

Richard's function, p. 361

Hurwitz polynomial:

$P(s)$, has no zeros
in $\sigma \geq 0$

\uparrow = makes strictly
Hurwitz

o.h. nat. freq. or h.c. nat
of lossless circuit
terminated in R are
only in $\sigma < 0$

$$P(s) = E_v(s) + O_v(s)$$

$$2E_v(s) = P(s) + P^*(s) = P + P^*$$

$$2O_v(s) = P(s) - P^*(s) = P - P^*$$

lower * means $s \rightarrow -s$ and
all Hurwitz conjugate

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$$P(z) = E_v(z) \left[1 + \frac{O(z)}{E_v(z)} \right]$$

"
" $Y(z)$ of a
lossless circuit.

$$z^2 - 1 = (z+1)(z-1)$$

Given $P(z)$, is it Hurwitz
form $Y(z) = \frac{O(z)}{E_v(z)}$

if $\delta[P(z)] = \delta[Y(z)]$ then

"
degree
if $Y(z)$ is lossless then
 $P(z)$ is Hurwitz

$$\begin{aligned} \text{Eg } P(z) &= z^3 + 3z^2 + 3z + 1 \\ &= \underbrace{(3z^2 + 1)}_{ev} + z \underbrace{(z^2 + 3)}_{od} \end{aligned}$$

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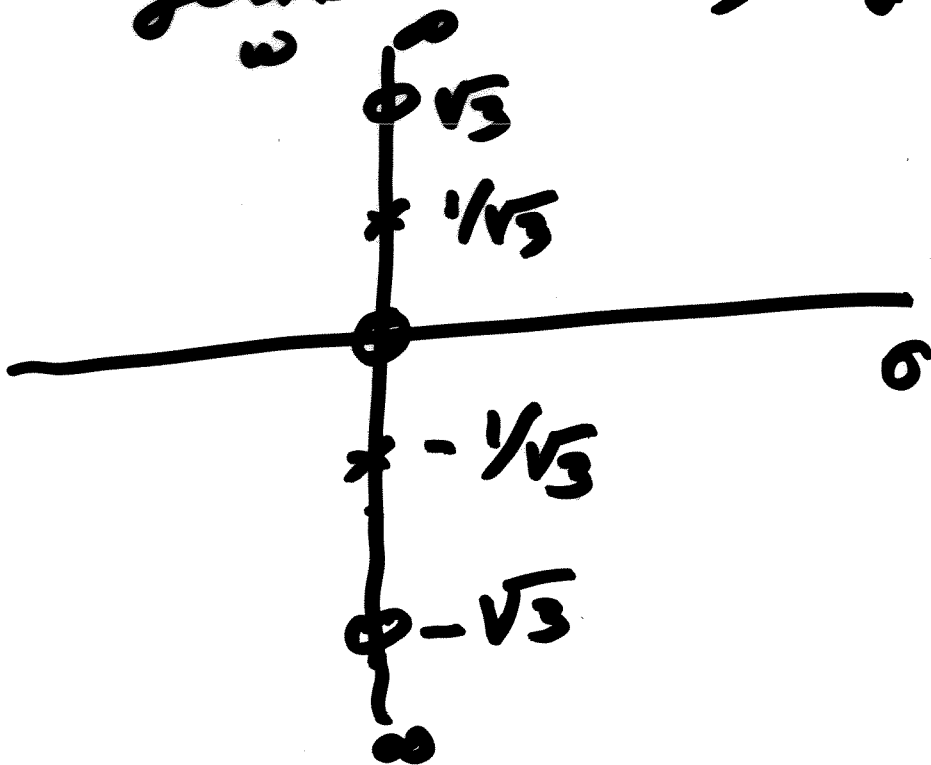
$$f(s) = \frac{s(s^2+3)}{3s^2+1} = \frac{sd}{2s}$$

