

Look at $S(a)$ for $y_L(a)$:

$$S_{y_L} = \frac{1 - y_L}{1 + y_L} = \frac{1 - \frac{kY(s) - aY(s)}{kY(s) - aY(s)}}{1 + \frac{kY(s) - aY(s)}{kY(s) - aY(s)}} = \frac{kY(s) - aY(s) - kY(s) + aY(s)}{kY(s) - aY(s) + kY(s) - aY(s)}$$

$$= \frac{k+1}{k-a} \cdot \frac{(-Y(s) + Y(s))}{(Y(s) + Y(s))} = \frac{1 + a/k}{1 - a/k} \cdot \frac{1 - \frac{Y(s)}{Y(s)}}{1 + \frac{Y(s)}{Y(s)}} \times (-1)$$

$$\left| S_{y_L}(j\omega) \right| = \left| \frac{1 + j\omega/k}{1 - j\omega/k} \right| \left| S_y(j\omega) \right| \leq 1$$

$$\frac{1 + \omega^2/k^2}{1 + \omega^2/k^2} \leq 1$$

$\therefore |S_{y_L}(j\omega)|^2 \leq 1 \Rightarrow S_{y_L}^*(s) S_{y_L}(s) \leq 1$ in $\sigma > 0$ if $S_{y_L}(s)$ is analytic

S_{y_L} has no poles in $\sigma > 0$ if S_y has no poles there
this is true if y is PR

But S_{y_L} looks to have a pole at $s = k$ due to $\frac{k+a}{k-a}$

so if y is PR, S_{y_L} is rational & $k-a$ cancels in numerator & denominator.

$\therefore S_{y_L}(s)$ is BR as is $S_y(s)$ if $y(s)$ is PR

Note $y(s) = \sqrt{s}$ is positive-real



Look at $S(s)$, $Y(s)$ as matrices

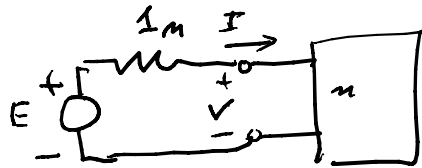
$$P_m = \operatorname{Re} V^{*T} I$$

$$2V^i = V + I = E$$

$$2V^n = V - I$$

$$\Rightarrow V = V^i + V^n$$

$$I = V^i - V^n$$



$$P_m = \operatorname{Re}(V^{*T} I) = \operatorname{Re}((V^i + V^n)^{*T} (V^i - V^n))$$

$$= \underbrace{V^{i*T} V^i - V^{n*T} V^n}_{=0} + \operatorname{Re}(V^{n*T} V^i - V^{i*T} V^n)$$

$$= V^{i*T} V^i - V^{n*T} V^n + \operatorname{Re}(V^{n*T} V^i - V^{i*T} V^n)$$

$$= V^{i*T} [1_m - S^{*T} S] V^i$$

If lossless $1_n = S^{*T}(j\omega) S(j\omega)$
 $= S^T(-j\omega) S(j\omega)$ for all real ω
 can extend to all $s = \sigma + j\omega$ by analytic continuation $j\omega \rightarrow s$

if lossless $1_m = S^T(-s) S(s)$ for all s

\therefore the inverse exists & is given by $S^{-1}(s) = S^T(-s)$

$$V = ZI, \quad I = YV$$

$$2V^i = V + I = V + YV = (1_m + Y)V$$

$$2V^n = V - I = V - YV = (1_m - Y)V = 2S V^i = S(1_m + Y)V$$

$$S = (1_m - Y)(1_m + Y)^{-1}$$

Ex: lossless

$$y(s) = sc$$

$$S_z(s) = \frac{1 - sc}{1 + sc} = S_y(-s)^{-1} \text{ as } S_y(-s) = \frac{1 - (-s)c}{1 + (-s)c} = \frac{1 + sc}{1 - sc}$$

(has a pole in $\sigma > 0$)

Ideal transformers are lossless; $P_{in} \equiv 0$

$$i_2 + T i_1 = 0, \quad v_1^* i_1 + v_2^* i_2 = v_1^* i_1 + v_2^* (-T i_1) = 0$$

$T = \text{turns ratio}$

$$v_1^* = T v_2^* \Rightarrow v_1 = T^* v_2$$

if conjugate

but for a real transformer $T = T^*$

$$\begin{bmatrix} T & 1 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 1 & -T \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \quad \begin{array}{l} i: \text{ no } Y \text{ or } Z \\ \text{no } YV = I \text{ or } ZI = V \end{array}$$

