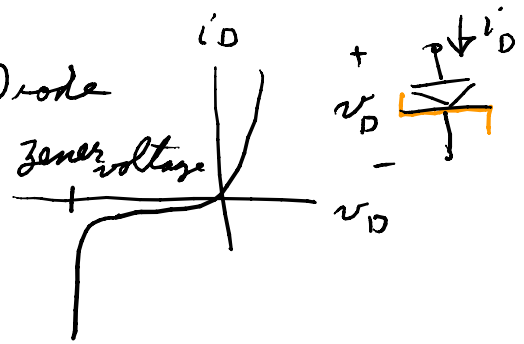


BJT small signal parameters

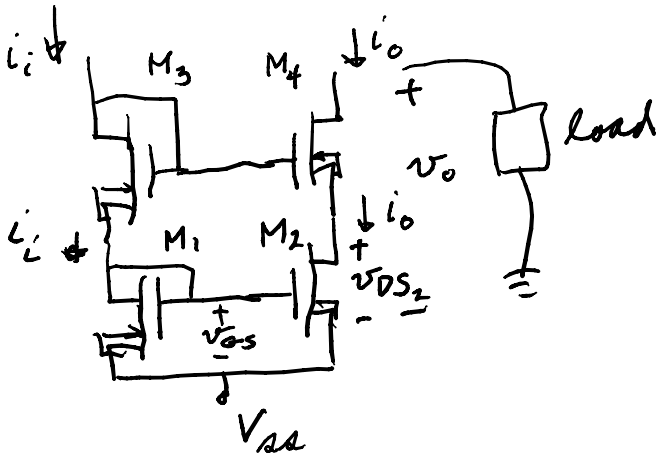
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P-N Diode

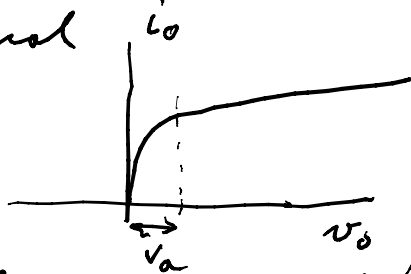


Cascode current mirrors

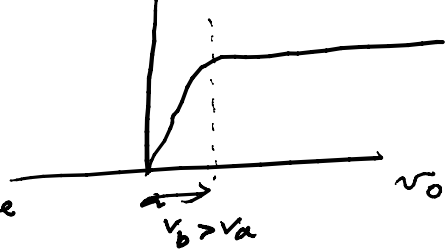


allows changes in v_o to not affect v_{DS2} so i_o is determined by M_1 & M_2

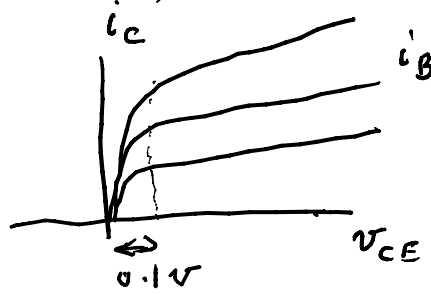
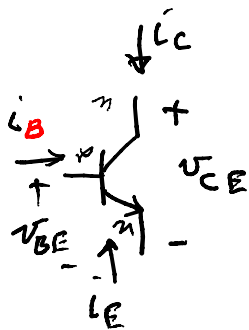
normal



