

1) a) the current-voltage relationship for C_1 is

$$i_3 = C_1 s V_3 - C_1 s V_6$$

$$i_6 = C_1 s V_6 - C_1 s V_3$$

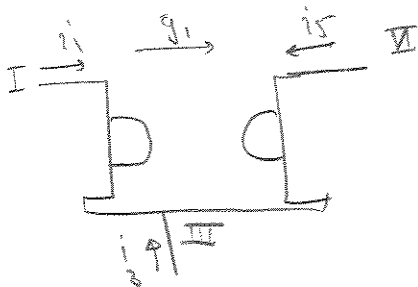
$$\Rightarrow Y_{ind C_1} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & sC_1 & 0 & 0 & -sC_1 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -sC_1 & 0 & 0 & sC_1 \end{bmatrix}$$

For C_2 : $i_5 = C_2 s V_5 - C_2 s V_6$

$$i_6 = C_2 s V_6 - C_2 s V_5$$

$$\Rightarrow Y_{ind C_2} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & sC_2 & 0 & -sC_2 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & -sC_2 & 0 & 0 & sC_2 \end{bmatrix}$$

For gyrator we have the following relationship:



$$i_3 = g_1 (V_5 - V_1)$$

$$i_1 = -g_1 (V_5 - V_3)$$

$$i_5 = g_1 (V_1 - V_3)$$

So $Y_{ind g_1} = \begin{bmatrix} 0 & 0 & g_1 & 0 & -g_1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -g_1 & 0 & 0 & 0 & g_1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ g_1 & 0 & -g_1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$

b) ground node 6 so $V_6 = 0$

$$Y_{\text{nodal}} = \begin{bmatrix} 0 & 0 & g_1 & 0 & -g_1 \\ 0 & 0 & 0 & -g_2 & g_2 \\ -g_1 & 0 & s_{c1} & 0 & g_1 \\ 0 & g_2 & 0 & s_{c2} & -g_2 \\ g_1 & -g_2 & -g_1 & g_2 & 0 \end{bmatrix}$$

c) eliminate node 3 first $\Rightarrow i_3 = 0$

$$\begin{bmatrix} i_1 \\ i_2 \\ i_3 \\ i_4 \\ i_5 \end{bmatrix} = Y_{\text{nodal}} \times \begin{bmatrix} v_1 \\ v_2 \\ v_3 \\ v_4 \\ v_5 \end{bmatrix} \quad \textcircled{I}$$

$$\text{so } i_3 = -g_1 v_1 + s_{c1} v_3 + g_1 v_5$$

$$i_3 = 0 \Rightarrow -g_1 v_1 + g_1 v_5 + s_{c1} v_3 = 0 \Rightarrow v_3 = \begin{bmatrix} g_1 \\ s_{c1} \end{bmatrix} \begin{bmatrix} v_1 \\ v_5 \end{bmatrix}$$

From equation \textcircled{I} we have:

$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} g_1 \\ 0 \end{bmatrix} \cdot v_3 + \begin{bmatrix} 0 & -g_1 \\ -g_2 & g_2 \end{bmatrix} \begin{bmatrix} v_4 \\ v_5 \end{bmatrix}$$

$$\begin{bmatrix} i_4 \\ i_5 \end{bmatrix} = \begin{bmatrix} 0 & g_2 \\ g_1 & -g_2 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + \begin{bmatrix} 0 \\ -g_1 \end{bmatrix} \cdot v_3 + \begin{bmatrix} s_{c2} & -g_2 \\ g_2 & 0 \end{bmatrix} \begin{bmatrix} v_4 \\ v_5 \end{bmatrix}$$

