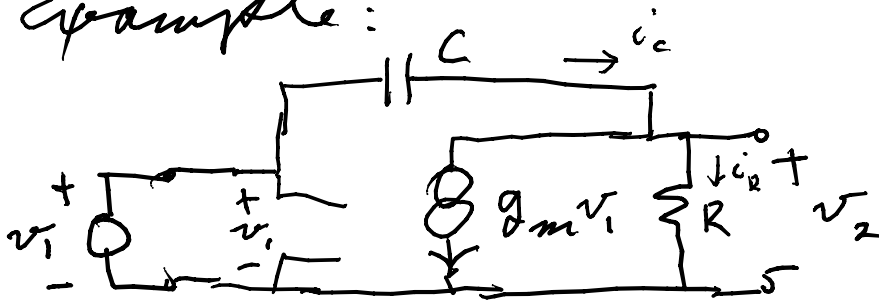
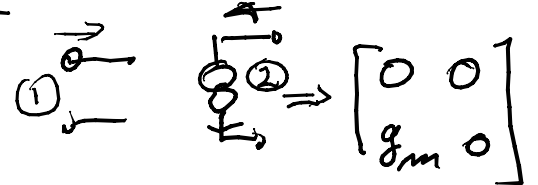


Example:



$$T(\omega) = \frac{V_2(\omega)}{V_1(\omega)}$$

find  $S_C^{T(\omega)} = \frac{\partial T(\omega) / \partial C}{T(\omega) / C}$



if  $V_2(\omega) = 1$  find  $V_1(\omega) \Rightarrow 1 = R \cdot i_R = R(i_C - g_m v_1)$

$$1 + RC\omega = [RC\omega - Rg_m]V_1 = R[\omega C[V_1 - V_2] - g_m V_1]$$

$$V_1 = \frac{1 + RC\omega}{R(C\omega - g_m)} \cdot 1 = V_2 = RC\omega \cdot V_1 - RC\omega - Rg_m V_1$$

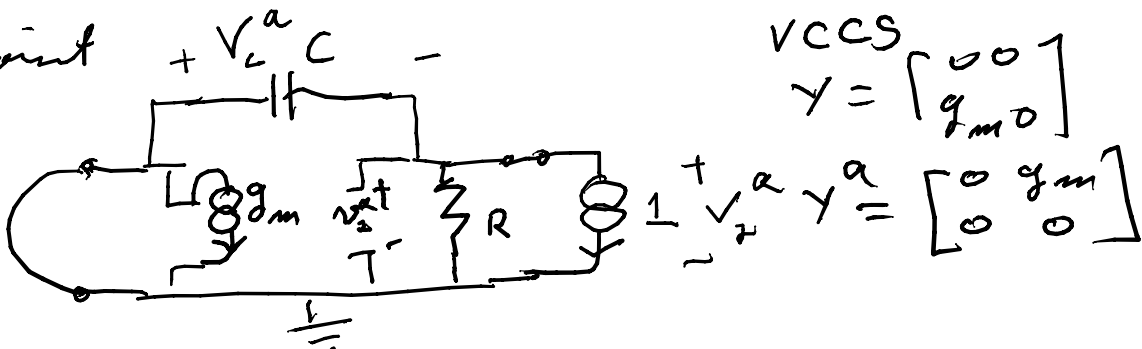
$$\frac{V_2}{V_1} = \frac{RC\omega - Rg_m}{RC\omega + 1} = T(\omega, g_m, R, C)$$

$$\frac{\partial T}{\partial C} = \frac{R\omega}{(1 + RC\omega)} - \frac{(RC\omega - Rg_m)R\omega}{(RC\omega + 1)^2} = \frac{R\omega(RC\omega + 1) - R\omega(RC\omega - Rg_m)}{(1 + RC\omega)^2}$$

$$= \frac{R\omega(1 + Rg_m)}{(1 + RC\omega)^2} \quad \therefore S_C^T = \frac{R\omega(1 + Rg_m)}{(1 + RC\omega)^2} \cdot \left( \frac{RC\omega - Rg_m}{RC\omega + 1} \right) \cdot \frac{1}{C}$$

