

#1. as the other coefficients are > 0 , n and d must be > 0 to guarantee no poles or zeros in $\text{Re } s > 0$. If $d = 0$ then $n = 0$ as poles at ∞ must be simple. If $d > 0$ any pole at ∞ , of residue n/d , can be removed and the remainder will be PR. By long division $\frac{m}{d}a^2 + \frac{3}{d}a + \frac{1}{d} \Big/ \frac{m}{d}a^2 + \frac{1}{d}$ $\Rightarrow y(s) = \frac{m}{d}a + \frac{3d-m}{d^2} \frac{a + 1/d}{a + 1/d}$

To avoid a zero in $\text{Re } s > 0$ we need $3d - m \geq 0 \Rightarrow 3d \geq m \geq 0$

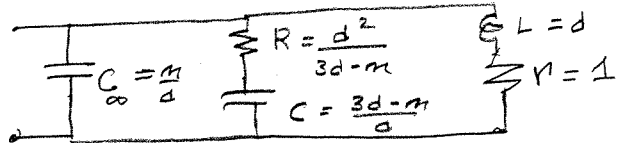
Note that $\frac{aa+b}{a+1/d} = \frac{aa}{a+1/d} + \frac{b}{a+1/d}$ is PR if $a \geq 0$ & $b \geq 0$ when $d > 0$

because $\frac{aa}{a+1/d} = \begin{cases} 0 & \text{if } a=0 \\ \frac{1}{\frac{1}{a} + \frac{1}{ad}} & \text{if } a \neq 0 \end{cases} \Rightarrow \begin{cases} \text{open} \\ R=1/a \quad C=ad \end{cases}$
 $\frac{b}{a+1/d} = \begin{cases} 0 & \text{if } b=0 \\ \frac{1}{\frac{a}{b} + \frac{1}{bd}} & \text{if } b \neq 0 \end{cases} \Rightarrow \begin{cases} \text{open (as } b=1/d \text{ not possible here)} \\ L=1/b \quad r=1/bd \end{cases}$

$\therefore y(s) = \frac{na^2 + 3a + 1}{da + 1}$ is PR if $\begin{cases} d=0 \text{ then } n=0 \\ d \neq 0 \text{ then } 3d \geq n \geq 0 \end{cases}$

b) $y(s)$ is lossless if $y(s) = -y(-s) \Rightarrow \frac{na^2 + 3a + 1}{da + 1} = -\frac{(na^2 - 3a + 1)}{-da + 1}$
 $\Rightarrow (na^2 + 3a + 1)(-da + 1) = (na^2 - 3a + 1)(-da - 1)$
 at $a=0 \Rightarrow 1 = -1$ or can never be lossless

c) synthesis; PR case

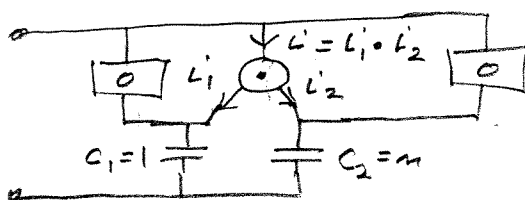


with opens, C_∞ if $n=0$, R if $3d=m$

d) If $d \neq 0$ the circuit of c) holds with possibly negative elements.

If $d=0$, $y(s) = na^2 + 3a + 1 \Rightarrow$

For $y_2 = na^2$, $n \neq 0$, we can use a current multiplier and a two nullators (to apply v onto the capacitor).



Note that a current multiplier is active as needed for a non-PR function

#1. c) alternate $Y(s) = \frac{n}{d} R = \frac{\frac{3d-n}{d^2} R + 1/d}{R + 1/d} = Y_1(s)$

$$Y_1(j\omega) = \frac{(1/d + j \frac{3d-n}{d^2} \omega)(1/d - j\omega)}{(1/d)^2 + \omega^2} \Rightarrow \text{Re } Y_1(j\omega) = \frac{(1/d)^2 + \frac{3d-n}{d^2} \omega^2}{(1/d)^2 + \omega^2} = R(\omega^2)$$

Find min Re $Y_1(j\omega)$ as can subtract this out as a resistor

$$\frac{dR(\omega^2)}{d\omega} = \frac{dR(\omega^2)}{d\omega^2} \cdot \frac{d\omega^2}{d\omega} = 2\omega \frac{dR(\omega^2)}{d\omega^2}$$