Use the relationship for v_3

$$\Rightarrow \begin{cases} i_1 = -g_1 v_3 - \frac{g_1^2}{s c_1} v_5 + \frac{g_1^2}{s c_1} v_1 \\ i_2 = -g_2 v_4 + g_2 v_5 \\ i_5 = g_1 v_1 - g_2 v_2 - \frac{g_1^2}{s c_1} v_4 + \frac{g_1^2}{s c_1} v_5 + g_2 v_4 \\ i_4 = s c_2 v_4 + g_2 v_2 - g_2 v_5 \\ i_3 = 0 \end{cases}$$

$$\begin{bmatrix} i_1 \\ i_2 \\ i_4 \\ i_5 \end{bmatrix} = \begin{bmatrix} \frac{g_1^2}{s c_1} & 0 & 0 & -g_1 - \frac{g_1^2}{s c_1} \\ 0 & 0 & -g_2 & g_2 \\ 0 & g_2 & s c_2 & -g_2 \\ g_1 - \frac{g_1^2}{s c_1} & -g_2 & g_2 & \frac{g_1^2}{s c_1} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_4 \\ v_5 \end{bmatrix}$$

let $i_4 = 0$

$$i_4 = g_2 v_2 + s c_2 v_4 - g_2 v_5 = 0 \Rightarrow v_4 = -\frac{g_2}{s c_2} v_2 + \frac{g_2}{s c_2} v_5$$

then

$$\begin{cases} i_2 = \frac{g_2^2}{s c_2} v_2 + g_2 v_5 - \frac{g_2^2}{s c_2} v_5 \\ i_5 = g_1 v_1 - \frac{g_1^2}{s c_1} v_1 - g_2 v_2 - \frac{g_2^2}{s c_2} v_2 + \frac{g_2^2}{s c_2} v_5 + \frac{g_1^2}{s c_1} v_5 \\ i_4 = 0 \end{cases}$$

$$\Rightarrow \begin{bmatrix} i_1 \\ i_2 \\ i_5 \end{bmatrix} = \begin{bmatrix} \frac{g_1^2}{s c_1} & 0 & 0 & -g_1 - \frac{g_1^2}{s c_1} \\ 0 & \frac{g_2^2}{s c_2} & 0 & 0 \\ g_1 - \frac{g_1^2}{s c_1} & -g_2 - \frac{g_2^2}{s c_2} & \frac{g_2^2}{s c_2} & \frac{g_1^2}{s c_1} + \frac{g_2^2}{s c_2} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_5 \end{bmatrix}$$

Let $i_3 = 0$ then $-(g_2 + \frac{g_2^2}{s c_2}) v_2 + (g_1 - \frac{g_1^2}{s c_1}) v_1 + (\frac{g_1^2}{s c_1} + \frac{g_2^2}{s c_2}) v_3 = 0$

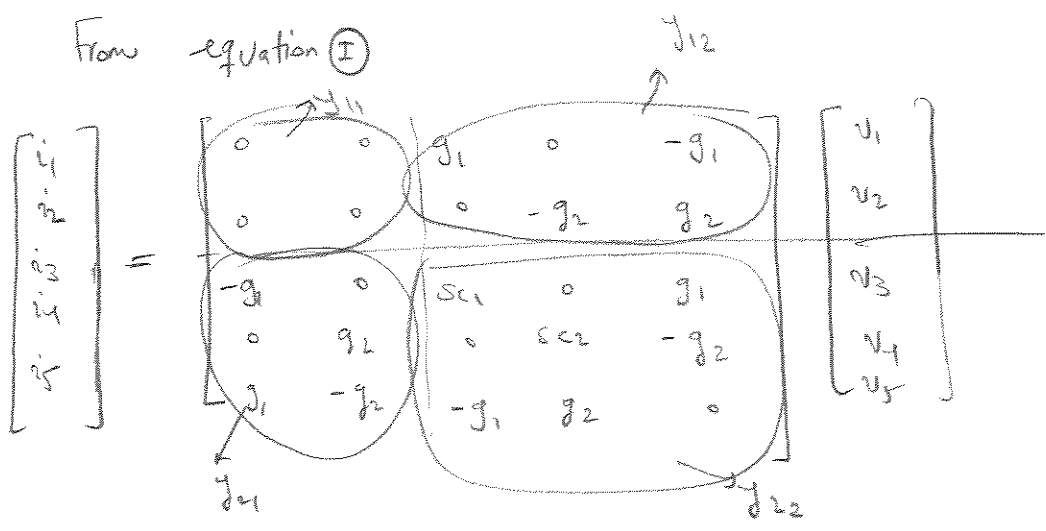
$$\Rightarrow v_3 = \frac{(g_1^2 c_2 - g_1 s c_1 c_2)}{g_1^2 c_2 + g_2^2 c_1} v_1 + \frac{(g_2 s c_1 c_2 + g_2^2 c_1)}{g_1^2 c_2 + g_2^2 c_1} v_2$$