But S exists even though Z & Y do not

$$AV = BI \quad ; \quad \begin{array}{l} V = V^c + V^n \\ I = V^c - V^n \end{array}$$

$$A(V^c + V^n) = B(V^c - V^n) \Rightarrow (A - B)V^c = -(A + B)V^n$$

$$\& V^n = S V^c \Rightarrow S = (B + A)^{-1} (B - A)$$

for the transformer

$$B = \begin{bmatrix} 0 & 0 \\ 1 & -T \end{bmatrix}, \quad A = \begin{bmatrix} T & 1 \\ 0 & 0 \end{bmatrix}, \quad A + B = \begin{bmatrix} T & 1 \\ 1 & -T \end{bmatrix}$$

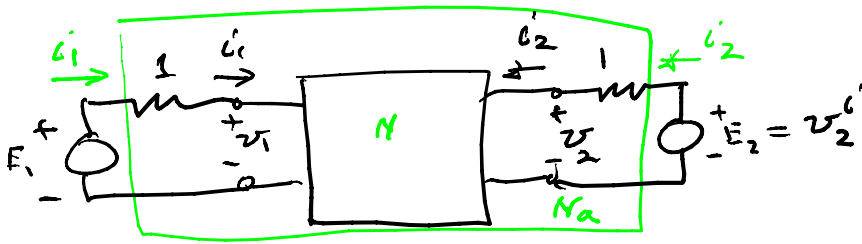
$$(B + A)^{-1} = \frac{1}{-(1 + T^2)} \begin{bmatrix} -T & -1 \\ -1 & T \end{bmatrix}, \quad B - A = \begin{bmatrix} -T & -1 \\ 1 & -T \end{bmatrix}$$

$$S = (B + A)^{-1} (B - A) = \frac{1}{1 + T^2} \begin{bmatrix} -T & -1 \\ -1 & T \end{bmatrix} \begin{bmatrix} -T & -1 \\ 1 & -T \end{bmatrix}$$

$$\begin{bmatrix} T^2 - 1 & 2T \\ 2T & 1 - T^2 \end{bmatrix}$$

$$S_{\text{trans}} = \begin{bmatrix} \frac{1 - T^2}{1 + T^2} & -\frac{2T}{1 + T^2} \\ -\frac{2T}{1 + T^2} & \frac{T^2 - 1}{1 + T^2} \end{bmatrix}$$

as the transformer is lossless, $S_{\text{trans}}^{-1} = S_{\text{trans}}^T$



$$E_2 = 0 \Rightarrow v_2^i = 0 = \frac{v_2 + i_2}{2} = v_2 = -i_2 \quad ; \quad E_1 = v_1^i$$

$$\begin{bmatrix} v_1^i \\ v_2^i \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \begin{bmatrix} v_1^i \\ v_2^i \end{bmatrix} \Rightarrow v_2^i = S_{21} v_1^i = S_{21} E_1$$

$$2v_2^i = v_2 - i_2 = 2v_2$$

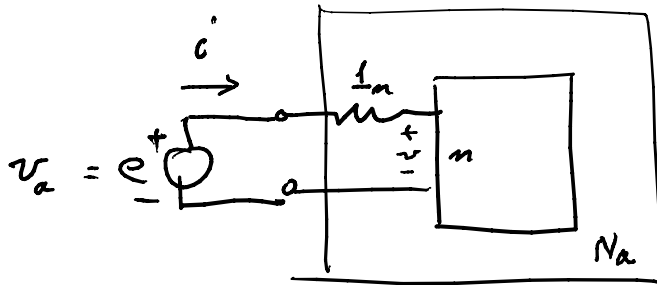
$$= 2v_2$$

$$S_{21} = 2 \frac{v_2}{E_1} = \text{terminated voltage gain}$$

one method of design

is from $S_{21}(j\omega) \rightarrow S_{21}(s) \rightarrow S$ which is para-unitary

$$S(s)S(-s) = I_2$$



$$i = Y_a e$$

$$v = e - i = e - Y_a e$$

$$2v^i = v + i = (e - Y_a e) + Y_a e = e$$

$$2v^r = v - i = (e - Y_a e) - Y_a e = (1 - 2Y_a)e$$

$$2v^i = e$$

$$2v^r = S(2v^i) = (1_m - 2Y_a)e$$

$$= (1_m - 2Y_a)(2v^i)$$

$$\Rightarrow S = 1_m - 2Y_a$$

$$\text{note } Av = Bi \Rightarrow (1_m - Y_a)i = (1_m - Y_a)Y_a e$$

$$= (Y_a - Y_a^2)e = Y_a(1_m - Y_a)e$$

$$= Y_a v$$

can set

$$B = 1_m - Y_a, \quad A = Y_a \Rightarrow S = (B+A)^{-1}(B-A)$$

$$= 1_m(1_m - 2Y_a)$$

It is true Y_a exists when N is passive (since Y does not have -1 to cancel $+1$)