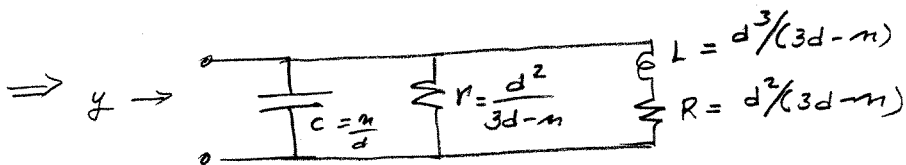
$$\frac{dR(\omega^2)}{d\omega^2} = \frac{\frac{3d-n}{d^2}}{(1/d)^2 + \omega^2} - \frac{[(1/d)^2 + \frac{3d-n}{d^2} \omega^2]}{((1/d)^2 + \omega^2)^2} = \frac{\frac{3d-n}{d^2} (1/d)^2 - (1/d)^2}{((1/d)^2 + \omega^2)^2}$$

$$= \frac{(1/d)^2 \left[\frac{3d-n}{d^2} - 1 \right]}{((1/d)^2 + \omega^2)^2} = 0 \text{ only @ } \omega = \infty \text{ if } 3d-n-d^2 \neq 0$$

$$\frac{dR(\omega^2)}{d\omega} = \frac{2\omega \left[\frac{3d-n-d^2}{d^4} \right]}{((1/d)^2 + \omega^2)^2} = 0 \Rightarrow \omega = \infty$$

$$\therefore Y_2 = Y_1 - \frac{3d-n}{d^2} = \frac{\frac{3d-n}{d^2} R + 1/d}{R + 1/d} - \frac{3d-n}{d^2} = \frac{(1/d) \left[\frac{3d-n}{d^2} \right]}{R + 1/d}$$

$$\therefore Y = \frac{n}{d} R + \frac{3d-n}{d^2} + \frac{\frac{3d-n}{d^3}}{R + 1/d} = \frac{n}{d} R + \frac{3d-n}{d^2} + \frac{1}{\frac{d^3}{3d-n} R + \frac{d^2}{3d-n}}$$

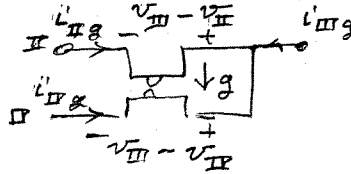


Note that this uses the minimum number of reactive elements

#2. a) tree branches: $0 = i_1 + i_4 + i_6$
 branch 2: $0 = i_2 - i_4 + i_5 - i_6$
 branch 3: $0 = i_3 + i_4 - i_5$ } $0 = C i_b \Rightarrow C = \begin{bmatrix} 1 & 0 & 0 & 1 & 0 & 1 \\ 0 & 1 & 0 & -1 & 1 & -1 \\ 0 & 0 & 1 & 1 & -1 & 0 \end{bmatrix}$

b) link branches: $0 = v_4 - v_1 + v_2 - v_3$
 branch 5: $0 = v_5 - v_2 + v_3$
 branch 6: $0 = v_6 - v_1 + v_2$ } $0 = D v_b \Rightarrow D = \begin{bmatrix} -1 & 1 & -1 & 1 & 0 & 0 \\ 0 & -1 & 1 & 0 & 1 & 0 \\ -1 & 1 & 0 & 0 & 0 & 1 \end{bmatrix}$

c) sum currents out of nodes I, II, III, IV. only the gyrator causes concern



$$-i_{IIg} = -g(v_{III} - v_{II})$$

$$-i_{IIIg} = g(v_{III} - v_{II})$$

$$i_{IIIg} = -(i_{IIg} + i_{IIIg}) = g(v_{III} - v_{II})$$

value $R = 1/G$

Then $Y_{ind} = \begin{bmatrix} a(C_2 + C_5) & -aC_2 & -aC_5 & 0 \\ -aC_2 & aC_2 + G & g & -G - g \\ -aC_5 & -g & aC_5 & g \\ 0 & -G + g & -g & G \end{bmatrix}$ note rows & columns all add to 0

d) scratch out row & column IV

$$Y = \begin{bmatrix} a(C_2 + C_5) & -aC_2 & -aC_5 \\ -aC_2 & aC_2 + G & g \\ -aC_5 & -g & aC_5 \end{bmatrix} \Rightarrow \begin{bmatrix} I_I \\ I_{II} \\ I_{III} \end{bmatrix} = Y \begin{bmatrix} V_I \\ V_{II} \\ V_{III} \end{bmatrix} \Rightarrow \begin{bmatrix} I_I \\ 0 \\ 0 \end{bmatrix} = Y \begin{bmatrix} V_{in} \\ V_{II} \\ V_{III} \end{bmatrix}$$