So $i_1 = \frac{g_1^2}{s c_1} v_1 + \left(\frac{g_1^2 c_2 - g_1 s c_1 c_2}{g_1^2 c_2 + g_2^2 c_1} \right) \left(-g_1 - \frac{g_1^2}{s c_1} \right) v_1 + \left(\frac{g_2 s c_1 c_2 + g_2^2 c_1}{g_1^2 c_2 + g_2^2 c_1} \right) \left(-g_1 - \frac{g_1^2}{s c_1} \right) v_2$

$$i_2 = \left(\frac{g_1^2 c_2 - g_1 s c_1 c_2}{g_1^2 c_2 + g_2^2 c_1} \right) \left(g_2 - \frac{g_2^2}{s c_2} \right) v_1 + \frac{g_2^2}{s c_2} v_2 + \left(\frac{g_2 s c_1 c_2 + g_2^2 c_1}{g_1^2 c_2 + g_2^2 c_1} \right) \left(g_2 - \frac{g_2^2}{s c_2} \right) v_2$$

From the equations above for i_1 and i_2 we have the relationship between $\begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$ and $\begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$.

c) eliminate all three nodes at the same time:



$$\Rightarrow \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = y_{11} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + y_{12} (-y_{22}^{-1} \cdot y_{21}) \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \Rightarrow \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = (y_{11} - y_{12} y_{22}^{-1} y_{21}) \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$\begin{bmatrix} i_3 \\ i_4 \\ i_5 \end{bmatrix} = y_{21} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + y_{22} \begin{bmatrix} v_3 \\ v_4 \\ v_5 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} \underbrace{\frac{(C_1 g_2^2 + g_1^2 c_2)(g_2^2 + s^2 c_1 c_2)}{s}}_{\mu_{11}} & \underbrace{\frac{(C_1 g_2^2 + g_1^2 c_2)(g_1 + s c_1)(g_2 + s c_2)(-g_1 g_2)}{s}}_{\mu_{12}} \\ \underbrace{\frac{(C_1 g_2^2 + g_1^2 c_2)(-g_2 + s c_1)(-g_1 + s c_2)(-g_2 c_2)}{s}}_{\mu_{21}} & \underbrace{\frac{(C_1 g_2^2 + g_1^2 c_2 / g_2^2)(g_1^2 + s^2 c_1 c_2)}{s}}_{\mu_{22}} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

The method which eliminates all the nodes together is easier and faster.

d) From above:

$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} \mu_{11} & \mu_{12} \\ \mu_{21} & \mu_{22} \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$v_2 = R i_2 \quad R: \text{load resistance}$$

$$i_1 = \mu_{11} v_1 + \mu_{12} v_2$$

$$i_2 = \mu_{21} v_1 + \mu_{22} v_2 \Rightarrow R i_2 = R \mu_{21} v_1 + \mu_{22} R v_2$$