cascode i_o



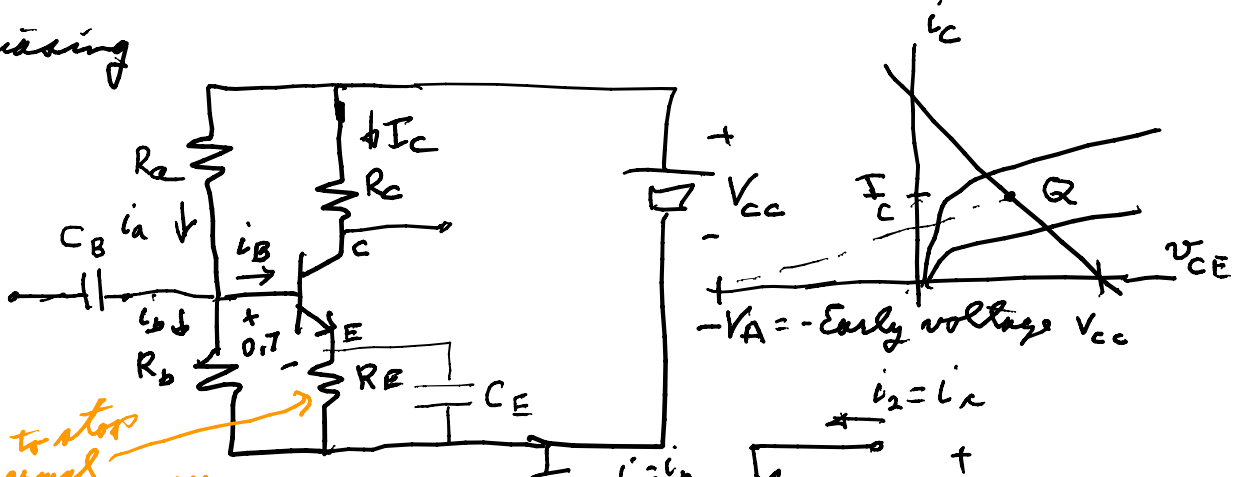
Forward active



(saturation)

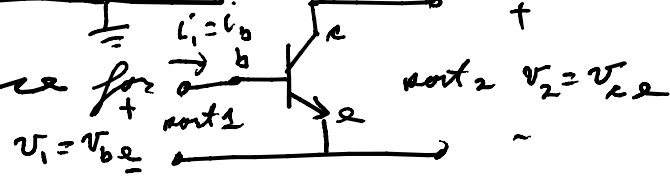
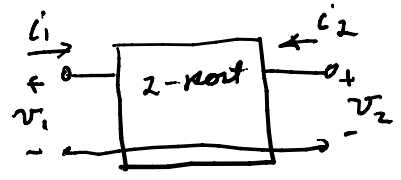
In forward active region C-B junction is back biased
E-B " " forward biased

Biasing

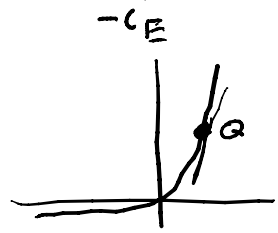


to stop thermal runaway

The 2-port admittance for



$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$



$$-i_E = I_{ES} e^{v_{BE}/V_T} \quad ; \quad i_C = \alpha(-i_E)$$

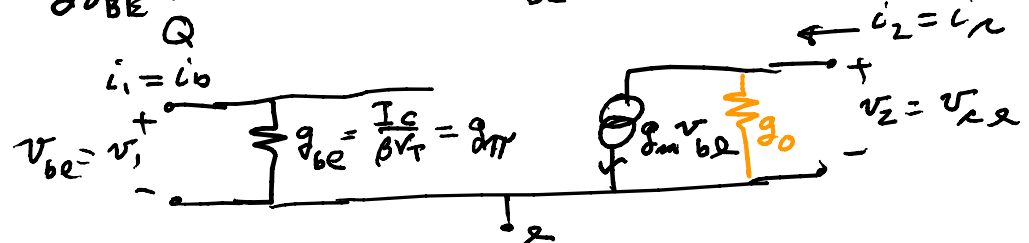
$$g_E = \frac{\partial(-i_E)}{\partial v_{BE}} = \frac{1}{V_T} I_{ES} e^{v_{BE}/V_T} = \frac{-i_E}{V_T} = \frac{1}{\alpha} \frac{i_C}{V_T} = \frac{I_C}{\alpha V_T}$$

$$i_B + i_E + i_C = 0 \text{ by KCL}$$

$$i_B = -(i_E + i_C) = -(i_E + \alpha i_E) = -(1 + \alpha)i_E = -\frac{i_C}{\alpha} \quad \beta = \frac{\alpha}{1 - \alpha}$$

$$= \frac{i_C}{\beta} \Rightarrow @ Q \quad I_B = \frac{I_C}{\beta} = \frac{\alpha V_T \cdot g_E}{\beta}$$

