

ENEE681

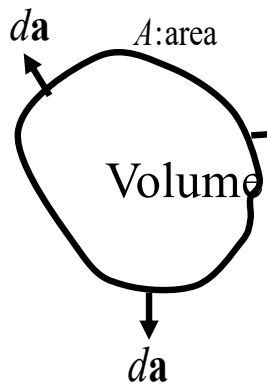
Lecture 2
Inductance
Mutual Inductance
Skin effect

Electrostatics

Coulomb's Law:

$$\mathbf{E}(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \int_V \frac{\rho(\mathbf{r}')(\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3} d^3r'$$

Gauss' Law:



$$\oint_S \vec{\mathbf{E}} \cdot d\vec{\mathbf{A}} = \frac{Q_{in}}{\epsilon_0} = \frac{1}{\epsilon_0} \int_V \rho d^3r$$
$$\oint_{loop} \vec{\mathbf{E}} \cdot d\vec{\mathbf{l}} = 0$$

Poisson Equation:

$$\nabla \cdot \vec{\mathbf{E}} = \frac{\rho}{\epsilon_0}$$
$$\nabla \times \vec{\mathbf{E}} = 0$$

Magnetostatics

Biot-Savart Law:

$$\mathbf{B}(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_V \frac{\mathbf{J}(\mathbf{r}') \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3} d^3r'$$

Ampere's Law:

$$\begin{aligned} \oint_{loop} \vec{\mathbf{B}} \cdot d\vec{\mathbf{S}} &= \mu_0 I_{enclosed} \\ &= \mu_0 \oint_S \vec{\mathbf{J}} \cdot d\vec{\mathbf{A}} \\ \oint_S \vec{\mathbf{B}} \cdot d\vec{\mathbf{A}} &= 0 \end{aligned}$$

Gauss' Law:

$$\begin{aligned} \nabla \times \vec{\mathbf{B}} &= \mu_0 \vec{\mathbf{J}} \\ \nabla \cdot \vec{\mathbf{B}} &= 0 \end{aligned}$$

Dynamic Fields

Faraday's Law

Maxwell's Displacement Current

Integrals around closed loops

Faraday's Law:

$$\oint_{loop} \vec{\mathbf{E}} \cdot d\vec{\mathbf{l}} = - \int_S d\vec{\mathbf{A}} \cdot \frac{\partial \vec{\mathbf{B}}}{\partial t}$$

$$\nabla \times \vec{\mathbf{E}} = - \frac{\partial \vec{\mathbf{B}}}{\partial t}$$

Ampere's Law:

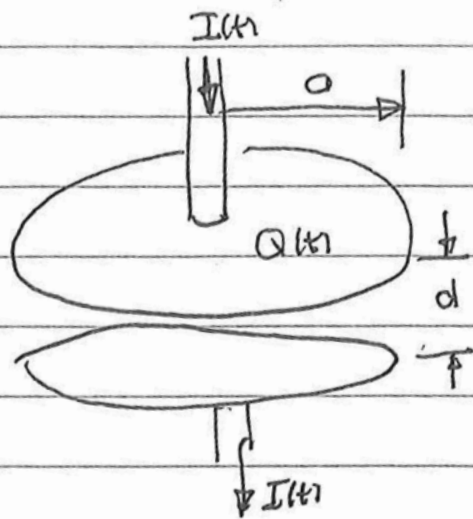
$$\oint_{Loop} \vec{\mathbf{B}}(\vec{\mathbf{r}}) \cdot d\vec{\mathbf{l}} = \mu_0 \int_S d\vec{\mathbf{A}} \cdot \left[\vec{\mathbf{J}} + \epsilon_0 \frac{\partial \vec{\mathbf{E}}}{\partial t} \right]$$

$$\nabla \times \vec{\mathbf{B}}(\vec{\mathbf{r}}) = \mu_0 \left[\vec{\mathbf{J}} + \epsilon_0 \frac{\partial \vec{\mathbf{E}}}{\partial t} \right]$$

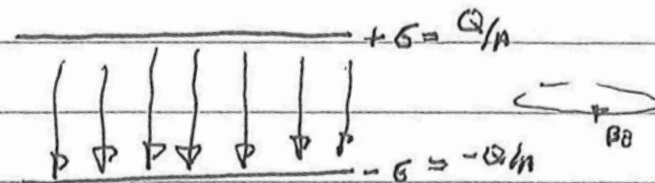
Displacement Current

Problem ~~4.3~~

Find field inside



Start with the assumption that fields are electrostatic



$$-\epsilon_0 E_z = \sigma = Q/A \quad A = \pi a^2$$

$$E_z = -\frac{Q(t)}{\epsilon_0 A}$$

$$\frac{dQ}{dt} = I$$

Ampere's Law with Displacement Current

$$(\nabla \times \mathbf{E})_z = \mu_0 \epsilon_0 \frac{\partial E_z}{\partial t} \quad \frac{1}{r} \frac{\partial}{\partial r} r B_\theta = \epsilon_0 \mu_0 \frac{\partial E_z}{\partial t}$$

$$B_\theta = \frac{r}{2} \epsilon_0 \mu_0 \frac{\partial E_z}{\partial t} = \frac{r}{2} \mu_0 \left(-\frac{1}{A} \frac{dI}{dt} \right) = -\frac{\mu_0 r}{2A} I(t)$$

Faraday's Law

$$-\frac{\partial B_\theta}{\partial t} = (\nabla \times \mathbf{E})_\theta = -\frac{\partial}{\partial r} E_z$$

$$E_z(r) = E_z(0) + \int_0^r dr' \frac{\partial}{\partial t} \left(\frac{\mu_0 r'}{2} \frac{\partial E_z}{\partial t} \right) = E_z(0) + \frac{\epsilon_0 \mu_0 r^2}{4} \frac{\partial^2 E_z(0)}{\partial t^2}$$

Suppose $E_z(0) = E_0 \sin \omega t$

$$E_z(r) = E_0 \sin \omega t \left\{ 1 - \frac{\epsilon_0 \mu_0 r^2 \omega^2}{4} \right\}$$

$$\lambda = c/f$$

$$\text{Require } \frac{\epsilon_0 \mu_0 a^2 \omega^2}{4} \ll 1$$

$$\frac{a^2 \omega^2}{4c^2} \ll 1 \quad \left(\frac{\pi a}{\lambda} \right)^2 \ll 1$$

Actually we should solve

$$\frac{1}{r} \frac{\partial}{\partial r} r B_{\theta} = \epsilon_0 \mu_0 \frac{\partial E_z}{\partial t}$$

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial B_{\theta}}{\partial t} = \epsilon_0 \mu_0 \frac{\partial^2 E_z}{\partial t^2}$$

$$\frac{\partial B_{\theta}}{\partial t} = \frac{\partial}{\partial r} E_z$$

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial E_z}{\partial t} = \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2}$$

$$E_z = \hat{E}_z \ln \cos \omega t \quad \text{Re} \{ \hat{E}_z \ln e^{-i\omega t} \}$$