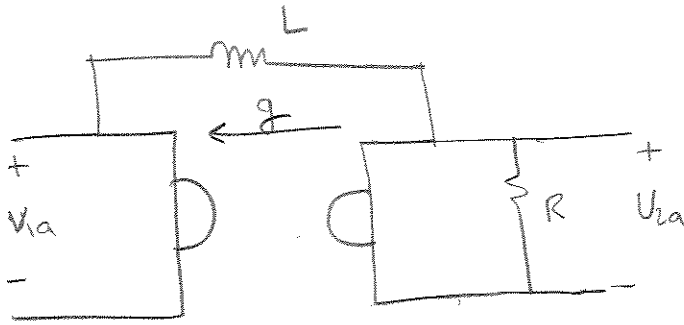
$$\text{then } v_2 = R \mu_{21} v_1 + R \mu_{22} v_2 \Rightarrow R \mu_{21} v_1 = (1 - R \mu_{22}) v_2 \Rightarrow v_2 = \frac{R \mu_{21}}{1 - R \mu_{22}} v_1$$

$$\text{so } v_2 = S v_1 \Rightarrow i_1 = (\mu_{11} + \mu_{12} S) v_1 \Rightarrow \frac{i_1}{v_1} = \mu_{12} S + \mu_{11}$$

$$\text{so } Z_{in} = \mu_{12} \left(\frac{R \mu_{21}}{1 - R \mu_{22}} \right) + \mu_{11}$$

Problem 2) a) the adjoint of a gyrator is a gyrator with negative gyration.

adjoint:



$$\Delta(T) = \mathbf{V}_{int}^T \Delta \mathbf{Y}^T \mathbf{V}_{int}$$

Voltage transfer function

$$\mathbf{V}_{int} = \begin{bmatrix} V_1 & V_2 \end{bmatrix}$$

$$\mathbf{V}_{int} = \begin{bmatrix} V_{1a} & V_{2a} \end{bmatrix}$$

finding Y:

$$Y = Y_R + Y_L + Y_g$$

$$Y_L = \begin{bmatrix} \frac{1}{L_s} & \frac{-1}{L_s} \\ \frac{1}{L_s} & \frac{1}{L_s} \end{bmatrix}$$

$$Y_R = \begin{bmatrix} 0 & 0 \\ 0 & \frac{1}{R} \end{bmatrix}$$

$$Y_g = \begin{bmatrix} 0 & g \\ g & 0 \end{bmatrix}$$

$$\Rightarrow Y = \begin{bmatrix} \frac{1}{L_s} & \frac{-1}{L_s} - g \\ \frac{-1}{L_s} + g & \frac{1}{L_s} + G \end{bmatrix} \quad G = \frac{1}{R}$$

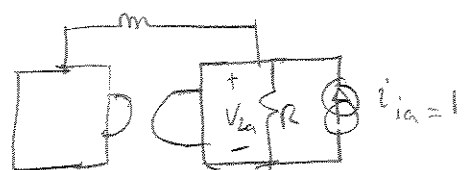
derivative w/respect to R

$$\Delta Y = \begin{bmatrix} 0 & 0 \\ 0 & \Delta G \end{bmatrix}$$

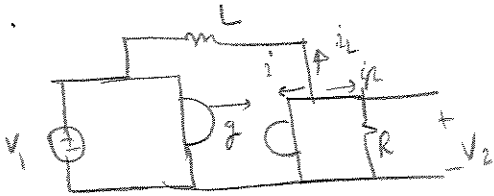
$$\frac{\Delta(T)}{\Delta G} = V_2 \cdot V_{2a}$$

to find derivative w/respect to R we have;

$$\begin{cases} V_{1a} = 0 \\ V_{2a} = 1 \end{cases}$$

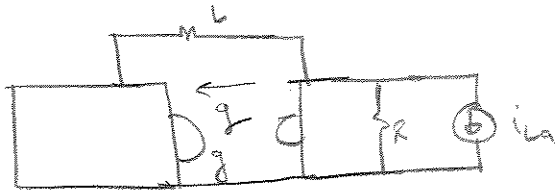


find v_2 :



