

Graph theory for eqs.

KCL: $\underline{0} = \underline{C} i_b$ t eqs.
 (Σ of currents into a "sphere"
 is 0, one [or out of]
 eq. per tree branch)

$t = \#$ of tree branches

$b =$ total # of branches

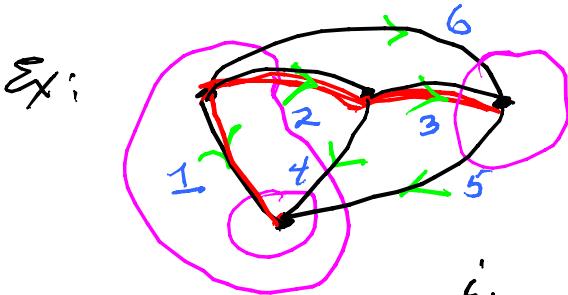
$l = \#$ of link branches
 $C =$ cotree branches)

$$b = t + l$$

$n = \#$ of nodes in the graph

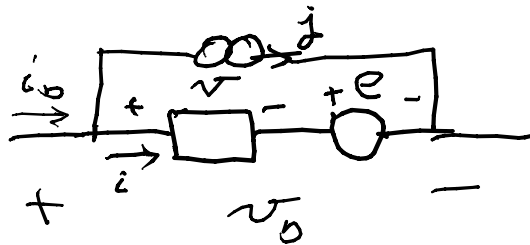
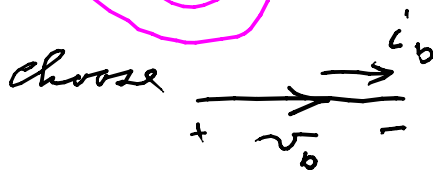
one separate part:

$$t = n - 1 ; l = b - t = b - n + 1$$



$$n = 4, b = 6$$

$$t = 3, l = 6 - 4 + 1 = 3$$



$$i_b = i + j$$

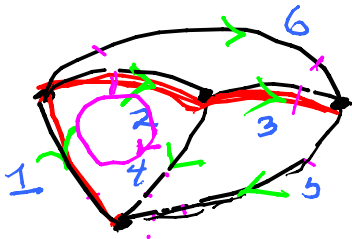
$$v_b = v + e$$

KCL: tree branch 1: $0 = i_{b1} + i_{b4} + i_{b5}$

tree branch 2: $0 = i_{b2} - i_{b4} - i_{b5} + i_{b6}$

tree branch 3: $0 = i_{b3} - i_{b5} + i_{b6}$

$$\begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & | & 1 & 1 & 0 \\ 0 & 1 & 0 & | & -1 & -1 & 1 \\ 0 & 0 & 1 & | & 0 & -1 & 1 \end{bmatrix} \begin{bmatrix} i_{b1} \\ i_{b2} \\ i_{b3} \\ \hline i_{b4} \\ i_{b5} \\ i_{b6} \end{bmatrix} = \mathcal{E} i_b = \begin{bmatrix} 1_3 & | & K_i \\ & & t \end{bmatrix} \begin{bmatrix} i_t \\ i_r \end{bmatrix}$$



Tie set 1: $0 = v_{4b} - v_{1b} + v_{2b}$ (branch 4)
 (branch 5) 2: $0 = v_{5b} - v_{1b} + v_{2b} + v_{3b}$
 (branch 6) 3: $0 = v_{6b} - v_{2b} - v_{3b}$

$$\begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -1 & 1 & 0 & | & 1 & 0 & 0 \\ -1 & 1 & 1 & | & 0 & 1 & 0 \\ 0 & -1 & -1 & | & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} v_{1b} \\ v_{2b} \\ v_{3b} \\ \hline v_{4b} \\ v_{5b} \\ v_{6b} \end{bmatrix} = \mathcal{J} v_b = \begin{bmatrix} K_v & | & 1_3 \\ & & t \end{bmatrix} \begin{bmatrix} v_t \\ v_r \end{bmatrix}$$