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \hat{E}_z(r)}{\partial r} + \frac{\omega^2}{c^2} \hat{E}_z(r) = 0 \quad \text{Bessel's Eqn. (3.7)}$$

Bessel's Eqn

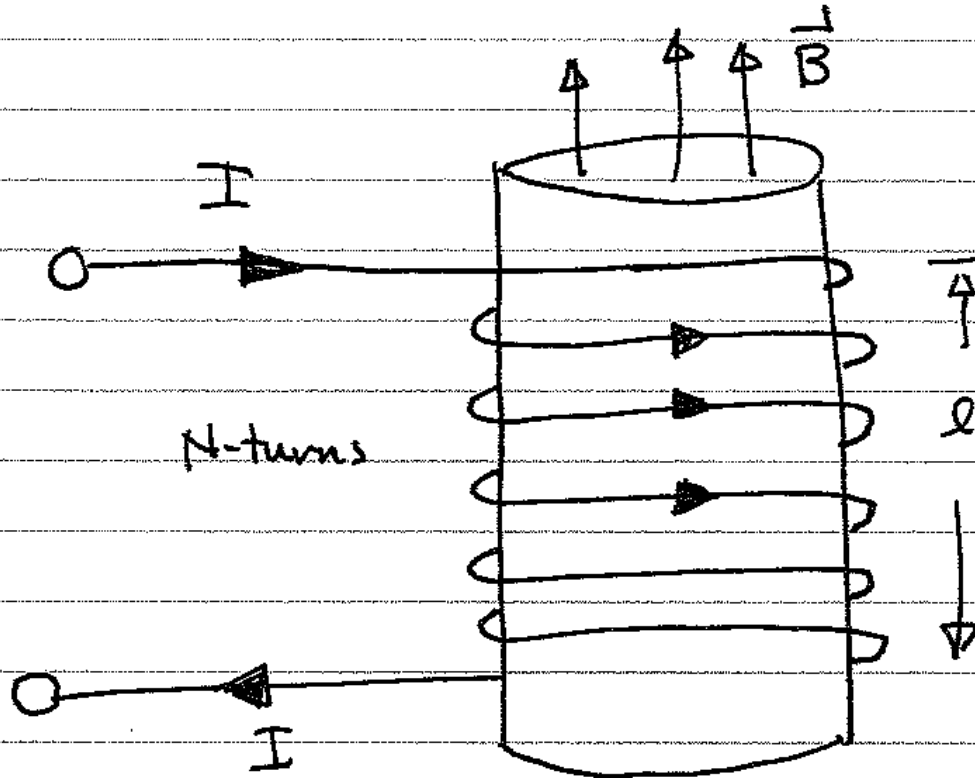
$$\hat{E}_z = E_0 J_0\left(\frac{\omega}{c} r\right)$$

$$J_0(x) \approx 1 - \frac{1}{4} x^2 + o(x^4)$$

$$J_0(x) = \sum_{m=0}^{\infty} \frac{(-1)^m (x/2)^{2m}}{(m!)^2}$$

$$\frac{1}{x} \frac{\partial}{\partial x} x \frac{\partial}{\partial x} J_0 + J_0 = 0$$

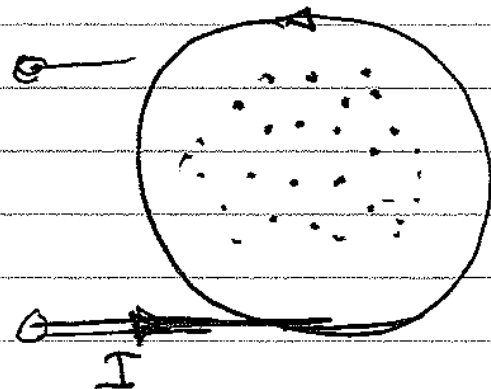
Consider a solenoid with N turns



Put your right thumb in direction of I . Fingers give direction of \vec{B} (up inside)

$$|\vec{B}| = \frac{\mu_0 I N}{l}$$

VIEW FROM ABOVE



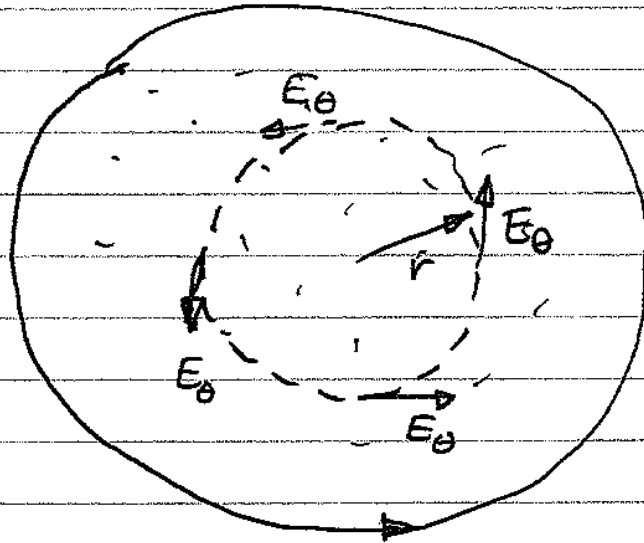
\vec{B} out of page

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I$$

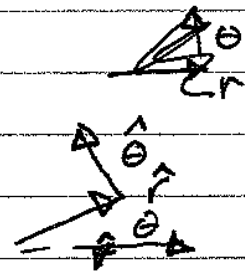
$$lB = \mu_0 NI$$

Calculate induced \vec{E} -field as a function of r

Consider a
loop of
radius r



\vec{B} - out of page
 $\vec{B} = B_z \hat{k}$



Q: Which direction is
 \vec{E} ? $+\hat{\theta}$ or $-\hat{\theta}$

Ans: We don't know, is B increasing or decreasing?

$$E_\theta = -\frac{r}{2} \frac{\partial B_z}{\partial t}$$

Faraday's Law for Stationary Loops

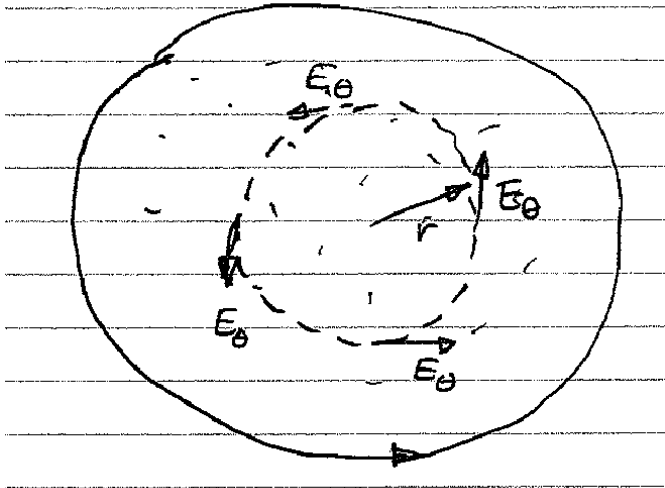
$$\oint_{loop} \vec{E} \cdot d\mathbf{l} = - \int_{Area} \frac{\partial \vec{B}}{\partial t} \cdot d\vec{A}$$