$$iR + i_L + i = 0 \Rightarrow \frac{v_2}{R} + gV_1 + \frac{1}{Ls}v_2 - \frac{1}{Ls}v_1 = 0 \Rightarrow v_2 = \left(\frac{1 - sLg}{1 + sLG} \right) v_1$$

find v_{2a} :



$$Z^{-1} = \frac{1}{Ls} + \frac{1}{R} = \frac{1}{Ls} + G = \frac{sLG + 1}{Ls} \Rightarrow v_{2a} = Z \cdot i_{La} = \frac{-Ls}{1 + sLG}$$

$$\frac{\partial T}{\partial G} = v_2 \cdot v_{2a} = \left(\frac{1 - sLG}{sLG + 1} \right) \left(\frac{-Ls}{1 + sLG} \right) = \frac{Lg \cdot s^2 - Ls}{(1 + sLG)^2}$$

with respect to L :

$$\Delta T = v_{int}^T \Delta y \quad v_{int a}$$

$$T = \frac{v_2}{v_1} \quad \Delta y = \begin{bmatrix} \frac{1}{\Delta Ls} & -\frac{1}{\Delta Ls} \\ -\frac{1}{\Delta Ls} & \frac{1}{\Delta Ls} \end{bmatrix}$$

$$v_{int a} = [v_{1a} \quad v_{2a}]^T = \begin{bmatrix} 0 & v_{2a} \end{bmatrix}^T = \begin{bmatrix} 0 \\ v_{2a} \end{bmatrix}$$

$$v_{1a} = 0, \quad i_{La} = 1$$

$$\Delta T = [v_1 \quad v_2] \begin{bmatrix} \frac{1}{\Delta Ls} & -\frac{1}{\Delta Ls} \\ -\frac{1}{\Delta Ls} & \frac{1}{\Delta Ls} \end{bmatrix} \begin{bmatrix} 0 \\ v_{2a} \end{bmatrix}^T = \frac{v_{2a}(v_2 - v_1)}{\Delta Ls}$$

assume $\bar{r} = \frac{1}{L} \Rightarrow \Delta y = \begin{bmatrix} \frac{\Delta r}{s} & -\frac{\Delta r}{s} \\ \frac{\Delta r}{s} & \frac{\Delta r}{s} \end{bmatrix}$

$$\Rightarrow \Delta V_2 = [V_1 \ V_2] \begin{bmatrix} \frac{\Delta r}{s} & -\frac{\Delta r}{s} \\ -\frac{\Delta r}{s} & \frac{\Delta r}{s} \end{bmatrix} \begin{bmatrix} 0 \\ V_{2a} \end{bmatrix}$$

$$\Rightarrow \Delta V_2 = V_{2a} (V_2 - V_1) \frac{\Delta r}{s} \Rightarrow V_2 = H(s) V_1$$

$$\Rightarrow \Delta V_2 = V_{2a} (H(s) V_1 - V_1) \frac{\Delta r}{s} \Rightarrow \Delta \left(\frac{V_2}{V_1} \right) = V_{2a} (H(s) - 1) \frac{\Delta r}{s}$$

$$\Rightarrow \frac{\Delta \left(\frac{V_2}{V_1} \right)}{\Delta r} = \frac{V_{2a}}{s} (H(s) - 1)$$

We know from before $H(s) = \frac{1 - sLg}{sLG + 1}$ and $V_{2a} = \frac{-Ls}{sLG + 1}$

substituting

$$\Rightarrow \frac{\Delta \left(\frac{V_2}{V_1} \right)}{\Delta r} = \frac{L^2}{(1 + sLG)^2} (g + G)$$

$$\Delta r = \frac{-1}{L^2} \Delta L \Rightarrow \frac{\Delta \left(\frac{V_2}{V_1} \right)}{\frac{-1}{L^2} \Delta L} = \frac{L^2}{(1 + sLG)^2} (g + G)$$

$$\Rightarrow \frac{\Delta \left(\frac{V_2}{V_1} \right)}{\Delta L} = \frac{-s}{(1 + sLG)^2} (g + G)$$