$$f(1) = \frac{1(4)}{4} = +1 > 0$$

$$f(s) + f(-s) = 0$$

poles: $s = \pm j\frac{1}{\sqrt{3}}, \infty$

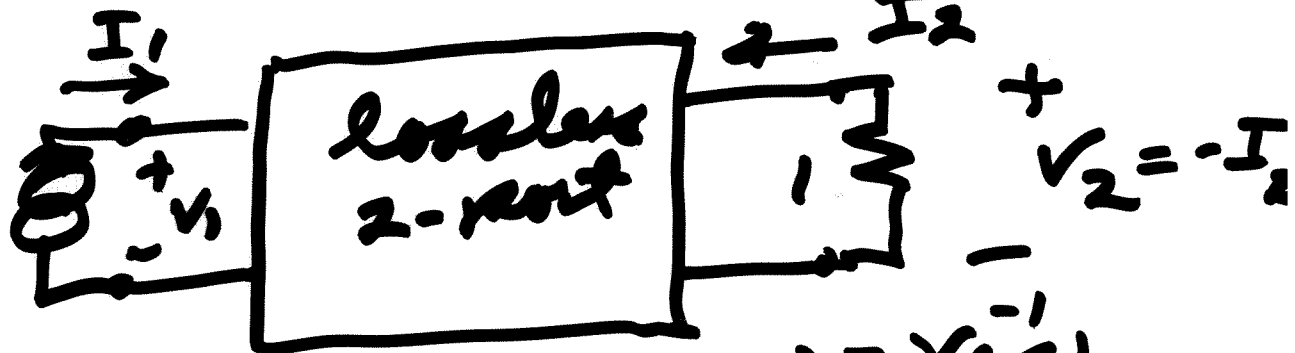
zeros: $s = 0, \pm j\sqrt{3}$



$\Rightarrow f(s)$ is Hurwitz

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Synthesis of transfer function



$$Y(\omega), Z(\omega) = Y(\omega)$$

$$I_1 = Y_{11} V_1 + Y_{12} V_2$$

$$I_2 = Y_{21} V_1 + Y_{22} V_2$$

$$-V_1 = Z_{11} I_1 + Z_{12} I_2$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2$$

$$V_2 = Z_{21} I_1 - Z_{22} V_2$$

$$(1 + Z_{22}) V_2 = Z_{21} I_1$$

$$\frac{V_2}{I_1}(\omega) = \frac{Z_{21}}{1 + Z_{22}}$$

} Hurwitz
if as
above

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V.5

Z_{21} must be odd in a

$$Z(a) = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix}$$

$v^T Z v = Z(a)$ must be PR if
 v real & for any
 v .

\Rightarrow requires all poles in Z_{12}
and Z_{21} must be in Z_{11}, Z_{22}

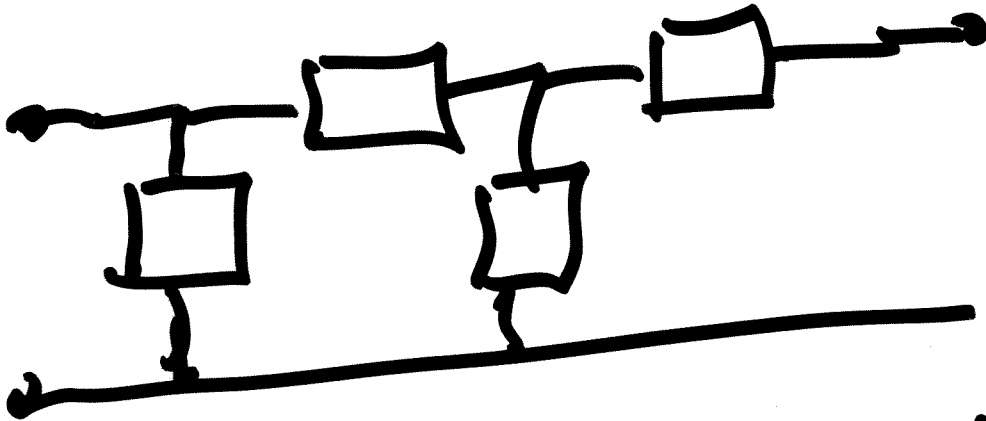
as Z_{11} & Z_{22} are lossless

\Rightarrow all poles of Z_{12} and Z_{21}
are on $j\omega$ axis; make
partial fraction expansion