e) $\Rightarrow \begin{bmatrix} aC_2 \\ aC_5 \end{bmatrix} V_{in} = \begin{bmatrix} aC_2 + G & g \\ -g & aC_5 \end{bmatrix} \begin{bmatrix} V_{II} \\ V_{III} \end{bmatrix} \Rightarrow \begin{bmatrix} V_{II} \\ V_{III} \end{bmatrix} = \frac{1}{\Delta} \begin{bmatrix} aC_5 & -g \\ g & aC_2 + G \end{bmatrix} \begin{bmatrix} C_2 \\ C_5 \end{bmatrix} V_{in}$

where $\Delta = (aC_2 + G)aC_5 + g^2 = \text{determinant} \neq 0$ as $C > 0$

$$\therefore V_0 = v_{II} - v_{III} = \frac{[aC_5 \cdot aC_2 - g \cdot aC_5] - (g \cdot aC_2 + aC_2 \cdot aC_5 + aC_5 \cdot G)}{\Delta} V_{in}$$

$$\therefore \frac{V_0}{V_{in}} = \frac{-[g(C_2 + C_5) + GC_5]a}{C_2 C_5 a^2 + GC_5 a + g^2} = \frac{-[2g + G]Ca}{C^2 a^2 + GCa + g^2} \text{ if } C_2 = C_5 = C$$

$$i_3 = -g v_{III} = -g [gC_2 a + C_2 C_5 a^2 + GC_5 a] V_{in} / \Delta$$

$$= -g [C^2 a^2 + (g + G)Ca] V_{in} / \Delta \text{ if } C_2 = C_5 = C$$

$$= -gCa [Ca + (g + G)] V_{in} / \Delta$$

f) for balance

both V_0 & $i_3 = 0$ @ $a = 0$ or $g = G = 0$ or $g = -\frac{G}{2}$ @ $a = -\frac{g + G}{C} = -\frac{G}{2C}$

can use to detect g (or G) @ $a = -\frac{G}{2C}$ for $g = -\frac{G}{2}$

#3, II, $i_D = f(v_{in} - v_2, v_1) = f(u - x_3, x_2) = -I_S$

$$\left. \begin{aligned} v_L &= L \frac{di_L}{dt} \\ &= V_{dd} - R_L i_L - (v_1 + v_2) \end{aligned} \right\} \Rightarrow L \frac{dx_1}{dt} = V_{dd} - R_L x_1 - x_2 - x_3$$

$$i_L = i_D + C_1 \frac{dv_1}{dt} \Rightarrow C_1 \frac{dx_2}{dt} = x_1 - f(u - x_3, x_2)$$

$$C_2 \frac{dv_2}{dt} = C_1 \frac{dv_1}{dt} - (i_S + \frac{1}{R_A} [v_2 - V_{DD}])$$

$$\Rightarrow C_2 \frac{dx_3}{dt} = [x_1 - f(u - x_3, x_2)] + f(u - x_3, x_2) - \frac{1}{R_A} x_3 + \frac{V_{DD}}{R_A}$$

also $y = v_D = v_1 + v_2 = x_2 + x_3$

a)
$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} -\frac{R_L}{L} & -\frac{1}{L} & -\frac{1}{L} \\ \frac{1}{C_1} & 0 & 0 \\ \frac{1}{C_2} & 0 & -\frac{1}{C_2 R_A} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} V_{DD}/L \\ -f(u - x_3, x_2)/C_1 \\ V_{DD}/(R_A C_2) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} u$$

$$y = \begin{bmatrix} 0 & 1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

b) If $i_D = g_m v_{GS}$ then the equations are linear affine and all solutions are exponential with possibly time multipliers; these are not chaotic, so no chaos will result when $i_D = g_m v_{GS}$ (the solutions can be "almost periodic" which may look a bit like chaotic ones).

