

Exam study

EE 303 Tu 10/14/08

MOS & BJT characteristics

differential pairs

$v_o/v_i(s)$; poles & zeros

small signal equivalents

For subthreshold use of MOS $\sim I_D \approx$ pico amp range

uses BSIM models; level 8 of PSpice

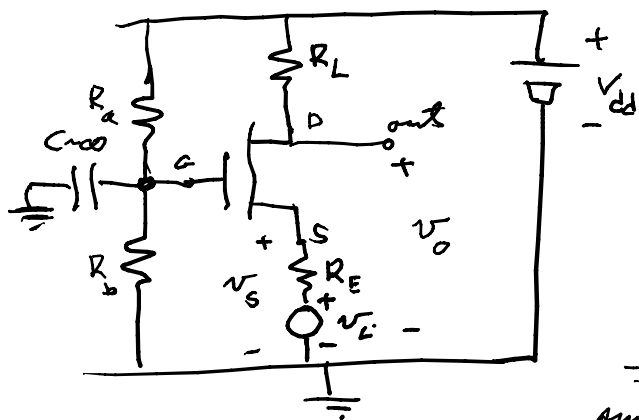
|| 49 in Cadence Hspice

NMOS

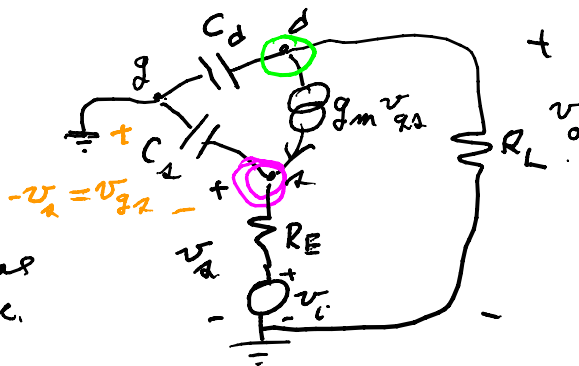
$$I_D \approx \frac{K_P \cdot W}{2 \cdot L} (V_T)^{2.18} e^{(V_{GS} - V_{TO})/mV_T} \cdot (1 - e^{-V_{DS}/V_T})$$

from CMOS by Baker, Li & Boyce (eq. (6.51))

Grounded Gate amplifiers



⇒ Small signal equiv. circ.



desire $\frac{v_o(s)}{v_i} =$ transfer function

if 0 use KCL leaving $\Sigma = 0$

$$1) \quad sC_d v_o + g_m (-v_a) + G_L v_o = 0$$

$$2) \quad v_a = \frac{sC_d + G_L}{g_m} v_o$$

where $G_L = 1/R_L$

at ∞ use KCL leaving $Z=0$

$$2) \quad \Delta C_A \cdot (+v_A) + G_E (v_A - v_i) - g_m (-v_A) = 0$$

$$(\Delta C_A + G_E + g_m) v_A = G_E v_i$$

$$G_E = 1/R_E$$

$$2') \quad v_A = \frac{G_E}{(\Delta C_A + (G_E + g_m))} \cdot v_i$$

equates 1') & 2')

$$3) \quad \frac{\Delta C_d + G_L}{g_m} v_o = \frac{G_E}{(\Delta C_A + (G_E + g_m))} \cdot v_i$$

$$\frac{v_o}{v_i}(s) = \frac{G_E g_m}{(\Delta C_d + G_L)(\Delta C_A + (G_E + g_m))}$$

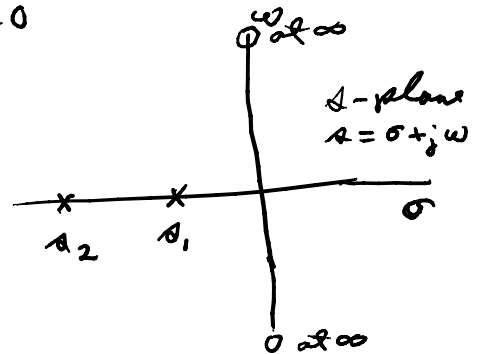
$$\omega=0 \text{ gain} = \frac{v_o(0)}{v_i} = \frac{G_E g_m}{G_L (G_E + g_m)} = \frac{R_L}{R_E} \cdot \frac{g_m}{g_m + G_E}$$

zeros: where $\frac{v_o}{v_i} \approx 0$ in s ; has a double zero at $s = \infty$

$$\text{poles: } \Delta C_d + G_L = 0, \quad \Delta C_A + (G_E + g_m) = 0$$

$$s_1 = -\frac{G_L}{C_d}$$

$$s_2 = -\frac{(G_E + g_m)}{C_A}$$

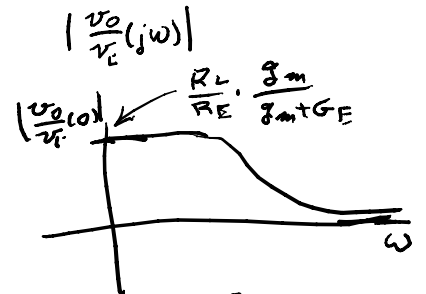


For the frequency response

$$s = j\omega$$

$$\frac{v_o}{v_i}(j\omega) = \frac{G_E g_m}{(G_L + j\omega C_d)((G_E + g_m) + j\omega C_A)}$$

$$\left| \frac{v_o}{v_i}(j\omega) \right|^2 = \frac{G_E g_m}{(G_L^2 + \omega^2 C_d^2)((G_E + g_m)^2 + \omega^2 C_A^2)}$$



a low pass filter

$$\begin{aligned} \angle \frac{v_o}{v_i}(j\omega) &\Rightarrow \frac{v_o}{v_i}(j\omega) = \left| \frac{v_o}{v_i}(j\omega) \right| e^{j\angle \frac{v_o}{v_i}} \\ &= | \cdot | e^{-j\angle(G_L + j\omega C_S)} \cdot e^{-j\angle(g_m + G_E) + j\omega C_D} \\ &= | \cdot | e^{-j\arctan \frac{\omega C_S}{G_L}} - j\arctan \frac{\omega C_D}{g_m + G_E} \end{aligned}$$

Let $v_i(t) = V_i \sin(\omega t) = V_i \left(\frac{e^{j\omega t} - e^{-j\omega t}}{2j} \right)$ $V_i > 0$

$$v_i = \frac{V_i e^{j\omega t}}{2j} - \frac{V_i e^{-j\omega t}}{2j}$$

Write with $v_i = \frac{V_i e^{j\omega t}}{2j}$

$$\begin{aligned} v_{o_1}(t) &= \left(\left| \frac{v_o}{v_i}(a) \right| \right) \cdot \frac{V_i}{2j} e^{j\omega t} = \frac{G_E g_m}{(C_D + G_L)(C_D + (G_E + g_m))} \left| \frac{V_i e^{j\omega t}}{2j} \right| \\ &= \frac{G_E g_m}{(G_L + j\omega C_D)(G + g_m) + j\omega C_D} \cdot \frac{V_i}{2j} e^{j\omega t} \end{aligned}$$

$v_{o_2}(t) = v_{o_1}^*(t)$ *by having real coefficients = real valued components*

$v_o(t) = v_{o_1}(t) + v_{o_1}^*(t)$ *by linearity*