$$Z_{21} = \frac{k_0}{a} + k_{\infty} a + \sum \frac{k_i}{a + j\omega_i} + \frac{k_i^*}{a - j\omega_i}$$

some coeff can be negative
but still $Z_{21}(a) = -Z_{21}(-a)$

Synthesis for lossless
ladders:



zeros of transmission are
where series arms are
open circuits ($Z = \infty$)
and shunt arms are
short circuits ($Z = 0$)
 \therefore interested in poles of
 Z in series & poles of Y
in shunt arms.

Ex:

$$\frac{V_2(s)}{I_1} = \frac{c}{s^3 + 3s^2 + 3s + 1}$$

$c = \text{real constant}$ [has 3 zeros of transmission at $s = \infty$]

$$= \frac{Z_{21}}{1 + Z_{22}}$$

need to divide out the odd part of the denominator to make Z_{21} odd

$$\frac{V_2}{I_1} = \frac{c / (s^3 + 3s)}{1 + \frac{3s^2 + 1}{s^3 + 3s}}$$

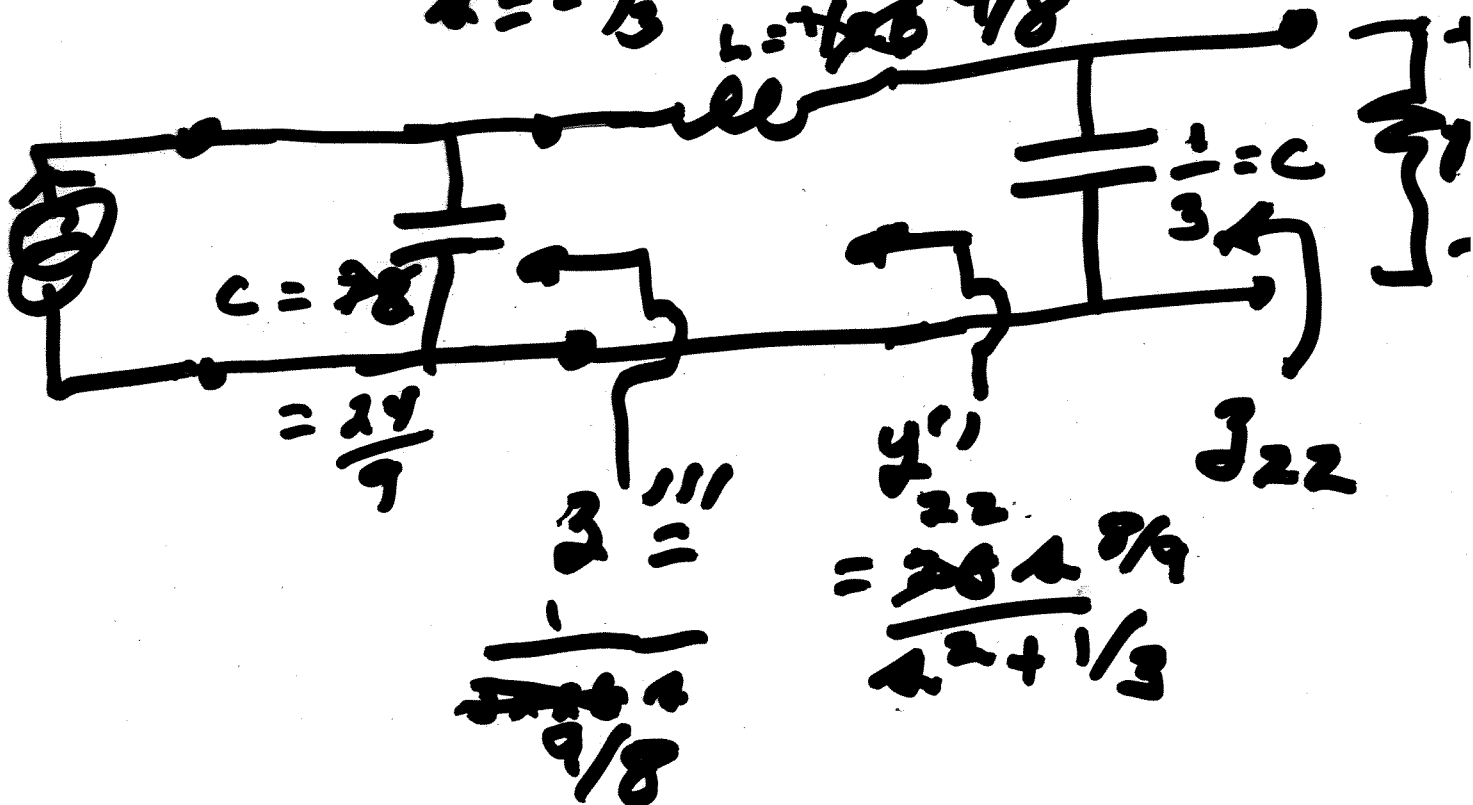
$$Z_{21} = \frac{c}{s(s^2 + 3)} ; Z_{22} = \frac{3(s^2 + 1/3)}{s(s^2 + 3)}$$