3. II. Synthesis with op-amps

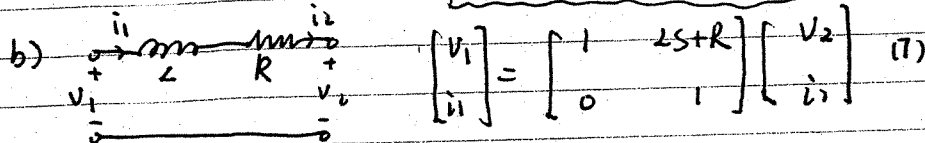
a) $V_3 = V_4 = G(s) \cdot (V_+ - V_-)$ (1)

$V_+ - V_- = \frac{R_1}{R_1 + R_2} (V_1 - V_2)$ (2)

$G(s) = \frac{G_0}{as+1}$ (5) $\therefore A_1 = \begin{bmatrix} 1 & \frac{R_1+R_2}{R_1 G_0} (as+1) \\ 0 & 1 \end{bmatrix}$ (6)

$V_1 = V_2 + \frac{R_1+R_2}{R_1 G_0} V_4$ (3)

$V_3 = V_4$ (4)



$Z = \frac{g(R_1+R_2)}{R_1 G_0}$ (8)
 $R = \frac{R_1+R_2}{R_1 G_0}$ (9)

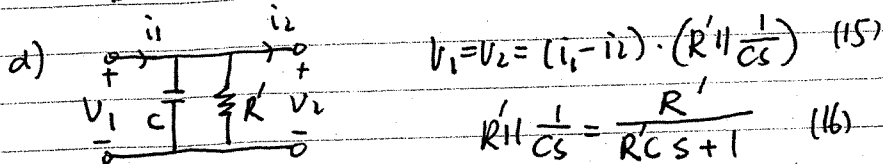
c) $V_1 = V_2 = G(s) \cdot (V_+ - V_-)$ (10)

$V_+ - V_- = \frac{R_1}{R_1 + R_2} (V_3 - V_4)$ (11)

$V_1 = V_2$ (12)

$V_3 = \frac{R_1+R_2}{R_1 G(s)} V_2 + V_4$ (13)

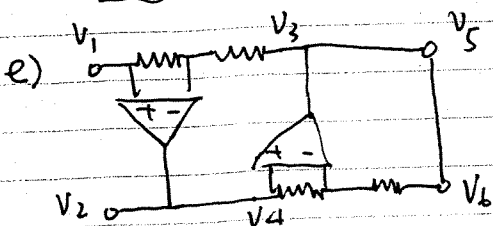
$A_2 = \begin{bmatrix} 1 & 0 \\ \frac{R_1+R_2}{R_1 G_0} (as+1) & 1 \end{bmatrix}$ (14)



$R' \parallel \frac{1}{Cs} = \frac{R'}{RCs+1}$ (16)

$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ Cs + \frac{1}{R'} & 1 \end{bmatrix} \begin{bmatrix} v_2 \\ v_1 \end{bmatrix}$ (17)

$\therefore C = \frac{g(R_1+R_2)}{R_1 G_0}$ (18)
 $R' = \frac{R_1 G_0}{R_1 + R_2}$ (19)



$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = A_1 \cdot \begin{bmatrix} v_3 \\ v_4 \end{bmatrix}$ (20) $\begin{bmatrix} v_3 \\ v_4 \end{bmatrix} = A_2 \cdot \begin{bmatrix} v_5 \\ v_6 \end{bmatrix}$ (21)

$\therefore \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = A_1 \cdot A_2 \begin{bmatrix} v_5 \\ v_6 \end{bmatrix}$ (22)

$A_1 \cdot A_2 = \begin{bmatrix} 1 + \left(\frac{R_1+R_2}{R_1 G_0}\right)^2 (as+1)^2 & \frac{R_1+R_2}{R_1 G_0} (as+1) \\ \frac{R_1+R_2}{R_1 G_0} (as+1) & 1 \end{bmatrix}$ (23)

$A = \frac{R_1+R_2}{R_1} \cdot \frac{1}{G_0} \cdot 2$

$T(s) = \frac{As + (A+1)}{As^2 + (2A^2+A)as + (A^2+A)}$ (24)

$T(s) = \frac{V_{out}}{V_{in}} = \frac{\frac{R_1+R_2}{R_1 G_0} \cdot s + \left(\frac{R_1+R_2}{R_1 G_0} + 1\right)}{\left|\frac{R_1+R_2}{R_1 G_0}\right|^2 s^2 + 2 \left[\frac{R_1+R_2}{R_1 G_0}\right] s + \left[\left(\frac{R_1+R_2}{R_1 G_0}\right)^2 + \frac{R_1+R_2}{R_1 G_0} + 1\right]}$ (24)