here $K_v = -K_i^T$ same

$$\frac{1}{3} v_r = -K_v v_t$$

$$v_b = \begin{bmatrix} v_t \\ v_r \end{bmatrix} = \begin{bmatrix} 1_t \\ -K_v \end{bmatrix} v_t = \begin{bmatrix} 1_t \\ K_i^T \end{bmatrix} v_t = \mathcal{E}^T v_t$$

also $i_b = \mathcal{J}^T i_r$

as the graph is a closed system

$$P_{in}(t) = \text{total power into a sphere around it} = 0$$

$$= v_{b1} i_{b1} + v_{b2} i_{b2} + \dots + v_{b6} i_{b6} = v_b^T i_b$$

$$= v^T e^T J^T i_x = 0 = \text{scalar zero}$$

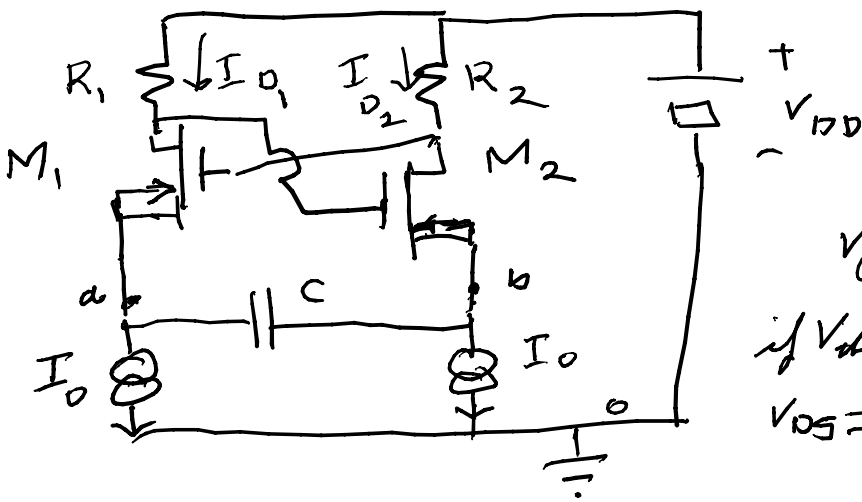
holds for anything in the branches, so choose any voltage sources as v_b & any current sources as $i_x \Rightarrow$ can cancel v & i_x from the above

$$e^T J^T = 0_{t \times r} = \left[\begin{array}{c|c} 1 & K_i \end{array} \right] \left[\begin{array}{c} K_v^T \\ \hline 1_x \end{array} \right] \quad \begin{array}{l} \text{by our} \\ \text{nice} \\ \text{numbering} \end{array}$$

$$\Rightarrow K_v^T = -K_i \quad \text{will always be true}$$

(KCL \Leftrightarrow KVL)

another example: MOS multivibrator



at perfect bias $v_{a_0} = v_{b_0}$

$$\Rightarrow V_{GS} = V_{DS} \text{ on } M_1 \text{ \& } M_2$$

if $V_{th} > 0$

$$V_{DS} = V_{GS} \geq V_{GS} - V_{th}$$

law for transistors is

$$I_D = \frac{k_p}{2} \frac{W}{L} (V_{GS} - V_{TO})^2 (1 + \lambda V_{DS}) \quad \lambda \text{ small}$$



take $\lambda = 0$ for now; at bias

$$I_0 = I_D = \frac{KPW}{2L} (V_{GS} - V_{TO})^2 \Rightarrow V_{GS} = V_{TO} + \sqrt{\frac{I_0}{\frac{KPW}{2L}}}$$

Now work with small change about the bias point

$$i_d = g_m v_{gs} \Rightarrow g_m = \left. \frac{dI_D}{dV_{GS}} \right|_{V_{GS} \text{ bias}}$$

$$= \frac{KPW}{2L} \cdot 2(V_{GS} - V_{TO}) = \frac{2I_0}{(V_{GS} - V_{TO})} \Big|_{\text{bias}}$$

Ex: 4007 $\Rightarrow KP = 20 \times 10^{-6} \text{ A/V}^2$

$V_{TO} = 1.3$