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Synthesize $Z_{22}(s)$ so
 shunt arms have $z = \infty$ at
 $s = \infty$, series arms have
 $z = \infty$ at ∞ .

$$\frac{1}{Z_{22}} = Y'_{22} = \frac{s^3 + 3s}{3s^2 + 1} = \frac{s}{3} + \frac{ks}{s^2 + 1/3}$$

$$k_1 = \frac{s^2 + 3}{3} \Big|_{s = -1/3} = \frac{-1/9 + 3}{3} = \frac{28}{27} \quad \frac{8}{9}$$

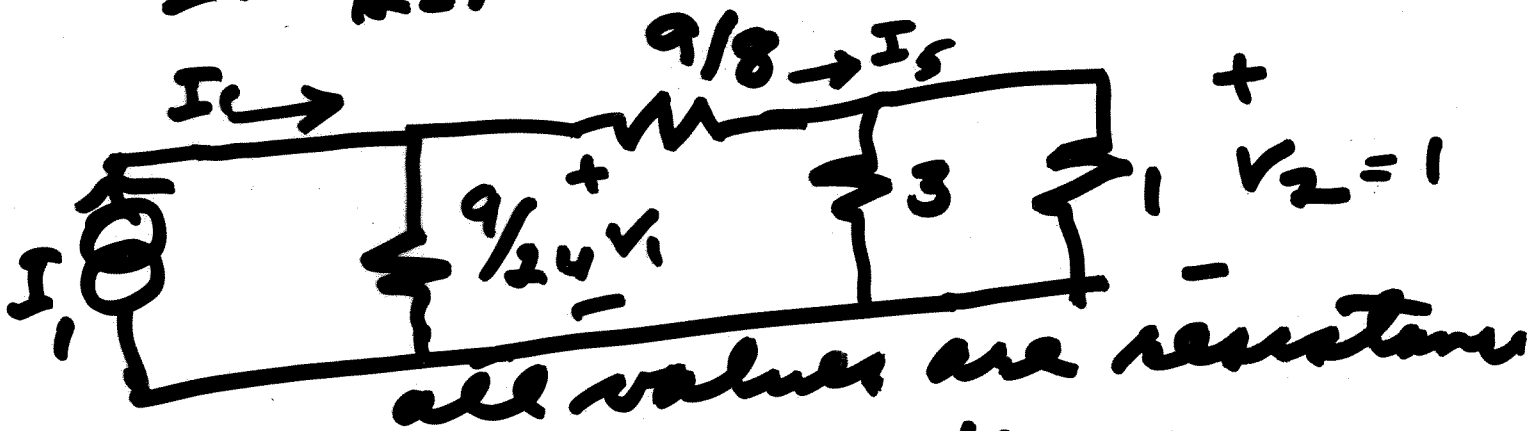


$$\frac{V_2}{I_1} = \frac{R}{R^3 + 3R^2 + 3R + 1}$$

to find R : let $a=1$

then $La=L$, $Ca=C$ (at resistors)