CCW

Out of page (+z)

Only time derivative of B enters

Call component of E in θ direction $E_\theta(r,t)$



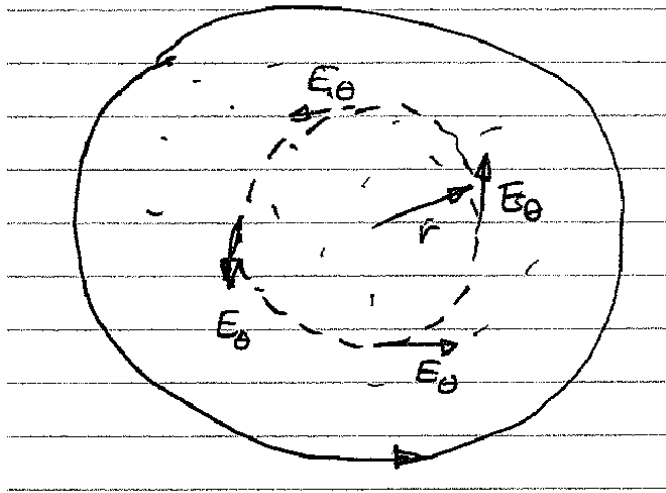
$$\oint_{loop} \vec{E} \cdot d\mathbf{l} = 2\pi r E_\theta(r,t)$$

$$\int_{Area} \frac{\partial \vec{B}}{\partial t} \cdot d\vec{A} = \pi r^2 \frac{\partial B_z}{\partial t}$$

Therefore:

$$E_\theta(r,t) = -\frac{r}{2} \frac{\partial B_z}{\partial t}$$

Is Lenz' s law satisfied ????



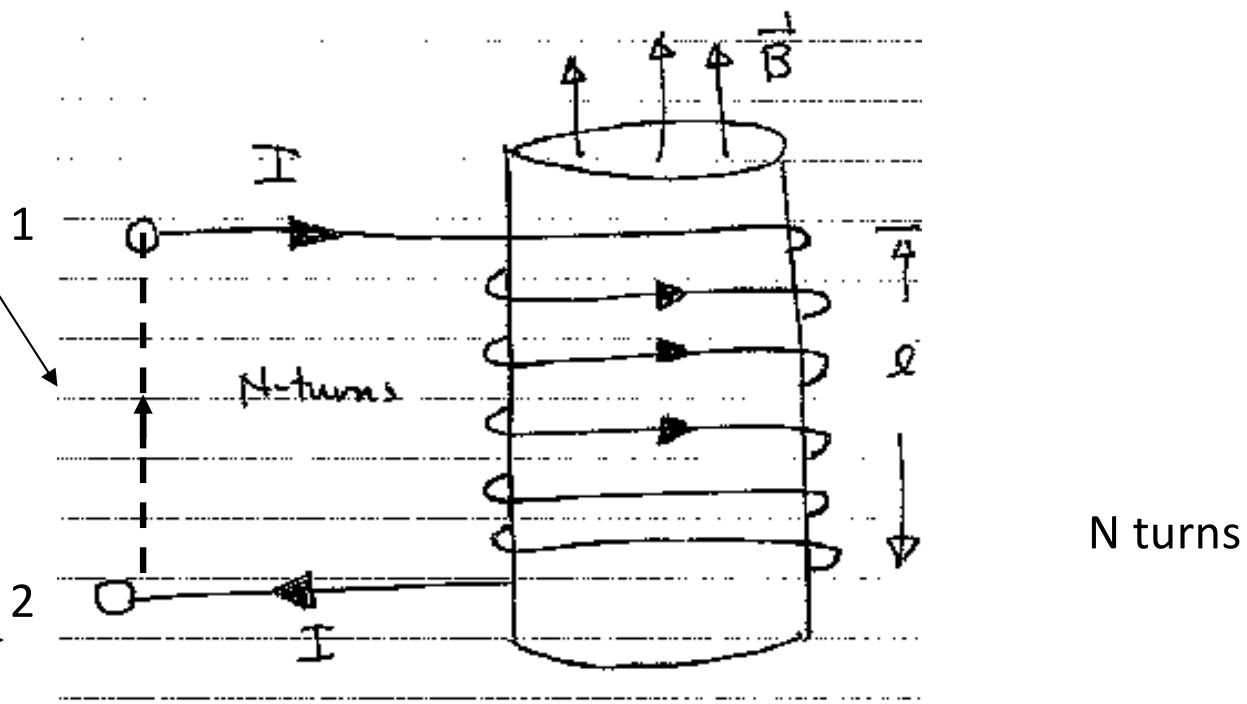
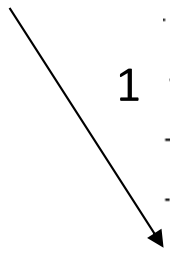
$$E_\theta(r,t) = -\frac{r}{2} \frac{\partial B_z}{\partial t}$$

