6}^a = -\frac{1}{AC_2} \cdot \frac{1}{1 + AR_1C_1} = -\frac{1}{AC_2}$$

\therefore by solving N & N^a we get $\frac{d(v_2/v_1)}{dg_m} = v_{b_6}^a \cdot v_{b_5} = -\frac{1}{AC_2} \cdot \frac{1}{1 + AR_1C_1}$
(which was what got by direct calculation!)

If no admittance $Y_{b \times b}$ of the internal circuit can make replacements (usually, can use gyrators), to form the adjoint

$$i_1 \rightarrow 1: T \leftarrow i_2 \Rightarrow i_1 + T i_2 = 0 \Rightarrow i_1 = -T i_2$$



$$\begin{bmatrix} i_1 \\ i_3 \end{bmatrix} = \begin{bmatrix} 0 & g_1 \\ -g_1 & 0 \end{bmatrix} \begin{bmatrix} v_1 \\ v_3 \end{bmatrix}, \quad \begin{bmatrix} -i_3 \\ i_2 \end{bmatrix} = \begin{bmatrix} 0 & g_2 \\ -g_2 & 0 \end{bmatrix} \begin{bmatrix} v_3 \\ v_2 \end{bmatrix}$$

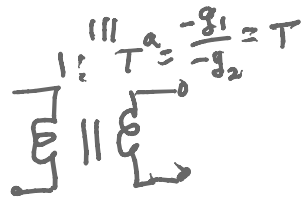
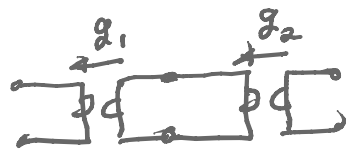
$$i_1 = g_1 v_3 \quad \& \quad -i_3 = g_2 v_3 \Rightarrow v_3 = -\frac{1}{g_2} i_2$$

$$\Rightarrow i_1 = -\frac{g_1}{g_2} i_2 \text{ looks like } T = \frac{g_1}{g_2}$$

$$i_3 = -g_1 v_1 \quad \& \quad -i_3 = g_2 v_2 =$$

$$\Rightarrow -g_1 v_1 = -g_2 v_2 \Rightarrow \frac{v_2}{v_1} = \frac{g_1}{g_2} = T$$

the adjoint



$$\text{as } Y_{gym} = \begin{bmatrix} 0 & g \\ g & 0 \end{bmatrix},$$

$$Y_{gym}^a = Y_{gym}^T = \begin{bmatrix} 0 & -g \\ g & 0 \end{bmatrix}$$

= turned around gyrator

Next: Design of transfer functions by setting up state-variable equations (do for single input single output); do for linear time-invariant; no pole at $\infty = a$.

$$\begin{aligned} \dot{x} &= Ax + Bu & T(s) &= \frac{y(s)}{u(s)} = D + C(AI_n - A)^{-1}B \\ y &= Cx + Du \end{aligned}$$

\therefore create C, B, D, A from $T(s)$ $n = \#$ of state variable

given $T(s) = \frac{y(s)}{u(s)} = d + \frac{\sum_{i=0}^{m-1} c_i s^i}{\sum_{i=0}^m a_i s^i}$ \therefore know d, c_i, a_i
 $i = 0, \dots, m-1$
 $a_m = 1$

follow what is in the book, p. 370-371

$$\text{let } \frac{y_1(s)}{u(s)} = \frac{\sum_{i=0}^{m-1} c_i s^i}{\sum_{i=0}^m a_i s^i} = \frac{y_1}{x_0} \cdot \frac{x_0}{u(s)}$$

$$\text{let } \frac{y_1}{x_0} = \sum_{i=0}^{m-1} c_i s^i$$

$$\frac{u}{x_0} = \sum_{i=0}^m a_i s^i$$

$$\Rightarrow y_1 = \sum_{i=0}^{m-1} c_i s^i x_0$$

$$u = \sum_{i=0}^m a_i s^i x_0 = A x_0 + \sum_{i=0}^{m-1} a_i s^i x_0$$

$$\equiv A x_0 = u - \sum_{i=0}^{m-1} a_i s^i x_0 = A x_m$$

gives output C part

gives $Ax + Bu$ part

$$\text{set } A^i x_0 = x_{i+1}$$

$$x_0 = x_1, A x_0 = A x_1 = x_2$$

$$A^2 x_0 = A x_2 = x_3 \dots A^{m-1} x_0 = x_m$$

use $s = d/dt$

$$\text{let } x = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_m \end{bmatrix}; \frac{dx}{dt} = \begin{bmatrix} A x_1 \\ A x_2 \\ \vdots \\ A x_{m-1} \\ A x_m \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & 0 & \dots \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \dots & 0 \\ -a_0 & -a_1 & \dots & \dots & -a_{m-1} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_{m-1} \\ x_m \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u$$

$$y = [c_0 \ c_1 \ \dots \ c_{m-1}] \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_m \end{bmatrix} + d u$$