$\therefore S_C^T = \frac{C\omega(1 + Rg_m)}{(1 + RC\omega)(C\omega - Rg_m)}$  is a function of  $\omega$

adjoint



$$VCCS \quad Y = \begin{bmatrix} 0 & 0 \\ g_m & 0 \end{bmatrix}$$

$$Y^a = \begin{bmatrix} 0 & g_m \\ 0 & 0 \end{bmatrix}$$

$$Y_{b \times b} = \begin{bmatrix} 0 & g_m & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & G & 0 \\ 0 & 0 & 0 & C_A \end{bmatrix} \Rightarrow Y_{b \times b}^a = \begin{bmatrix} 0 & 0 & 0 & 0 \\ g_m & 0 & 0 & 0 \\ 0 & 0 & G & 0 \\ 0 & 0 & 0 & C_A \end{bmatrix}$$

$$\frac{\partial Y_{b \times b}}{\partial C} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \therefore \text{want } V_c \text{ \& } V_c^a$$

$$\text{then } \frac{\partial V_2/V_1}{\partial C} = V_c^a \cdot a \cdot V_c$$

$$-V_c = V_2 - V_1 = \frac{R(C_A - g_m)}{1 + RC_A} - 1 \stackrel{V_1 = 1V}{=} \frac{-Rg_m - 1}{1 + RC_A}$$

$$I_{\text{amp}} = aC V_c^a - G V_2^a = (aC + G) V_c^a$$

$$V_c^a = \frac{1}{aC + G} = \frac{R}{1 + RC_A} \stackrel{V_2^a}{=}$$

$$\frac{\partial V_2/V_1}{\partial C} = V_c^a \cdot a \cdot V_c = \frac{a(+1)(1 + Rg_m) \cdot R}{(1 + RC_A)^2}$$

checks direct calculation

$$S_a^{T(j\omega)} = |S_a^{T(j\omega)}| \cdot e^{j \angle S_a^{T(j\omega)}}$$

$$\begin{aligned} |S_a^T| &= \frac{\left| \frac{\partial T(j\omega)}{\partial a} \right|}{|T(j\omega)/a|} \stackrel{?}{=} \frac{\frac{\partial |T(j\omega)|}{\partial a}}{|T(j\omega)|/a} \quad \text{if } a \text{ is real} \\ &= S_a^{T(j\omega)} \end{aligned}$$

$$T(j\omega) = T_{\text{real}} + j T_{\text{imag}} = T_R + j T_I$$

$$|T(j\omega)| = \sqrt{T_R^2 + T_I^2}$$

$$\frac{\partial |T(j\omega)|}{\partial a} = \frac{1}{2} \frac{1}{\sqrt{T_R^2 + T_I^2}} \left( 2 \frac{\partial T_R}{\partial a} + 2 \frac{\partial T_I}{\partial a} \right)$$

$$= \frac{1}{|T(j\omega)|} \cdot \left[ \frac{\partial T_R}{\partial a} + \frac{\partial T_I}{\partial a} \right]$$

$$\left| \frac{\partial T(j\omega)}{\partial a} \right| = \left| \frac{\partial T_R}{\partial a} + j \frac{\partial T_I}{\partial a} \right| = \sqrt{\left( \frac{\partial T_R}{\partial a} \right)^2 + \left( \frac{\partial T_I}{\partial a} \right)^2}$$

not a nice relationship! But look

at  $S_a = \frac{T(j\omega)}{a} = \frac{|T(j\omega)| e^{j\angle T(j\omega)}}{a}$

$$= \frac{\partial |T(j\omega)| \cdot e^{j\angle T(j\omega)}}{a}$$

$$= \frac{\frac{\partial |T(j\omega)|}{\partial a} \cdot e^{j\angle T(j\omega)} + |T(j\omega)| \cdot \frac{\partial e^{j\angle T(j\omega)}}{\partial a}}{|T(j\omega)| e^{j\angle T(j\omega)} / a}$$

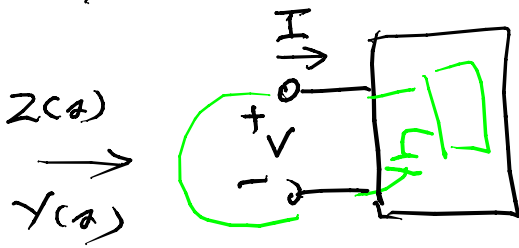
$$= \underbrace{S_a}_{\text{real (a real)}} + \underbrace{S_a \cdot j \frac{\partial \angle T(j\omega)}{\partial a}}_{j \cdot \text{imaginary}}$$

real  
(a real)

j · imaginary

$\therefore \Re[S_a^{TC(j\omega)}] = S_a^{TC(j\omega)}$  what normally  
 would measure (note can replace  $j\omega$  by  $s$ )

More on natural frequencies



$$V = ZI, \quad I = YV$$

if open  $I = 0$   
 if  $V \neq 0 \Rightarrow Z = \infty$   
 $\Rightarrow$  a pole

if short  $V = 0$

$\Rightarrow Y$  has a pole  $= Z$

has a zero

$\therefore$  poles of  $Z$   
 (= zeros of  $Y$ ) are  
 open circuit  
 natural frequencies

$\therefore$  short  
 circuit N.F.'s  
 are  $Z = 0, Y = \infty$