B_z - out of page and increasing

An induced current would flow Counterclockwise

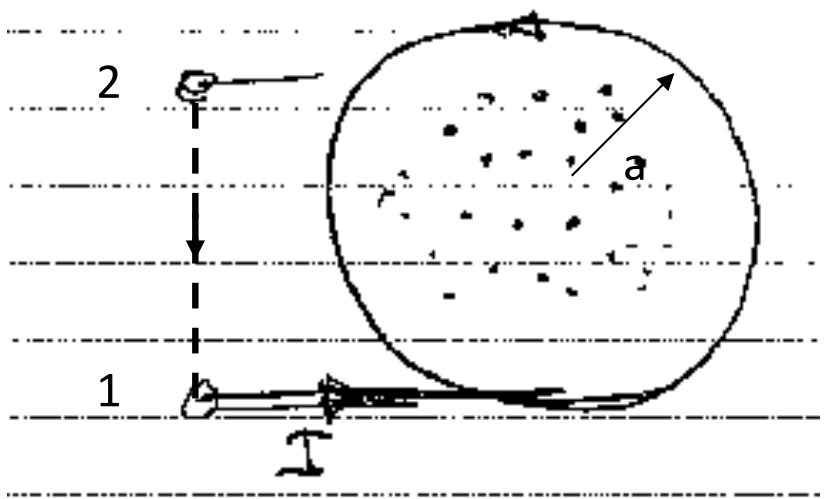
What is

$$\int_2^1 \vec{E} \cdot d\vec{l}$$



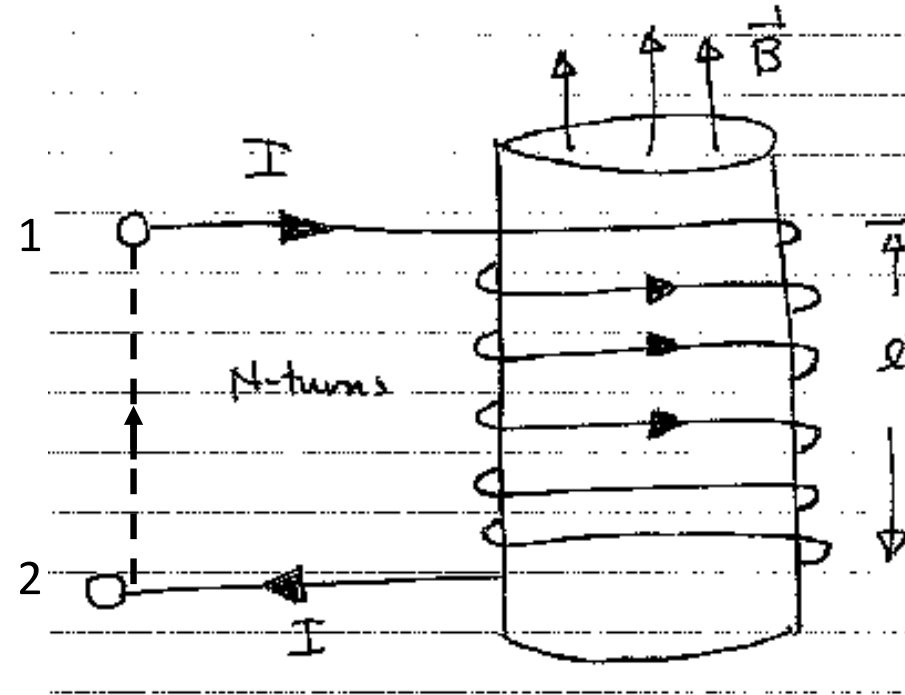
$$\int_2^1 \vec{E} \cdot d\vec{l} + \int_{1, \text{ wire}}^2 \vec{E} \cdot d\vec{l}$$

$$= \oint_{\text{Loop}} \vec{E} \cdot d\vec{l} = -N\pi a^2 \frac{\partial B_z}{\partial t}$$



Top view

Inductance



$$\int_2^1 \vec{\mathbf{E}} \cdot d\vec{\mathbf{l}} = -N\pi a^2 \frac{\partial B_z}{\partial t}$$

$$B_z = \frac{\mu_0 NI}{l}$$

$$V_1 - V_2 = - \int_2^1 \vec{\mathbf{E}} \cdot d\vec{\mathbf{l}} = \frac{\mu_0 N^2 \pi a^2}{l} \frac{dI}{dt} = L \frac{dI}{dt}$$

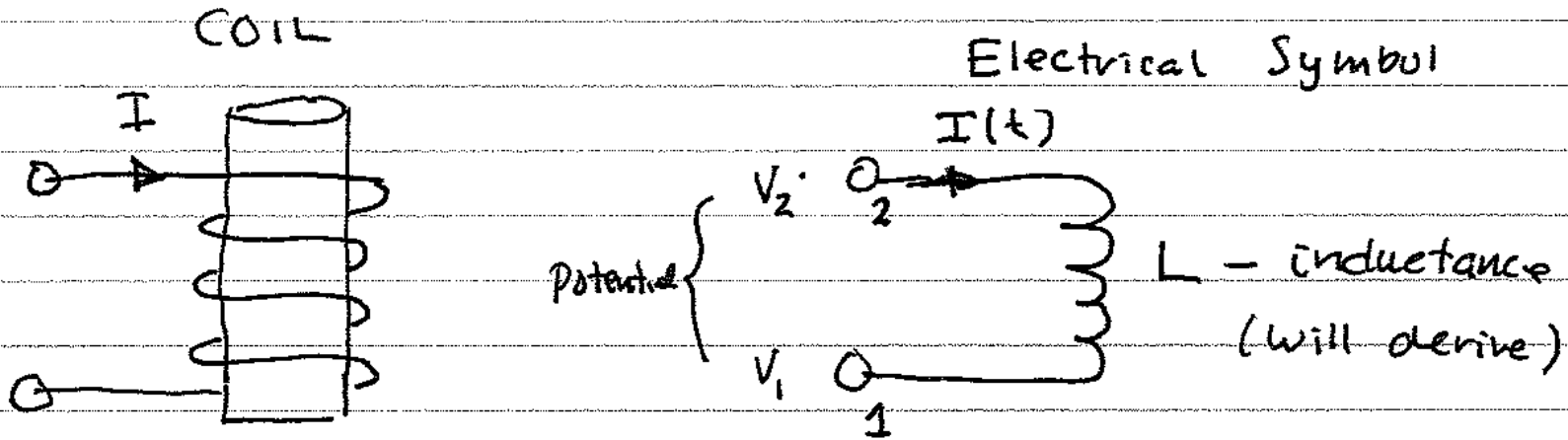
$$L = \frac{\mu_0 N^2 \pi a^2}{l}$$

Depends in geometry of coil, not I

Inductors

An inductor is a coil of wire

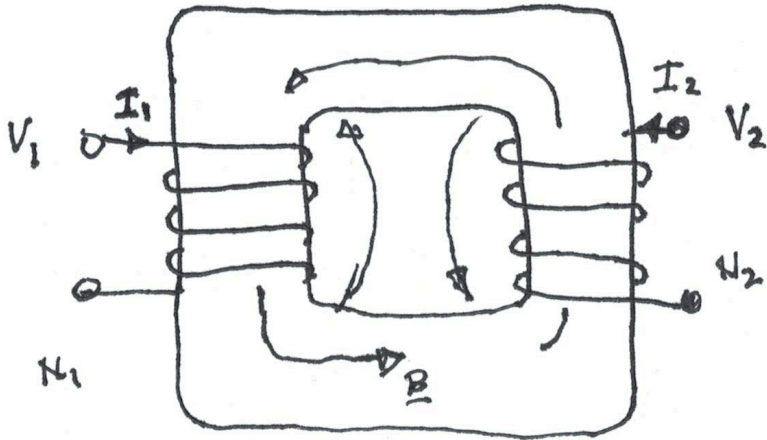
Any length of wire has inductance: but it's usually negligible



Engineering sign convention for labeling voltage and current

$$V_L = V(2) - V(1) = L \frac{dI}{dt}$$

Transformer



$$\begin{pmatrix} \psi_1 \\ \psi_2 \end{pmatrix} = \begin{bmatrix} L_{11} & L_{12} \\ L_{21} & L_{22} \end{bmatrix} \begin{pmatrix} I_1 \\ I_2 \end{pmatrix}$$

$$\begin{pmatrix} V_1 \\ V_2 \end{pmatrix} = \begin{bmatrix} L_{11} & L_{12} \\ L_{21} & L_{22} \end{bmatrix} \begin{pmatrix} dI_1 / dt \\ dI_2 / dt \end{pmatrix}$$