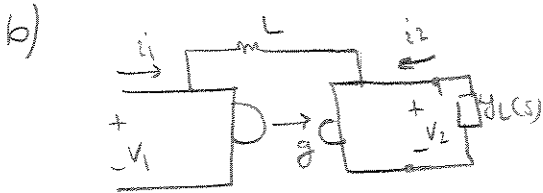
Direct derivation with respect to R and L

$$\frac{V_2}{V_1} = \frac{1 - sLg}{1 + sLG}$$

$$\frac{\partial \left(\frac{V_2}{V_1} \right)}{\partial G} = \frac{-sL(1 - sLg)}{(1 + sLG)^2} = \frac{-sL + L^2 g s^2}{(1 + sLG)^2}$$

the same

$$\frac{\partial(\frac{V_2}{V_1})}{\partial L} = \frac{-sg - sG}{(1+sLG)^2} \quad \text{the same}$$



$$i_2 = Y_L(s)V_2$$

From class notes:

$$y(s) = \frac{i_1}{V_1} = \frac{1}{Ls} - (-\frac{1}{Ls} - g) (Y_L + \frac{1}{Ls})^{-1} (g - \frac{1}{Ls})$$

$$\Rightarrow y(s) = \frac{g^2 L - \frac{Y_L}{s}}{L Y_L + \frac{1}{s}} \Rightarrow y(s) = \frac{Y_L + s g^2 L}{s Y_L + 1} \Rightarrow Y_L(s) = \frac{y(s) - s g^2 L}{1 - s L y(s)}$$

in order to check the input admittance for $Y_L = G$

$$\begin{cases} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} \frac{1}{Ls} & -\frac{1}{Ls} - g \\ -\frac{1}{Ls} + g & \frac{1}{Ls} + G \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} \\ i_2 = -\frac{1}{R} V_2 = -G V_2 \end{cases} \Rightarrow \frac{i_1}{V_1} = y(s) = \frac{\frac{1}{Ls}(V_1) + (-\frac{1}{Ls} - g)(-\frac{1}{Ls} + g)/(1/Ls + 2G)}{V_2}$$

$$\Rightarrow \frac{i_1}{V_1} = \frac{s g^2 L + G}{sL G + 1}$$

$$d) \text{EVP } y(s) = \frac{1}{2} (y(s) + y(-s)) = \frac{1}{2} \left(\frac{Y_L(s) + s g^2 L}{1 + s L Y_L(s)} + \frac{Y_L(-s) - s g^2 L}{1 - s L Y_L(-s)} \right)$$

$$\Rightarrow \text{EVP } y(s) = \frac{(Y_L(s) + Y_L(-s)) - L^2 s^2 g^2 (Y_L(s) + Y_L(-s))}{(1 + s L Y_L(s))(1 - s L Y_L(-s))} \Rightarrow$$

$$2 \text{ EV } \{y(s)\} = \frac{(y_L(s) + y_L(-s))(1 - L^2 s^2 g^2)}{(1 + Ls y_L(s)) [1 - Ls y_L(-s)]}$$

$$\text{EV } \{y(s)\} = \frac{1}{2} \frac{[y_L(s) + y_L(-s)] [1 - L^2 s^2 g^2]}{[1 + Ls y_L(s)] [1 - Ls y_L(-s)]}$$

$$y_L(s) = G \quad , \quad y_L(-s) = G$$

$$\Rightarrow \text{EV } \{y(s)\} = \frac{1}{2} \frac{2G(1 - L^2 s^2 g^2)}{(1 + LsG)(1 - LsG)} = \frac{G(1 - L^2 s^2 g^2)}{(1 - L^2 s^2 G^2)}$$

$$R=5, \quad g=3, \quad L=2$$

$$B(1 - L^2 s^2 g^2) = 0 \Rightarrow 1 - 36s^2 = 0 \Rightarrow s = \pm \frac{1}{6} = \text{zeros}$$