$$\frac{V_2}{I_1} \Big|_{R=1} = \frac{1}{1+3+3+1} = \frac{1}{8}$$



$$I_5 = 1 \cdot (1 + \frac{1}{3}) = \frac{4}{3} \text{ amp}$$

$$V_1 = V_2 + I_5 \cdot \frac{9}{8} = 1 + \frac{3}{2} = \frac{5}{2} \text{ volt}$$

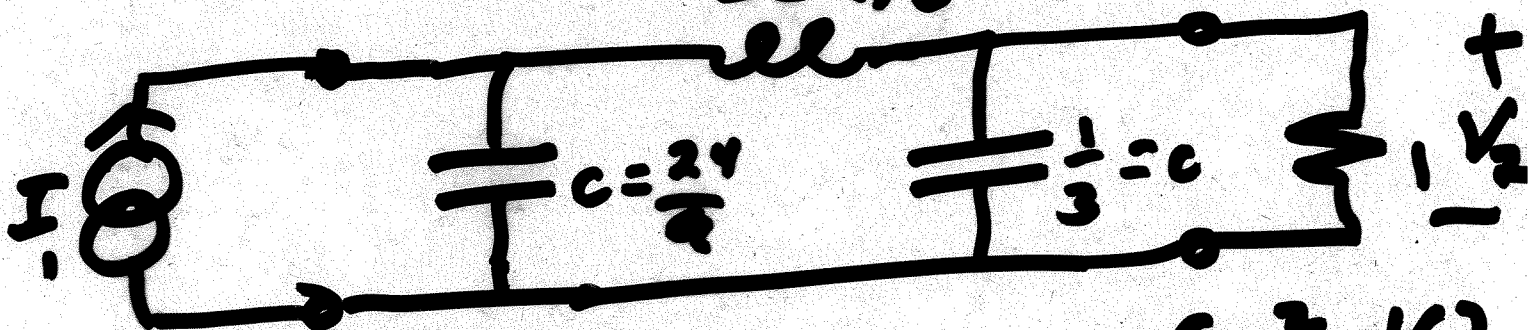
$$I_1 = \frac{24}{9} \cdot V_1 + I_5 = \frac{24}{9} \cdot \frac{5}{2} + \frac{4}{3} = \frac{60}{9} + \frac{12}{9}$$

$$= \frac{72}{9} = 8 \text{ amp} \quad \text{or} \quad \frac{V_2}{I_1} = \frac{1}{8} = \frac{R}{8}$$

$$R = 1$$

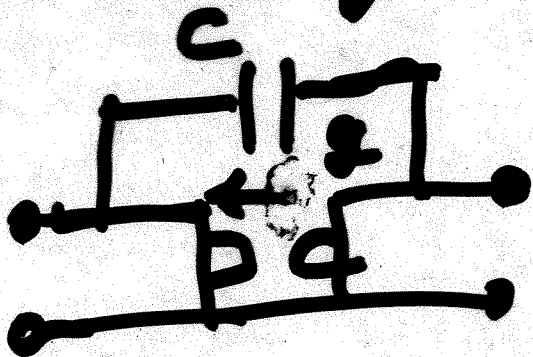
$$\frac{V_2}{I_1}(s) = \frac{1}{s^3 + 3s^2 + 3s + 1}$$

$L = 9/8$



$$z_{21} = \frac{s=1}{s(s^2+3)}, \quad z_{22} = \frac{3(s^2+1/3)}{s(s^2+3)}$$

Richard's' function:



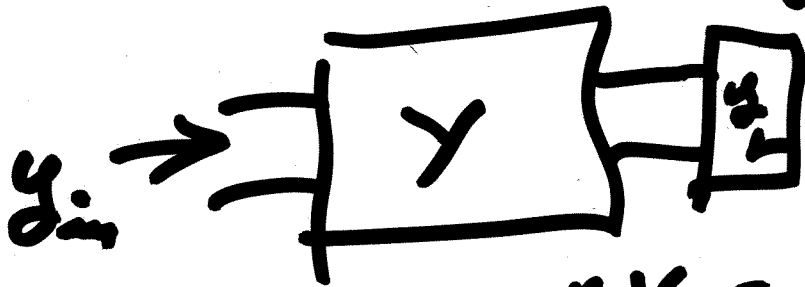
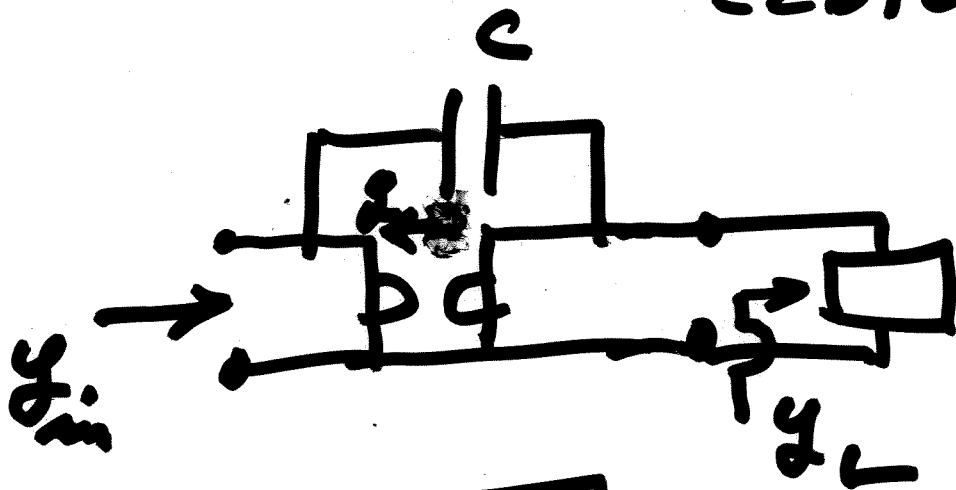
$$y = \begin{bmatrix} 0 & -g \\ +g & 0 \end{bmatrix}$$

$$Y(s) = \begin{bmatrix} cs & -(g+cs) \\ g-cs & cs \end{bmatrix} \quad y + y^T = 0_2$$

$$y_{sc} = \begin{bmatrix} cs & -cs \\ -cs & cs \end{bmatrix}$$

a lossless
2-port

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$$I_2 = -Y_L V_2 =$$

$$-Y_L V_2 = I_2 = Y_{21} V_1 + Y_{22} V_2$$

$$-(Y_L + Y_{22})^{-1} Y_{21} V_1 = V_2$$

$$I_1 = Y_{in} V_1 = Y_{11} V_1 + Y_{12} V_2$$

$$= \left[Y_{11} + Y_{12} \left[-(Y_L + Y_{22})^{-1} Y_{21} \right] \right] V_1$$

$$Y_{in} = \frac{\Delta Y + Y_{11} Y_L}{Y_L + Y_{22}}$$

$$\Delta y = y_{11}y_{22} - y_{12}y_{21}$$

$$= (Ca)^2 + (g+Ca)(g-Ca)$$

$$= g^2$$

$$\therefore y_{in} = \frac{g^2 + Ca \cdot y_L}{y_L + Ca}$$

is PR
if y_L is PR

to get y_L of y_{in} :

$$y_{in} \cdot y_L + Ca \cdot y_{in} = g^2 + Ca \cdot y_L$$

$$(y_{in} - Ca) y_L = g^2 - Ca \cdot y_{in}$$

$$y_L^{(a)} = \frac{g^2 - Ca \cdot y_{in}(a)}{y_{in}(a) - Ca}$$

here y_L is PR if y_{in} is PR

identify with a bilinear function p. 361

$$= \frac{a y(a) - a y(a)}{a y(a) - a y(a)}$$