Inductance Matrix

$$\det[\mathbf{L}] = L_{11}L_{22} - L_{12}L_{21} > 0$$

Reciprocal

$$L_{12} = L_{21}$$

Coupling coefficient, $-1 < k < 1$

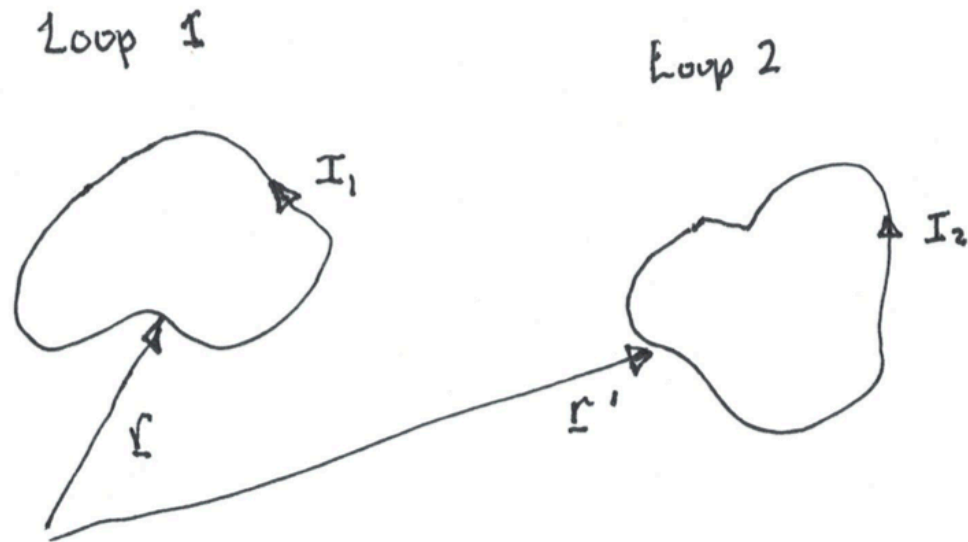
$$L_{12} = k\sqrt{L_{11}L_{22}}$$

Symmetry of Inductance Matrix

$$\mathbf{B}_{12}(\mathbf{r}) = \frac{\mu_0}{4\pi} \int_V \frac{\mathbf{J}_2(\mathbf{r}') \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3} d^3r'$$

$$= \frac{\mu_0 I_2}{4\pi} \int_{L_2} \frac{d\mathbf{l}' \times (\mathbf{r} - \mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|^3}$$

$$\psi_{12} = \int_{S_1} d\mathbf{a} \cdot \mathbf{B}_{12}(\mathbf{r})$$



Step 1

$$\mathbf{B}_{12}(\mathbf{r}) = \nabla \times \mathbf{A}_{12}(\mathbf{r})$$

$$\mathbf{A}_{12}(\mathbf{r}) = \frac{\mu_0 I_2}{4\pi} \int_{L_2} \frac{d\mathbf{l}'}{|\mathbf{r} - \mathbf{r}'|}$$

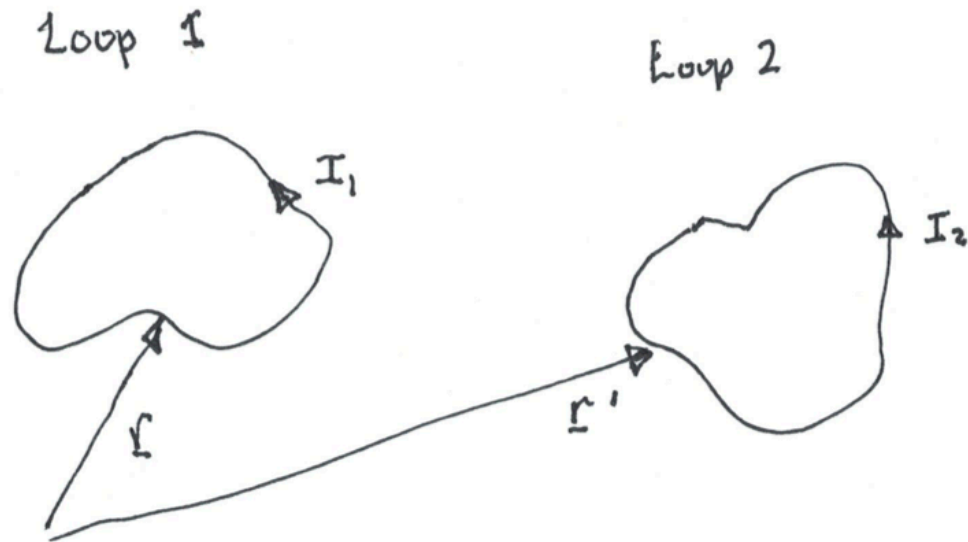
$$\nabla \times \mathbf{A}_{12}(\mathbf{r}) = \frac{\mu_0 I_2}{4\pi} \int_{L_2} \nabla \times \frac{d\mathbf{l}'}{|\mathbf{r} - \mathbf{r}'|} = -\frac{\mu_0 I_2}{4\pi} \int_{L_2} d\mathbf{l}' \times \nabla \frac{1}{|\mathbf{r} - \mathbf{r}'|}$$

$$= \frac{\mu_0 I_2}{4\pi} \int_{L_2} d\mathbf{l}' \times \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|^3} = \mathbf{B}_{12}(\mathbf{r})$$

$$\begin{aligned}\nabla \times \mathbf{A}_{12}(\mathbf{r}) &= \frac{\mu_0 I_2}{4\pi} \int_{L_2} \nabla \times \frac{d\mathbf{l}'}{|\mathbf{r} - \mathbf{r}'|} = -\frac{\mu_0 I_2}{4\pi} \int_{L_2} d\mathbf{l}' \times \nabla \frac{1}{|\mathbf{r} - \mathbf{r}'|} \\ &= \frac{\mu_0 I_2}{4\pi} \int_{L_2} d\mathbf{l}' \times \frac{\mathbf{r} - \mathbf{r}'}{|\mathbf{r} - \mathbf{r}'|^3} = \mathbf{B}_{12}(\mathbf{r})\end{aligned}$$

Step 2

$$\begin{aligned}\psi_{12} &= \int_{S1} d\mathbf{a} \cdot \mathbf{B}_{12}(\mathbf{r}) \\ &= \int_{S1} d\mathbf{a} \cdot \nabla \times \mathbf{A}_{12}(\mathbf{r}) \\ &= \int_{L1} d\mathbf{l} \cdot \mathbf{A}_{12}(\mathbf{r})\end{aligned}$$



$$\psi_{12} = \int_{L1} d\mathbf{l} \cdot \mathbf{A}_{12}(\mathbf{r}) = \frac{\mu_0 I_2}{4\pi} \int_{L1} \int_{L2} \frac{d\mathbf{l} \cdot d\mathbf{l}'}{|\mathbf{r} - \mathbf{r}'|} = L_{12} I_2$$

$$L_{12} = L_{21}$$

$$U = \int_{-\infty}^t dt' \mathbf{V}(t') \cdot \mathbf{I}(t') = \int_{-\infty}^t dt' \mathbf{I}(t') \cdot \mathbf{L} \cdot \frac{d}{dt} \mathbf{I}(t') = \frac{1}{2} \mathbf{I}(t) \cdot \mathbf{L} \cdot \mathbf{I}(t) \geq 0$$

Energy stored must be positive

All diagonal elements of \mathbf{L} must be positive

Eigenvalues and Eigenfunctions of \mathbf{L} : $\mathbf{L} \mathbf{I}_\mu = L_\mu \mathbf{I}_\mu$