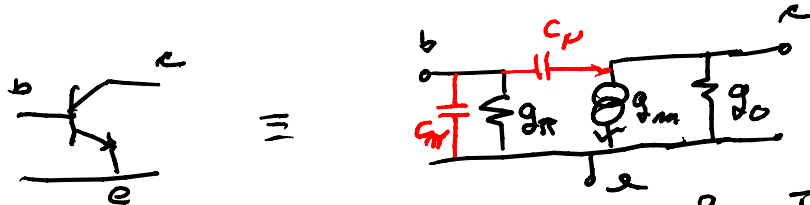
$$i_b = i_1 = \frac{\partial i_B}{\partial v_{BE}} \Big|_Q \cdot v_{be} = \frac{\partial i_B}{\partial i_E} \cdot \frac{\partial i_E}{\partial v_{BE}} \cdot v_{be} = -(1 + \alpha) \frac{I_C}{\alpha V_T} \cdot v_{be} = \frac{I_C}{\beta V_T} \cdot v_1$$



$$\frac{\partial i_C}{\partial v_{BE}} \Big|_Q = g_m = \frac{\partial(-\alpha i_E)}{\partial v_{BE}} \Big|_Q = \alpha \left(\frac{\partial(-i_E)}{\partial v_{BE}} \right) \Big|_Q = \alpha \cdot \frac{I_C}{\alpha V_T} = \frac{I_C}{\alpha} = g_m$$

= mutual conductance
= transconductance

$$\left. \frac{\partial I_c}{\partial V_{CE}} \right|_Q = g_o = \text{output conductance} = \frac{I_c}{V_A}$$

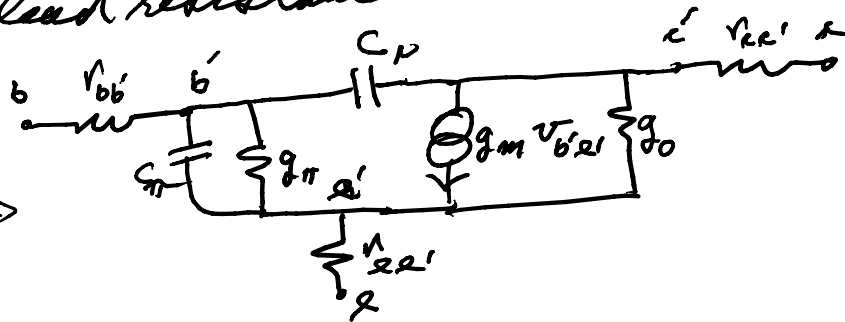


C_μ & C_π are junction capacitors

$$g_m = \frac{I_c}{V_T}, \quad g_\pi = \frac{g_m}{\beta} = \frac{I_c}{\beta V_T}, \quad g_o = \frac{I_c}{V_A}$$

putting in lead resistance

hybrid- $\pi \Rightarrow$
equivalent circuit



Example: $I_c = 1 \text{ mA}$, $\beta = 100$, $V_A = 200$, $V_T = 26 \text{ mV}$

$$g_m = \frac{I_c}{V_T} = \frac{10^{-3}}{26 \times 10^{-3}} = \frac{1}{26}, \quad g_\pi = \frac{g_m}{\beta} = \frac{1}{2600}, \quad g_o = \frac{1 \times 10^{-3}}{200}$$

$$r_\pi = \frac{1}{g_\pi} = 2.6 \text{ k}\Omega$$

$$r_o = \frac{1}{g_o} = 2 \times 10^5 = 200 \text{ k}\Omega$$