Suppose $\mathbf{I} = \mathbf{I}_\mu$, $U = \frac{1}{2} L_\mu |\mathbf{I}_\mu|^2 \rightarrow L_\mu \geq 0$ all $\mu \rightarrow \det[\mathbf{L}] \geq 0$

What about self Inductance?

$$\psi_{11} = \int_{L1} d\mathbf{l} \cdot \mathbf{A}_{11}(\mathbf{r}) = \frac{\mu_0 I_1}{4\pi} \int_{L1} \int_{L1} \frac{d\mathbf{l} \cdot d\mathbf{l}'}{|\mathbf{r} - \mathbf{r}'|} = L_{11} I_1$$

For wire of vanishing thickness $L_{11} \rightarrow \infty$

$$\oint B dl = 2\pi r B_\theta(r) = \mu_0 I \rightarrow B_\theta(r) = \frac{\mu_0 I}{2\pi r}$$



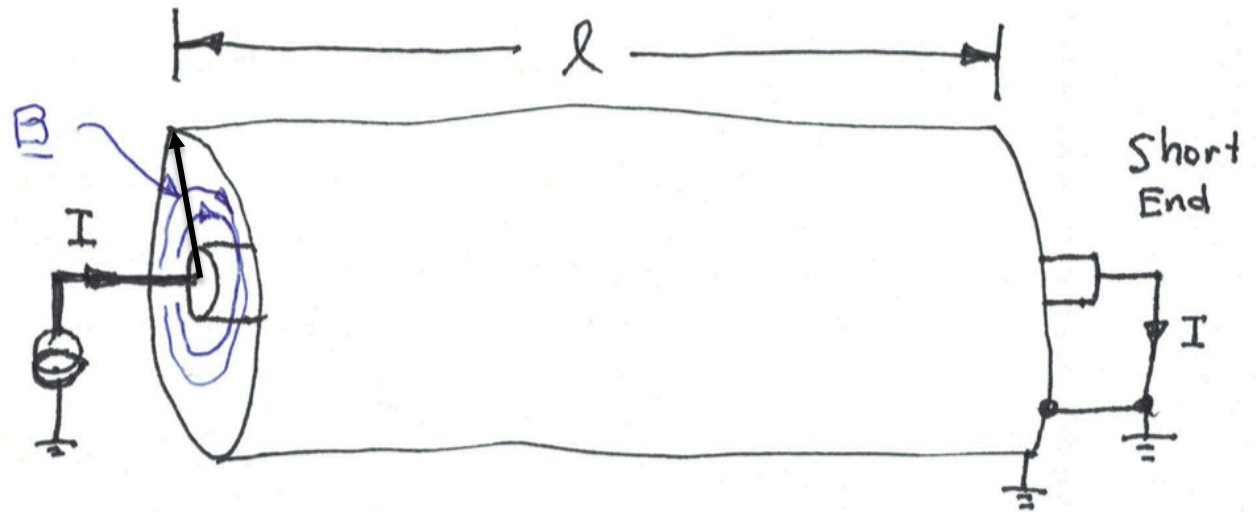
L' and C' for coaxial line

$$B_{\theta}(r) = \frac{\mu I}{2\pi r}$$

$$\psi = \int_a^b dr \int_0^l dz \frac{\mu I}{2\pi r} = \frac{\mu I l}{2\pi} \ln\left(\frac{b}{a}\right)$$

Inductance/length

$$L' = \psi / I = \frac{\mu}{2\pi} \ln\left(\frac{b}{a}\right)$$

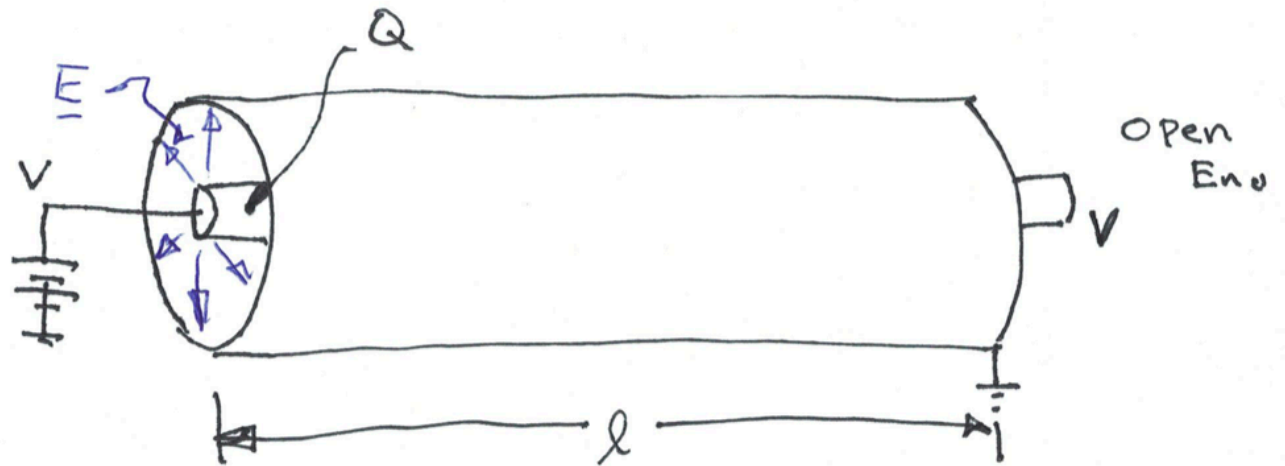


$$E_r(r) = \frac{Q/l}{2\pi\epsilon r}$$

$$V = \int_a^b dr E_r = \frac{Q/l}{2\pi\epsilon} \ln\left(\frac{b}{a}\right)$$

Capacitance/length

$$C' = \frac{Q/l}{V} = 2\pi\epsilon / \ln\left(\frac{b}{a}\right)$$



Coaxial Transmission Line

Inductance/length

$$L' = \frac{\mu}{2\pi} \ln\left(\frac{b}{a}\right)$$

Capacitance/length

$$C' = 2\pi\epsilon / \ln\left(\frac{b}{a}\right)$$

$$\left. \begin{array}{l} a \rightarrow 0 \\ b \rightarrow \infty \end{array} \right\} L \rightarrow \infty$$

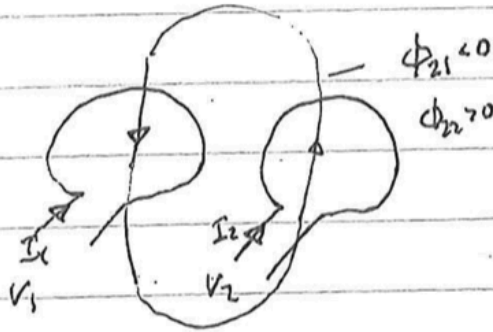
Propagation Speed

$$v^2 = 1 / (L'C') = 1 / (\mu\epsilon)$$

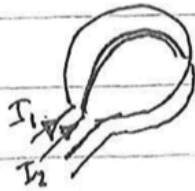
Characteristic Impedance

$$Z_0 = \sqrt{L' / C'} = \sqrt{\frac{\mu}{\epsilon} \left[\frac{1}{2\pi} \ln\left(\frac{b}{a}\right) \right]}$$

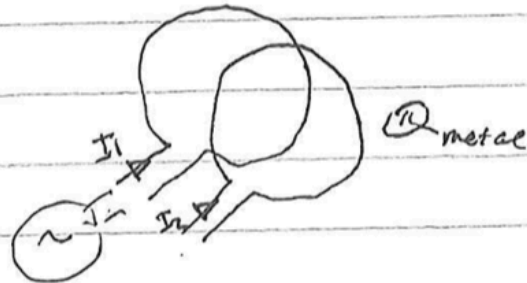
Two Loops



$$L_{12} \geq 0? \quad L_{12} < 0$$

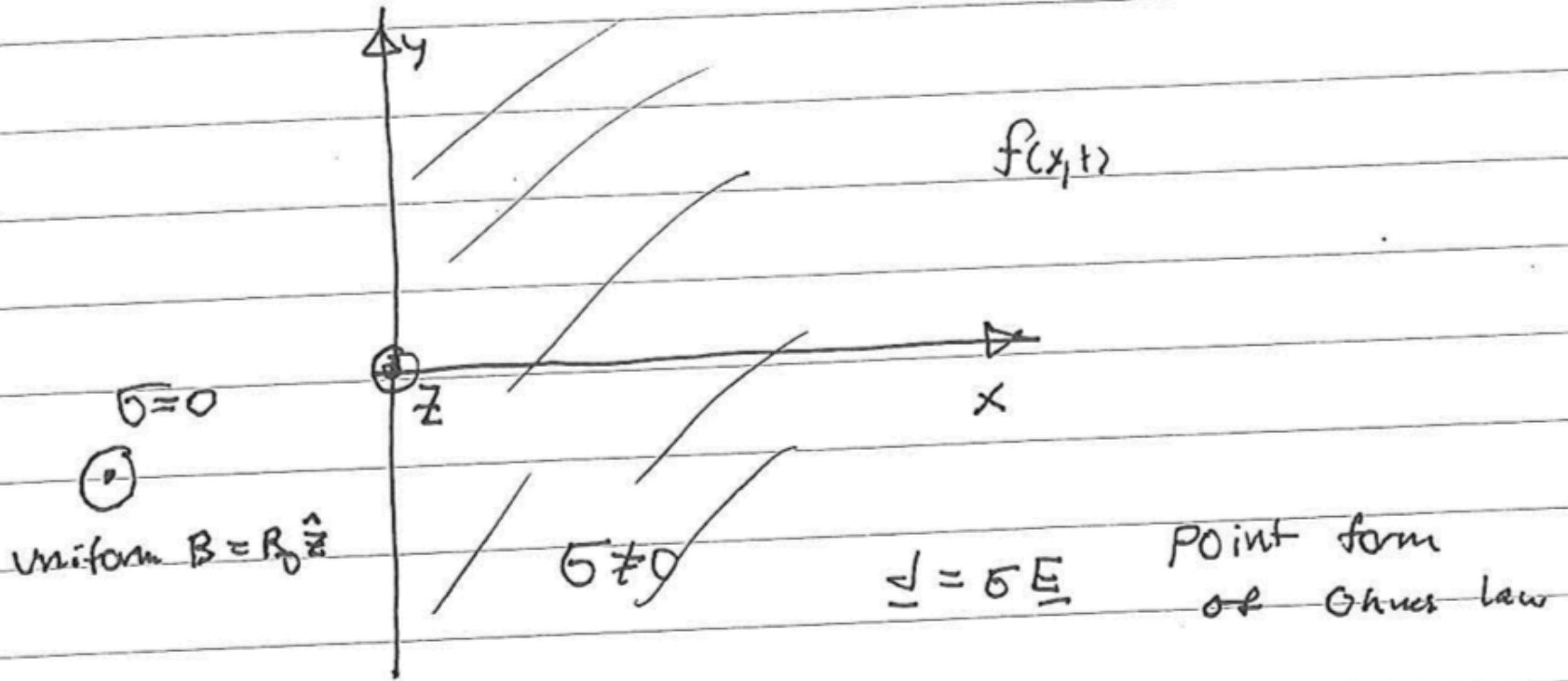


$$L_{12} \geq 0? \quad L_{12} > 0$$



$$L_{12} \stackrel{?}{=} 0$$

Skin Effect



For $x > 0$ what components of fields

$$\underline{B} = (0, 0, B_z)$$

$$\underline{E} = (0, E_y, 0)$$

$$\underline{j} = (0, j_y, 0)$$

$$\frac{\partial B_z(x,t)}{\partial t} = - \left(\frac{\partial E_y}{\partial x} - \frac{\partial E_x}{\partial y} \right)$$

$$- \frac{\partial B_z(x,t)}{\partial x} = \mu_0 (j_y + \epsilon_0 \frac{\partial E_y}{\partial t})$$

$$(\nabla \times \underline{B})_y$$

$$j_y = \sigma E_y$$

"good" conductor

$$\sigma E_y \gg \epsilon_0 \frac{\partial E_y}{\partial t}$$

$$E_y = - \frac{1}{\mu_0 \sigma} \frac{\partial}{\partial x} \frac{\partial B_z}{\partial t}$$

$$\frac{\partial B_z}{\partial t} = - \frac{\partial E_y}{\partial x} = \frac{1}{\mu_0 \sigma} \frac{\partial^2 B_z}{\partial x^2}$$

D

diffusion Eqn

$$D = \frac{1}{\mu_0 \sigma} = \text{diffusion coefficient}$$

Diffusion Equation

$$\frac{\partial n}{\partial t} = D \frac{\partial^2 n}{\partial x^2} \quad \text{solution} \quad n(x,t) = \frac{n_0}{w(t)} \exp\left[-\frac{x^2}{w^2(t)}\right]$$

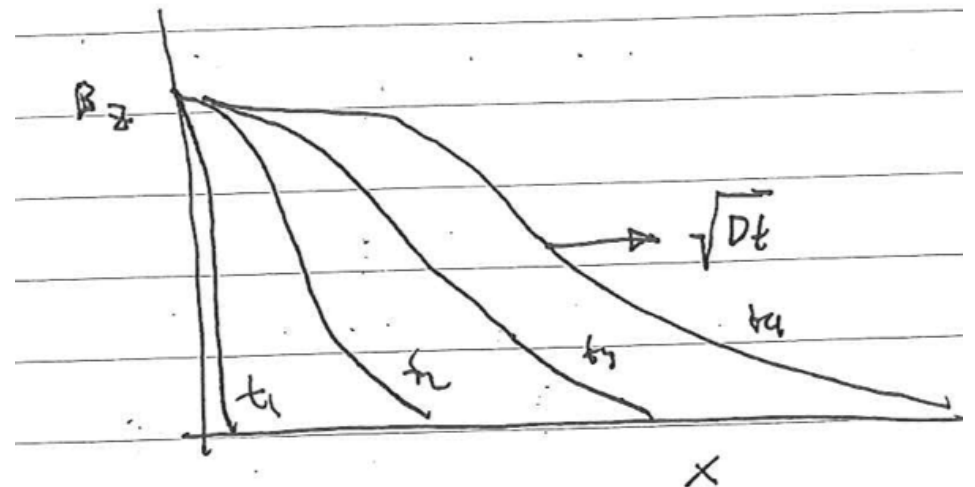
$$w^2(t) = w^2(0) + 4Dt$$

If $n(x,t)$ is a solution then so $B(x,t)$ where $n = \frac{\partial B}{\partial x}$

$$B(x,t) = \frac{2B_0}{\pi^{1/2}} \int_x^\infty dx' \frac{1}{w(t)} \exp\left[-\frac{x'^2}{w^2(t)}\right],$$

$$B(0,t) = B_0$$

$$B(x,t) \rightarrow 0 \quad \text{as} \quad x \rightarrow \infty$$



Time Harmonic

$$\frac{\partial B_z(x,t)}{\partial t} = D \frac{\partial^2 B_z(x,t)}{\partial x^2} \quad B_z(x=0,t) = \text{Re}\{B_0 e^{-i\omega t}\}$$

$$B_z(x=0,t) = \text{Re}\{\hat{B}(x)e^{-i\omega t}\}$$

$$-i\omega \hat{B}(x) = D \frac{\partial^2 \hat{B}(x)}{\partial x^2} \quad \text{Try } \hat{B}(x) = B_0 \exp(-\kappa x)$$

$$-i\omega = D\kappa^2 \quad \kappa = \pm \sqrt{\frac{-i\omega}{D}} = \pm \sqrt{-i} \sqrt{\frac{\omega}{D}} = \pm \frac{1-i}{\sqrt{2}} \sqrt{\frac{\omega}{D}} \quad \text{Pick solution } \text{Re}\{\kappa\} > 0$$

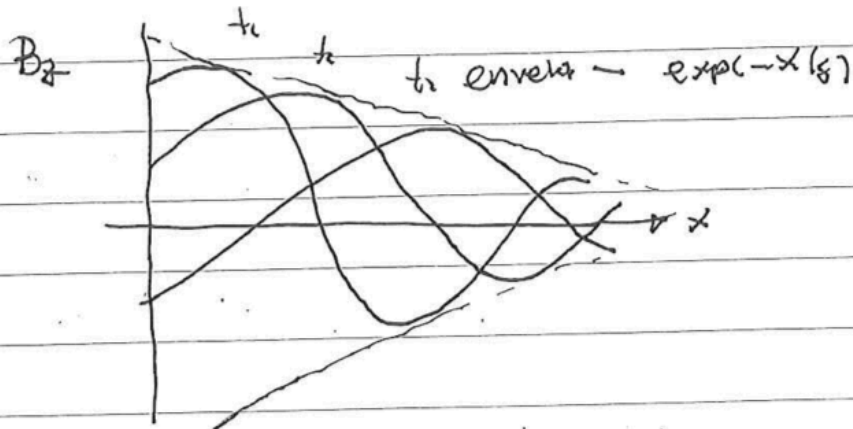
$$\kappa = \frac{1-i}{\delta} \quad \delta = \sqrt{\frac{2D}{\omega}} = \sqrt{\frac{2}{\omega\sigma\mu_0}} \quad \text{Skin Depth}$$

$$B_z(x,t) = \frac{B_0}{2} \operatorname{Re} \left\{ \hat{B}(0) \exp(-i\omega t - (1-i)x/\delta) \right\}$$

$$\delta = \sqrt{\frac{2D}{\omega}} = \sqrt{\frac{2\mu_0}{\sigma\omega}}$$

δ = skin depth

$$B_z(x,t) = \frac{B_0}{2} \exp(-x/\delta) \cos(\omega t - x/\delta)$$



Surface Current Density

Surface Impedance

$$\vec{B}(x,t) = \frac{1}{2} \operatorname{Re} \{ \hat{B}(x) \exp(-i\omega t) \} \quad \hat{B}(x) = \hat{B}(0) \exp(-|K|x)$$

$$|K| = (1-i) \sqrt{\frac{\omega \mu_0 \sigma}{2}}$$

$$\delta = \text{skin depth} = \sqrt{\frac{2}{\omega \mu_0 \sigma}}$$

Ampere's Law $\nabla \times \vec{B} = \mu_0 (\vec{j} + \epsilon_0 \partial \vec{E} / \partial t)$

$$j_y = -\frac{1}{\mu_0} \frac{\partial}{\partial x} B_z$$

$$j_y(x,t) = \frac{1}{2} \operatorname{Re} \left\{ \frac{|K|}{\mu_0} \hat{B}(0) \exp(-i\omega t - |K|x) \right\}$$

↙ flows in
normal dir

$$E_y = \frac{j_y}{\sigma}$$

$$E_y(x,t) = \frac{1}{2} \operatorname{Re} \left\{ \frac{|K|}{\mu_0 \sigma} \hat{B}(0) \exp(-i\omega t - |K|x) \right\}$$

Surface Current Density K_y Amps/meter

$$\underline{B} = \mu_0 \underline{H}$$

$$K_y = \int_0^\infty dx J_y(x,t) = \int_0^\infty dx \left\{ -\frac{1}{\mu_0} \frac{\partial B_z}{\partial x} \right\} = B_z(\omega) / \mu_0 = H_z(\omega)$$

$H [A/m]$

$$E_y(\omega, t) = \text{Re} \left\{ \frac{1K}{\sigma} \hat{H}_z(\omega) \right\}$$

$$\frac{1K}{\sigma} = \frac{1-i}{\sigma \delta}$$

$$\hat{E}_y(\omega) = \frac{1-i}{\sigma \delta} \hat{H}_z(\omega)$$

$\left[\begin{array}{l} \text{V/m} \end{array} \right]$	$\left[\begin{array}{l} \text{ } \end{array} \right]$	$\hat{H}_z(\omega)$	$\hat{H}_z(\omega)$
		μ_0	μ_0
		A/m	A/m
		ohms	ohms

$$Z_s = \frac{1-i}{\sigma \delta} = (1-i) \sqrt{\frac{\omega \mu_0}{2\sigma}}$$

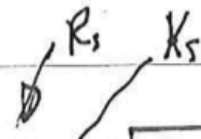


TABLE 8-1
Skin Depths, δ in (mm), of Various Materials

Material	σ (S/m)	$f = 60$ (Hz)	1 (MHz)	1 (GHz)
Silver	6.17×10^7	8.27 (mm)	0.064 (mm)	0.0020 (mm)
Copper	5.80×10^7	8.53	0.066	0.0021
Gold	4.10×10^7	10.14	0.079	0.0025
Aluminum	3.54×10^7	10.92	0.084	0.0027
Iron ($\mu_r \cong 10^3$)	1.00×10^7	0.65	0.005	0.00016
Seawater	4	32 (m)	0.25 (m)	†

† The ϵ of seawater is approximately $72\epsilon_0$. At $f = 1$ (GHz), $\sigma/\omega\epsilon \cong 1$ (not $\gg 1$). Under these conditions, seawater is not a good conductor, and Eq. (8-57) is no longer applicable.

termine the attenuation constant phase constant intrinsic impedance phase velocity